User's Guide

SNVA404B–July 2009–Revised May 2013

AN-1986 LM3429 Boost Evaluation Board

1 Introduction

This evaluation board showcases the LM3429 NFET controller used with a boost current regulator. It is designed to drive 9 to 12 LEDs at a maximum average LED current of 1A from a DC input voltage of 10 to 26V.

The evaluation board showcases most features of the LM3429 including PWM dimming, overvoltage protection and input under-voltage lockout. It also has a right angle connector (J7) which can mate with an external LED load board allowing for the LEDs to be mounted close to the driver. Alternatively, the LED+ and LED- banana jacks can be used to connect the LED load.

The boost circuit can be easily redesigned for different specifications by changing only a few components (see Alternate Designs). Note that design modifications can change the system efficiency for better or worse. See the *LM3429 LM3429Q1 N-Channel Controller for Constant Current LED Drivers* (SNVS616) data sheet for a comprehensive explanation of the device and application information.

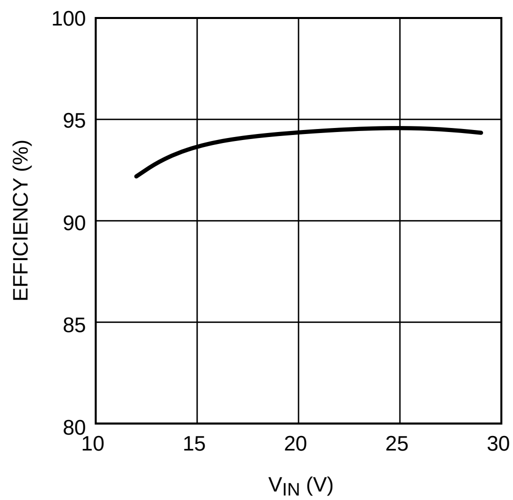

Figure 1. Efficiency with 9 Series LEDS AT 1A

2 Schematic

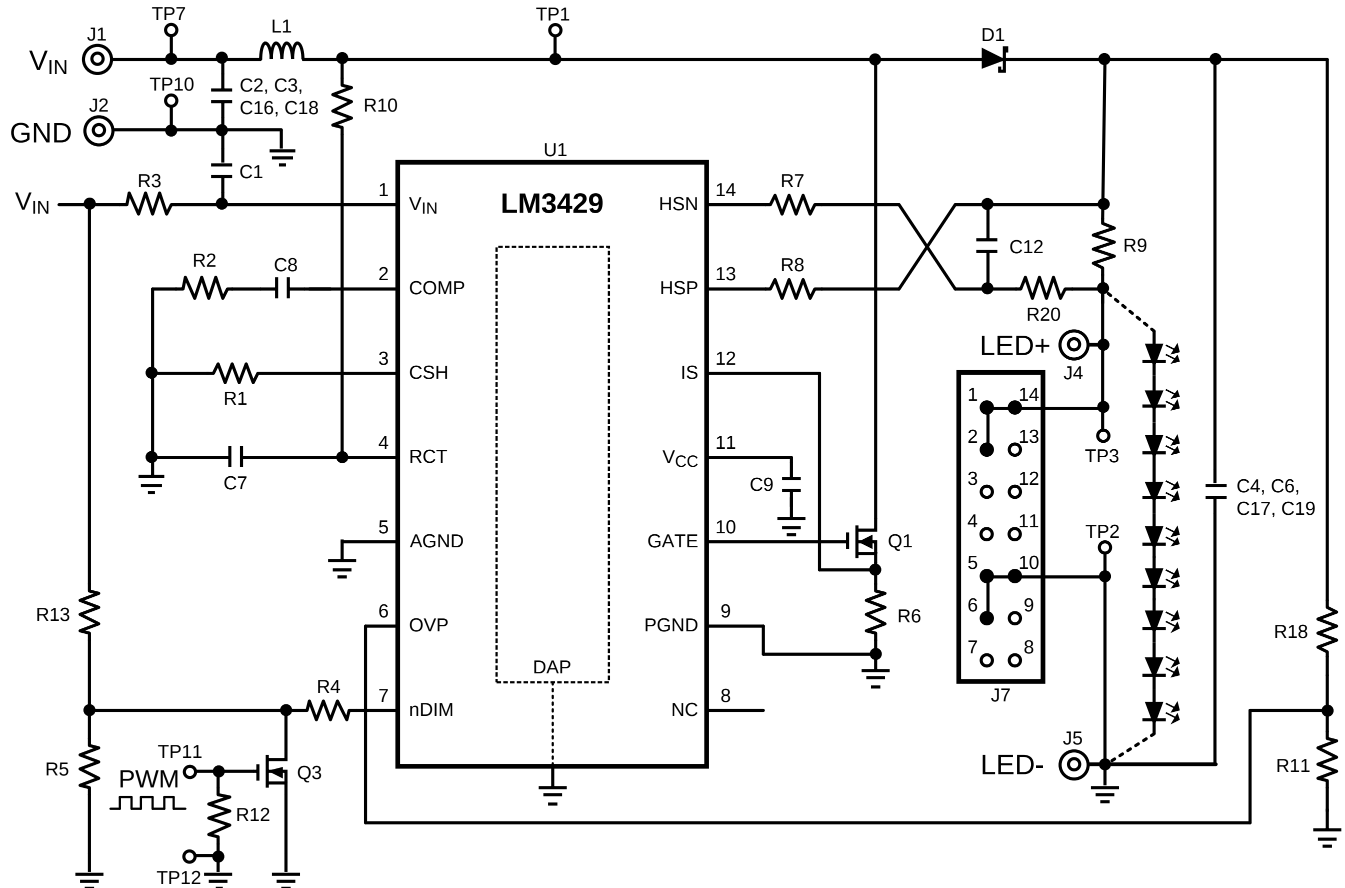

Figure 2. Board Schematic

3 Pin Descriptions

Pin	Name	Description	Application Information
1	V_{IN}	Input Voltage	Bypass with 100 nF capacitor to AGND as close to the device as possible in the circuit board layout.
2	COMP	Compensation	Connect a capacitor to AGND.
3	CSH	Current Sense High	Connect a resistor to AGND to set the signal current. For analog dimming, connect a controlled current source or a potentiometer to AGND as detailed in the *Analog Dimming* section.
4	RCT	Resistor Capacitor Timing	Connect a resistor from the switch node and a capacitor to AGND to set the switching frequency.
5	AGND	Analog Ground	Connect to PGND through the DAP copper circuit board pad to provide proper ground return for CSH, COMP, and RCT.
6	OVP	Over-Voltage Protection	Connect to a resistor divider from V_O to program output over-voltage lockout (OVLO). Turn-off threshold is 1.24V and hysteresis for turn-on is provided by 20 µA current source.
7	nDIM	Not DIM input	Connect a PWM signal for dimming as detailed in the *PWM Dimming* section and/or a resistor divider from V_{IN} to program input under-voltage lockout (UVLO). Turn-on threshold is 1.24V and hysteresis for turn-off is provided by 20 µA current source.
8	NC	No Connection	Leave open.
9	PGND	Power Ground	Connect to AGND through the DAP copper circuit board pad to provide proper ground return for GATE.
10	GATE	Gate Drive Output	Connect to the gate of the external NFET.
11	V_{CC}	Internal Regulator Output	Bypass with a 2.2 µF–3.3 µF, ceramic capacitor to PGND.
12	IS	Main Switch Current Sense	Connect to the drain of the main N-channel MosFET switch for R_{DS-ON} sensing or to a sense resistor installed in the source of the same device.
13	HSP	High-Side LED Current Sense Positive	Connect through a series resistor to the positive side of the LED current sense resistor.
14	HSN	High-Side LED Current Sense Negative	Connect through a series resistor to the negative side of the LED current sense resistor.
DAP (15)	DAP	Thermal pad on bottom of IC	Star ground, connecting AGND and PGND.

4 Bill of Materials

Qty	Part ID	Part Value	Manufacturer	Part Number
2	C1, C4	0.1 µF X7R 10% 100V	TDK	C2012X7R2A104K
4	C2, C3, C16, C18	4.7 µF X7R 10% 100V	MURATA	GRM55ER72A475KA01L
3	C6, C17, C19	2.2 µF X7R 10% 100V	TDK	C4532X7R2A225K
1	C7	1000 pF COG/NPO 5% 50V	MURATA	GRM2165C1H102JA01D
1	C8	1 µF X7R 10% 16V	MURATA	GRM21BR71C105KA01L
1	C9	2.2 µF X7R 10% 16V	MURATA	GRM21BR71C225KA12L
1	C12	0.1 µF X7R 10% 25V	MURATA	GRM21BR71E104KA01L
1	D1	Schottky 100V 12A	VISHAY	12CWQ10FNPBF
4	J1, J2, J4, J5	banana jack	KEYSTONE	575-8
1	J7	2 x 7 shrouded header	SAMTEC	TSSH-107-01-SDRA
1	L1	33 µH 20% 6.3A	COILCRAFT	MSS1278-333MLB
1	Q1	NMOS 100V 40A	VISHAY	SUD40N10-25
1	Q3	NMOS 60V 260 mA	ON-SEMI	2N7002ET1G
1	R1	12.4 kΩ 1%	VISHAY	CRCW080512k4FKEA
1	R2	0Ω 1%	VISHAY	CRCW08050000Z0EA
2	R3, R20	10Ω 1%	VISHAY	CRCW080510R0FKEA

1	R4	16.9 kΩ 1%	VISHAY	CRCW080516k9FKEA
1	R5	1.43 kΩ 1%	VISHAY	CRCW08051k43FKEA
1	R6	0.04Ω 1% 1W	VISHAY	WSL2512R0400FEA
2	R7, R8	1.0 kΩ 1%	VISHAY	CRCW08051k00FKEA
1	R9	0.1Ω 1% 1W	VISHAY	WSL2512R1000FEA
1	R10	35.7 kΩ 1%	VISHAY	CRCW080535k7FKEA
1	R11	15.8 kΩ 1%	VISHAY	CRCW080515k8FKEA
2	R12, R13	10.0 kΩ 1%	VISHAY	CRCW080510k0FKEA
1	R18	750 kΩ 1%	VISHAY	CRCW0805750kFKEA
7	TP1, TP2, TP3, TP7, TP10, TP11, TP12	turret	KEYSTONE	1502-2
1	U1	Buck-boost controller	TI	LM3429

5 PCB Layout

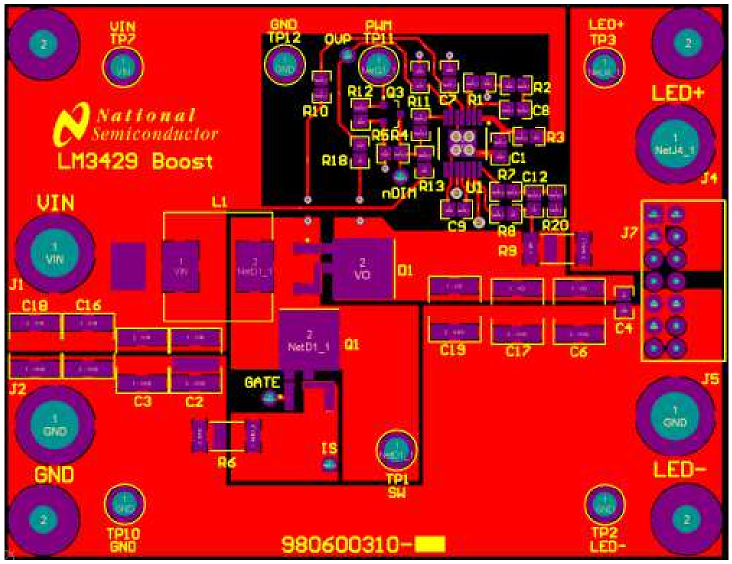

Figure 3. Top Layer

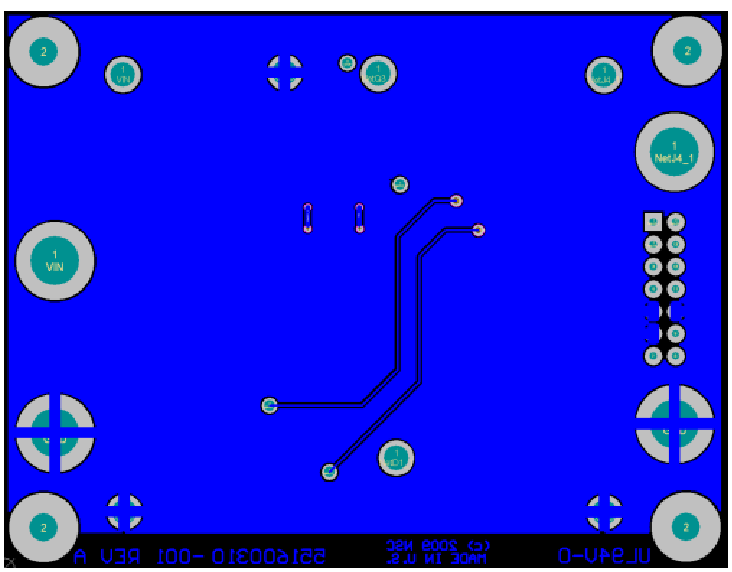

Figure 4. Bottom Layer

6 Design Procedure

Refer to *LM3429 LM3429Q1 N-Channel Controller for Constant Current LED Drivers* (SNVS616) data sheet for design considerations.

6.1 Specifications

$N = 9$

$V_{LED} = 3.5V$

$r_{LED} = 325\ m\Omega$

$V_{IN} = 24V$

$V_{IN\text{-}MIN} = 10V$; $V_{IN\text{-}MAX} = 27V$

$f_{SW} = 700\ kHz$

$V_{SNS} = 100\ mV$

$I_{LED} = 1A$

$\Delta i_{L\text{-}PP} = 250\ mA$

$\Delta i_{LED\text{-}PP} = 17\ mA$

$\Delta v_{IN\text{-}PP} = 100\ mV$

$I_{LIM} = 6A$

$V_{TURN\text{-}ON} = 10V$; $V_{HYS} = 3V$

$V_{TURN\text{-}OFF} = 60V$; $V_{HYSO} = 15V$

6.2 Operating Point

Solve for V_O and r_D:

$$V_O = N \times V_{LED} = 9 \times 3.5V = 31.5V \tag{1}$$

$$r_D = N \times r_{LED} = 9 \times 325\ m\Omega = 2.925\Omega \tag{2}$$

Solve for D, D', D_{MAX}, and D_{MIN}:

$$D = \frac{V_O - V_{IN}}{V_O} = \frac{31.5V - 24V}{31.5V} = 0.238 \tag{3}$$

$$D' = 1 - D = 1 - 0.238 = 0.762 \tag{4}$$

$$D_{MIN} = \frac{V_O - V_{IN\text{-}MAX}}{V_O} = \frac{31.5V - 26V}{31.5V} = 0.175 \tag{5}$$

$$D_{MAX} = \frac{V_O - V_{IN\text{-}MIN}}{V_O} = \frac{31.5V - 10V}{31.5V} = 0.683 \tag{6}$$

6.3 Switching Frequency

Assume C7 = 1 nF and solve for R10:

$$R10 = \frac{25}{f_{SW} \times C7} = \frac{25}{700\ kHz \times 1\ nF} = 35.7\ k\Omega \tag{7}$$

The closest standard resistor is actually 35.7 kΩ therefore the f_{SW} is:

$$f_{SW} = \frac{25}{R10 \times C7} = \frac{25}{35.7\ k\Omega \times 1\ nF} = 700\ kHz \tag{8}$$

The chosen components from step 2 are:

$$\boxed{\begin{array}{l} C7 = 1\ nF \\ R10 = 35.7\ k\Omega \end{array}} \tag{9}$$

6.4 Average LED Current

Solve for R9:

$$R9 = \frac{V_{SNS}}{I_{LED}} = \frac{100\,mV}{1A} = 0.1\Omega \tag{10}$$

Assume R1 = 12.4 kΩ and solve for R8:

$$R8 = \frac{I_{LED}\ x\ R1\ x\ R9}{1.24V} = \frac{1A\ x\ 12.4\ k\Omega\ x\ 0.1\Omega}{1.24V} = 1.0\ k\Omega \tag{11}$$

The closest standard resistor for R9 is 0.1Ω and the closest for R8 (and R7) is actually 1 kΩ therefore I_{LED} is:

$$I_{LED} = \frac{1.24V\ x\ R8}{R9\ x\ R1} = \frac{1.24V\ x\ 1.0\ k\Omega}{0.1\Omega\ x\ 12.4\ k\Omega} = 1.0A \tag{12}$$

The chosen components from step 3 are:

$$\boxed{\begin{array}{l} R9 = 0.1\Omega \\ R1 = 12.4\ k\Omega \\ R8 = R7 = 1\ k\Omega \end{array}} \tag{13}$$

6.5 Inductor Ripple Current

Solve for L1:

$$L1 = \frac{V_{IN}\ x\ D}{\Delta i_{L-PP}\ x\ f_{SW}} = \frac{24V\ x\ 0.238}{250\ mA\ x\ 700\ kHz} = 32.6\ \mu H \tag{14}$$

The closest standard inductor is 33 µH therefore the actual Δi_{L-PP} is:

$$\Delta i_{L-PP} = \frac{V_{IN}\ x\ D}{L1\ x\ f_{SW}} = \frac{24V\ x\ 0.238}{33\ \mu H\ x\ 700\ kHz} = 247\ mA \tag{15}$$

Determine minimum allowable RMS current rating:

$$\begin{aligned} I_{L-RMS} &= \frac{I_{LED}}{D'}\ x\ \sqrt{1 + \frac{1}{12}\ x \left(\frac{\Delta i_{L-PP}\ x\ D'}{I_{LED}}\right)^2} \\ I_{L-RMS} &= \frac{1A}{0.762}\ x\ \sqrt{1 + \frac{1}{12}\ x \left(\frac{247\ mA\ x\ 0.762}{1A}\right)^2} \\ I_{L-RMS} &= 1.31A \end{aligned} \tag{16}$$

The chosen component from step 4 is:

$$\boxed{L1 = 33\ \mu H} \tag{17}$$

6.6 Output Capacitance

Solve for C_O:

$$\begin{aligned} C_O &= \frac{I_{LED}\ x\ D}{r_D\ x\ \Delta i_{LED-PP}\ x\ f_{SW}} \\ C_O &= \frac{1A\ x\ 0.238}{2.925\Omega\ x\ 17\ mA\ x\ 700\ kHz} = 6.84\ \mu F \end{aligned} \tag{18}$$

A total value of 6.6 µF (using 3 2.2 µF X7R ceramic capacitors) is chosen therefore the actual Δi_{LED-PP} is:

$$\begin{aligned} \Delta i_{LED-PP} &= \frac{I_{LED}\ x\ D}{r_D\ x\ C_O\ x\ f_{SW}} \\ \Delta i_{LED-PP} &= \frac{1A\ x\ 0.238}{2.925\Omega\ x\ 6.6\mu F\ x\ 700\ kHz} = 17.6\ mA \end{aligned} \tag{19}$$

Determine minimum allowable RMS current rating:

$$I_{CO\text{-}RMS} = I_{LED} \times \sqrt{\frac{D_{MAX}}{1 - D_{MAX}}} = 1A \times \sqrt{\frac{0.683}{1 - 0.683}} = 1.47A \quad (20)$$

The chosen components from step 5 are:

$$\boxed{C6 = C17 = C19 = 2.2\ \mu F} \quad (21)$$

6.7 Peak Current Limit

Solve for R6:

$$R6 = \frac{245\ mV}{I_{LIM}} = \frac{245\ mV}{6A} = 0.041\,\Omega \quad (22)$$

The closest standard resistor is 0.04 Ω therefore I_{LIM} is:

$$I_{LIM} = \frac{245\ mV}{R6} = \frac{245\ mV}{0.04\Omega} = 6.1A \quad (23)$$

The chosen component from step 6 is:

$$\boxed{R6 = 0.04\Omega} \quad (24)$$

6.8 Loop Compensation

ω_{P1} is approximated:

$$\omega_{P1} = \frac{2}{r_D \times C_O} = \frac{2}{2.925\Omega \times 6.6\,\mu F} = 104k\frac{rad}{sec} \quad (25)$$

ω_{Z1} is approximated:

$$\omega_{Z1} = \frac{r_D \times D'^2}{L1} = \frac{2.925\,\Omega \times 0.762^2}{33\,\mu H} = 52k\frac{rad}{sec} \quad (26)$$

T_{U0} is approximated:

$$T_{U0} = \frac{D' \times 310V}{I_{LED} \times R_{LIM}} = \frac{0.762 \times 310V}{1A \times 0.04\Omega} = 5900 \quad (27)$$

To ensure stability, calculate ω_{P2}:

$$\omega_{P2} = \frac{\min(\omega_{P1}, \omega_{Z1})}{5 \times T_{U0}} = \frac{\omega_{Z1}}{5 \times 5900} = \frac{52k\frac{rad}{sec}}{5 \times 5900} = 1.76\ \frac{rad}{sec} \quad (28)$$

Solve for C8:

$$C8 = \frac{1}{\omega_{P2} \times 5e^6\Omega} = \frac{1}{1.76\ \frac{rad}{sec} \times 5e^6\Omega} = 0.11\,\mu F \quad (29)$$

Since PWM dimming can be evaluated with this board, a much larger compensation capacitor C8 = 1.0 µF is chosen.

To attenuate switching noise, calculate ω_{P3}:

$$\omega_{P3} = \max(\omega_{P1}, \omega_{Z1}) \times 10 = \omega_{P1} \times 10$$

$$\omega_{P3} = 104k\frac{rad}{sec} \times 10 = 1.04\,M\frac{rad}{sec} \quad (30)$$

Assume R20 = 10Ω and solve for C12:

$$C12 = \frac{1}{10\Omega \times \omega_{P3}} = \frac{1}{10\Omega \times 1.04M\frac{rad}{sec}} = 0.097\,\mu F \quad (31)$$

The chosen components from step 7 are:

$$\boxed{\begin{array}{l} C8 = 1.0\,\mu F \\ R20 = 10\Omega \\ C12 = 0.1\,\mu F \end{array}} \tag{32}$$

6.9 Input Capacitance

Solve for the minimum C_{IN}:

$$C_{IN} = \frac{\Delta i_{L-PP}}{8 \times \Delta v_{IN-PP} \times f_{SW}} = \frac{250\text{ mA}}{8 \times 100\text{ mV} \times 700\text{ kHz}} = 0.45\,\mu F \tag{33}$$

To minimize power supply interaction a much larger capacitance of approximately 20 µF is used, therefore the actual Δv_{IN-PP} is much lower. Since high voltage ceramic capacitor selection is limited, four 4.7 µF X7R capacitors are chosen.

Determine minimum allowable RMS current rating:

$$I_{IN-RMS} = \frac{\Delta i_{L-PP}}{\sqrt{12}} = \frac{250\text{ mA}}{\sqrt{12}} = 72\text{ mA} \tag{34}$$

The chosen components from step 8 are:

$$\boxed{C2 = C3 = C16 = C18 = 4.7\,\mu F} \tag{35}$$

6.10 NFET

Determine minimum Q1 voltage rating and current rating:

$$V_{T-MAX} = V_O = 31.5V \tag{36}$$

$$I_{T-MAX} = \frac{0.683}{1-0.683} \times 1A = 2.2A \tag{37}$$

A 100V NFET is chosen with a current rating of 40A due to the low R_{DS-ON} = 50 mΩ. Determine I_{T-RMS} and P_T:

$$I_{T-RMS} = \frac{I_{LED}}{D'} \times \sqrt{D} = \frac{1A}{0.762} \times \sqrt{0.238} = 640\text{ mA} \tag{38}$$

$$P_T = I_{T-RMS}^2 \times R_{DSON} = 640\text{ mA}^2 \times 50\text{ m}\Omega = 20\text{ mW} \tag{39}$$

The chosen component from step 9 is:

$$\boxed{Q1 \rightarrow 40A,\ 100V,\ DPAK} \tag{40}$$

6.11 Diode

Determine minimum D1 voltage rating and current rating:

$$V_{RD-MAX} = V_O = 31.5V \tag{41}$$

$$I_{D-MAX} = I_{LED} = 1A \tag{42}$$

A 100V diode is chosen with a current rating of 12A and V_D = 600 mV. Determine P_D:

$$P_D = I_D \times V_{FD} = 1A \times 600\text{ mV} = 600\text{ mW} \tag{43}$$

The chosen component from step 10 is:

$$\boxed{D1 \rightarrow 12A,\ 100V,\ DPAK} \tag{44}$$

6.12 Input UVLO

Since PWM dimming will be evaluated a three resistor network will be used. Assume R13 = 10 kΩ and solve for R5:

$$R5 = \frac{1.24V \times R13}{V_{TURN\text{-}ON} - 1.24V} = \frac{1.24V \times 10\,k\Omega}{10V - 1.24V} = 1.43\,k\Omega \tag{45}$$

The closest standard resistor is 1.43 kΩ therefore $V_{TURN\text{-}ON}$ is:

$$V_{TURN\text{-}ON} = \frac{1.24V \times (R5 + R13)}{R5}$$

$$V_{TURN\text{-}ON} = \frac{1.24V \times (1.43\,k\Omega + 10\,k\Omega)}{1.43\,k\Omega} = 9.91V \tag{46}$$

Solve for R4:

$$R4 = \frac{R5 \times (V_{HYS} - 20\,\mu A \times R13)}{20\,\mu A \times (R5 + R13)}$$

$$R4 = \frac{1.43\,k\Omega \times (2.9V - 20\,\mu A \times 10\,k\Omega)}{20\,\mu A \times (1.43\,k\Omega + 10\,k\Omega)} = 16.9\,k\Omega \tag{47}$$

The closest standard resistor is 16.9 kΩ making V_{HYS}:

$$V_{HYS} = \frac{20\,\mu A \times R4 \times (R5 + R13)}{R5} + 20\,\mu A \times R_{UV2}$$

$$V_{HYS} = \frac{20\,\mu A \times 16.9\,k\Omega \times (1.43\,k\Omega + 10\,k\Omega)}{1.43\,k\Omega} + 20\,\mu A \times 10\,k\Omega = 2.9V \tag{48}$$

The chosen components from step 11 are:

$$\boxed{\begin{array}{l} R5 = 1.43\,k\Omega \\ R13 = 10\,k\Omega \\ R4 = 16.9\,k\Omega \end{array}} \tag{49}$$

6.13 Output OVLO

Solve for R18:

$$R18 = \frac{V_{HYSO}}{20\,\mu A} = \frac{15V}{20\,\mu A} = 750\,k\Omega \tag{50}$$

The closest standard resistor is 750 kΩ therefore V_{HYSO} is:

$$V_{HYSO} = R18 \times 20\,\mu A = 750\,k\Omega \times 20\,\mu A = 15V \tag{51}$$

Solve for R11:

$$R11 = \frac{1.24V \times R18}{V_{TURN\text{-}OFF} - 1.24V} = \frac{1.24V \times 750\,k\Omega}{60V - 1.24V} = 15.8\,k\Omega \tag{52}$$

The closest standard resistor is 15.8 kΩ making $V_{TURN\text{-}OFF}$:

$$V_{TURN\text{-}OFF} = \frac{1.24V \times (R11 + R18)}{R11}$$

$$V_{TURN\text{-}OFF} = \frac{1.24V \times (15.8\,k\Omega + 750\,k\Omega)}{15.8\,k\Omega} = 40V \tag{53}$$

The chosen components from step 12 are:

$$\boxed{\begin{array}{l} R11 = 15.8\,k\Omega \\ R18 = 750\,k\Omega \end{array}} \tag{54}$$

7 Typical Waveforms

T_A = +25°C, V_{IN} = 24V and V_O = 31.5V.

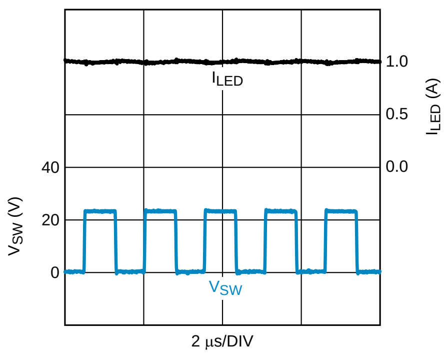

Figure 5. Standard Operation TP1 Switch Node Voltage (V_{SW}) LED Current (I_{LED})

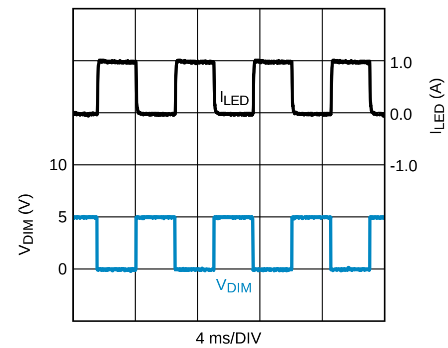

Figure 6. 200Hz 50% PWM Dimming TP11 Dim Voltage (V_{DIM}) LED Current (I_{LED})

8 Alternate Designs

Alternate designs with the LM3429 evaluation board are possible with very few changes to the existing hardware. The evaluation board FETs and diodes are already rated higher than necessary for design flexibility. The input UVLO, output OVP, input and output capacitance can remain the same for the designs shown below. These alternate designs can be evaluated by changing only R9, R10, and L1.

Table 1 gives the main specifications for four different designs and the corresponding values for R9, R10, and L1. PWM dimming can be evaluated with any of these designs.

Table 1. Alternate Design Specifications

Specification / Component	Design 1	Design 2	Design 3	Design 4
V_{IN}	10V	15V	20V	25V
V_O	14V	21V	28V	35V
f_{SW}	600kHz	700kHz	500kHz	700kHz
I_{LED}	2A	500mA	2.5A	1.25A
R9	0.05Ω	0.2Ω	0.04Ω	0.08Ω
R10	41.2 kΩ	35.7 kΩ	49.9 kΩ	35.7 kΩ
L1	22µH	68µH	15µH	33µH