

TLV07

SBOS832A - JULY 2017-REVISED AUGUST 2017

# TLV07 36-V Precision, Rail-to-Rail Output Operational Amplifier

#### **Features**

Low Offset Voltage: 100 µV (Maximum)

Rail-to-Rail Output

Low Noise: 19 nV / √Hz

Unity-Gain Stable

**RFI** Filtered Inputs

Input Range Includes Negative Supply

Rail-to-Rail Output

Gain Bandwidth: 1 MHz

Low Quiescent Current: 930 µA

Full Industrial Temperature Range: -40°C to +125°C

Offered in the Industry-Standard 8-Pin SOIC Package

## 2 Applications

- **Battery Testers**
- Tracking Amplifier in Power Modules
- Merchant Power Supplies
- **Transducer Amplifiers**
- **Temperature Measurements**
- Strain Gauge Amplifiers

## 3 Description

The TLV07 device is a 36-V, single-supply, low-noise, precision operational amplifier (op manufactured using TI's laser trim operational amplifier technology. Each amplifiers' input offset voltage is trimmed in production to obtain a low offset voltage of 100  $\mu$ V (maximum).

The TLV07 offers outstanding dc precision and ac performance, including rail-to-rail output, low offset voltage (±100 µV, maximum) and 1-MHz bandwidth. The TLV07 is stable at G = 1 with capacitive loads up to 200 pF. The input can operate 100 mV below the negative rail and within 2 V of the positive rail. This wide input voltage range, combined with a high CMRR of 120 dB, make the TLV07 well-suited when operated in the non-inverting configuration.

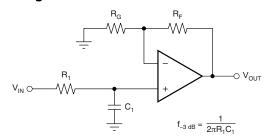
The TLV07 op amp is specified from -40°C to +125°C.

#### Device Information<sup>(1)</sup>

PART NUMBER	PACKAGE	BODY SIZE (NOM)
TLV07	SOIC (8)	4.90 mm × 3.91 mm

(1) For all available packages, see the orderable addendum at the end of the data sheet.

## Single Pole Low-Pass Filter With Gain



$$\frac{V_{OUT}}{V_{IN}} = \left(1 + \frac{R_F}{R_G}\right) \left(\frac{1}{1 + sR_1C_1}\right)$$



## **Table of Contents**

1	Features 1	7.4 Device Functional Modes	16
2	Applications 1	8 Application and Implementation	17
3	Description 1	8.1 Application Information	17
4	Revision History2	8.2 Typical Application	17
5	Pin Configuration and Functions 3	9 Power Supply Recommendations	s 18
6	Specifications4	10 Layout	19
•	6.1 Absolute Maximum Ratings	10.1 Layout Guidelines	19
	6.2 ESD Ratings	10.2 Layout Example	20
	6.3 Recommended Operating Conditions	11 Device and Documentation Supp	oort 21
	6.4 Thermal Information: TLV07	11.1 Device Support	21
	6.5 Electrical Characteristics5	11.2 Documentation Support	22
	6.6 Typical Characteristics	11.3 Community Resources	22
7	Detailed Description	11.4 Trademarks	
-	7.1 Overview	11.5 Electrostatic Discharge Caution.	22
	7.2 Functional Block Diagram	11.6 Glossary	22
	7.3 Feature Description	12 Mechanical, Packaging, and Ord Information	

## 4 Revision History

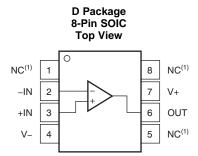
NOTE: Page numbers for previous revisions may differ from page numbers in the current version.

## Changes from Original (July 2017) to Revision A

Page



# 5 Pin Configuration and Functions



## (1) NC- no internal connection

## **Pin Functions: TLV07**

NAME	NO.	I/O	DESCRIPTION
-IN	2	I	Negative (inverting) input
+IN	3	I	Positive (non-inverting) input
NC	1, 5, 8	_	No internal connection (can be left floating)
OUT	6	0	Output
V+	7	_	Positive (highest) power supply
V-	4	_	Negative (lowest) power supply

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## 6 Specifications

#### 6.1 Absolute Maximum Ratings

Over operating free-air temperature range, unless otherwise noted. (1)

	MIN	MAX	UNIT
Supply voltage	-20	20	V
Single supply voltage		40	V
Signal input pin voltage	(V-) - 0.5	(V+) + 0.5	V
Signal input pin current	-10	10	mA
Output short-circuit current <sup>(2)</sup>	Contin	uous	
Operating ambient temperature, T <sub>A</sub>	-40	125	°C
Junction temperature, T <sub>J</sub>		150	°C
Storage temperature, T <sub>stg</sub>	-65	150	°C

<sup>(1)</sup> Stresses beyond those listed under Absolute Maximum Ratings may cause permanent damage to the device. These are stress ratings only, which do not imply functional operation of the device at these or any other conditions beyond those indicated under Recommended Operating Conditions. Exposure to absolute-maximum-rated conditions for extended periods may affect device reliability.

## 6.2 ESD Ratings

			VALUE	UNIT
\/	Floatroatatia diagharga	Human-body model (HBM), per ANSI/ESDA/JEDEC JS-001 <sup>(1)</sup>	±2000	V
V <sub>(ESD)</sub> Electrostatic discharge		Charged-device model (CDM), per JEDEC specification JESD22-C101 <sup>(2)</sup>	±500	V

<sup>(1)</sup> JEDEC document JEP155 states that 500-V HBM allows safe manufacturing with a standard ESD control process.

## 6.3 Recommended Operating Conditions

over operating free-air temperature range (unless otherwise noted)

		MIN	MAX	UNIT
Vs	Supply voltage $(V_S = V + - V -)$	2.7	36	V
T <sub>A</sub>	Operating temperature	-40	125	°C

#### 6.4 Thermal Information: TLV07

		TLV07		
	THERMAL METRIC	D (SOIC)	UNIT	
		8 PINS		
$R_{\theta JA}$	Junction-to-ambient thermal resistance	149.5	°C/W	
$R_{\theta JC(top)}$	Junction-to-case (top) thermal resistance	97.9	°C/W	
$R_{\theta JB}$	Junction-to-board thermal resistance	87.7	°C/W	
ΤιΨ	Junction-to-top characterization parameter	35.5	°C/W	
ΨЈВ	Junction-to-board characterization parameter	89.5	°C/W	
$R_{\theta JC(bot)}$	Junction-to-case (bottom) thermal resistance	_	°C/W	

<sup>(2)</sup> Short-circuit to ground, one amplifier per package.

<sup>(2)</sup> JEDEC document JEP157 states that 250-V CDM allows safe manufacturing with a standard ESD control process.



## 6.5 Electrical Characteristics

at  $T_A$  = 25°C, V+ = +15 V, V- = -15 V,  $V_{CM}$  =  $V_{OUT}$  =  $V_S$  / 2, and  $R_L$  = 10 k $\Omega$  connected to  $V_S$  / 2 (unless otherwise noted).

	PARAMETER	$\frac{V_{OUT} = V_S / 2, \text{ and } K_L = 10 \text{ kg/confident}}{\text{TEST CONDITIONS}}$	MIN	TYP	MAX	UNIT
OFFSET	VOLTAGE		1			
Vos	Input offset voltage			50	±100	μV
dV <sub>OS</sub> /dT	Input offset voltage drift	$T_A = -40$ °C to 125°C		±0.9		μV/°C
PSRR	Input offset voltage vs power supply	V <sub>S</sub> = 2.7 V to 36 V		0.3		μV/V
INPUT BI	AS CURRENT					
1	Input bigg gurrent			±40		pA
I <sub>B</sub>	Input bias current	$T_A = -40$ °C to 125°C		±3		nA
I <sub>OS</sub>	Input offset current			±4		pA
NOISE						
	Input voltage noise	f = 0.1 Hz to 10 Hz		2.7		$\mu V_{PP}$
e <sub>n</sub>	Input voltage noise density	f = 1  kHz		19		nV/√ <del>Hz</del>
INPUT VO	DLTAGE					
V <sub>CM</sub>	Common-mode voltage range		(V-) - 0.1		(V+) - 2	V
CMRR	Common-mode rejection ratio	$V_S = \pm 18 \text{ V}, (V-) - 0.1 \text{ V} < V_{CM} < (V+) - 2 \text{ V}$	104	120		dB
INPUT IM	PEDANCE					
	Differential			100    3		$M\Omega \parallel pF$
	Common-mode			6    3		10 <sup>12</sup> Ω    pF
OPEN-LO	OP GAIN		1			
A <sub>OL</sub>	Open-loop voltage gain	$(V-) + 0.35 V < V_O < (V+) - 0.35 V$	110	130		dB
FREQUE	NCY RESPONSE		1			
GBP	Gain bandwidth product			1		MHz
SR	Slew rate	G = 1		0.4		V/µs
		To 0.1%, V <sub>S</sub> = ±18 V, G = +1, 10-V step		20		μs
t <sub>S</sub>	Settling time	To 0.01% (12-bit), $V_S = \pm 18 \text{ V}$ G = 1 10-V step		28		μs
OUTPUT			•			
Vo	Voltage output swing from rail	$R_L = 10 \text{ k}\Omega$		120		mV
I <sub>SC</sub>	Short-circuit current			17		mA
R <sub>O</sub>	Open-loop output resistance	f = 1  MHz $I_0 = 0 \text{ A}$		900		Ω
POWER S	SUPPLY					
$I_Q$	Quiescent current per amplifier	I <sub>O</sub> = 0 A		930	1800	μΑ
TEMPERA	ATURE					
	Specified range		-40		125	°C
	Operating range		-40		125	°C



## 6.6 Typical Characteristics

 $V_S$  = ±18 V,  $V_{CM}$  =  $V_S$  / 2,  $R_{LOAD}$  = 10 k $\Omega$  connected to  $V_S$  / 2, and  $C_L$  = 100 pF, (unless otherwise noted)

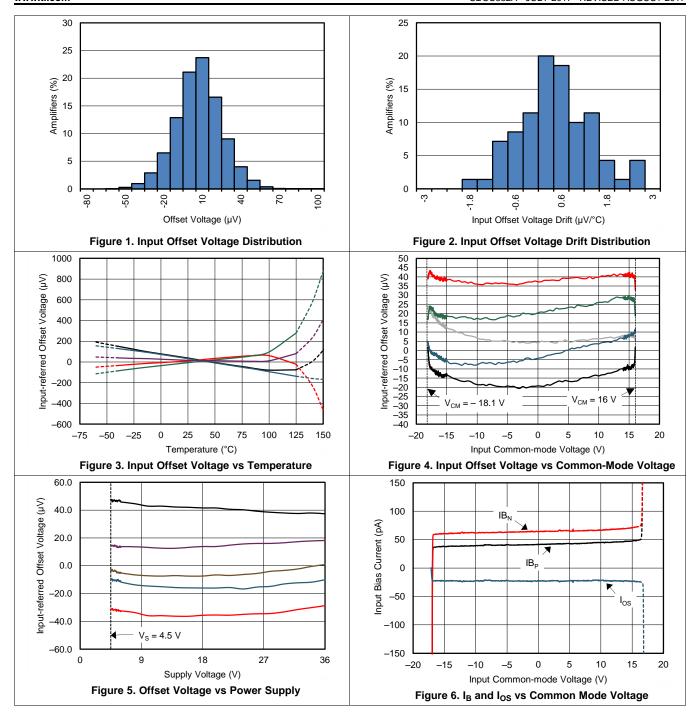
## **Table 1. Characteristic Performance Measurements**

DESCRIPTION	FIGURE
Offset Voltage Production Distribution	Figure 1
Offset Voltage Drift Distribution	Figure 2
Offset Voltage vs Temperature	Figure 3
Offset Voltage vs Common-Mode Voltage	Figure 4
Offset Voltage vs Power Supply	Figure 5
I <sub>B</sub> and I <sub>OS</sub> vs Common-Mode Voltage	Figure 6
Input Bias Current vs Temperature	Figure 7
Output Voltage Swing vs Output Current (Maximum Supply)	Figure 8
CMRR and PSRR vs Frequency (Referred-to-Input)	Figure 9
CMRR vs Temperature	Figure 10
PSRR vs Temperature	Figure 11
0.1-Hz to 10-Hz Noise	Figure 12
Input Voltage Noise Spectral Density vs Frequency	Figure 13
THD+N Ratio vs Frequency	Figure 14
THD+N vs Output Amplitude	Figure 15
Quiescent Current vs Temperature	Figure 16
Quiescent Current vs Supply Voltage	Figure 17
Open-Loop Gain and Phase vs Frequency	Figure 18
Closed-Loop Gain vs Frequency	Figure 19
Open-Loop Gain vs Temperature	Figure 20
Open-Loop Output Impedance vs Frequency	Figure 21
No Phase Reversal	Figure 22
Positive Overload Recovery	Figure 23
Negative Overload Recovery	Figure 24
Small-Signal Step Response	Figure 25, Figure 26
Large-Signal Step Response	Figure 27, Figure 28
Large-Signal Settling Time	Figure 29
Short-Circuit Current vs Temperature	Figure 30
Maximum Output Voltage vs Frequency	Figure 31
EMIRR IN+ vs Frequency	Figure 32

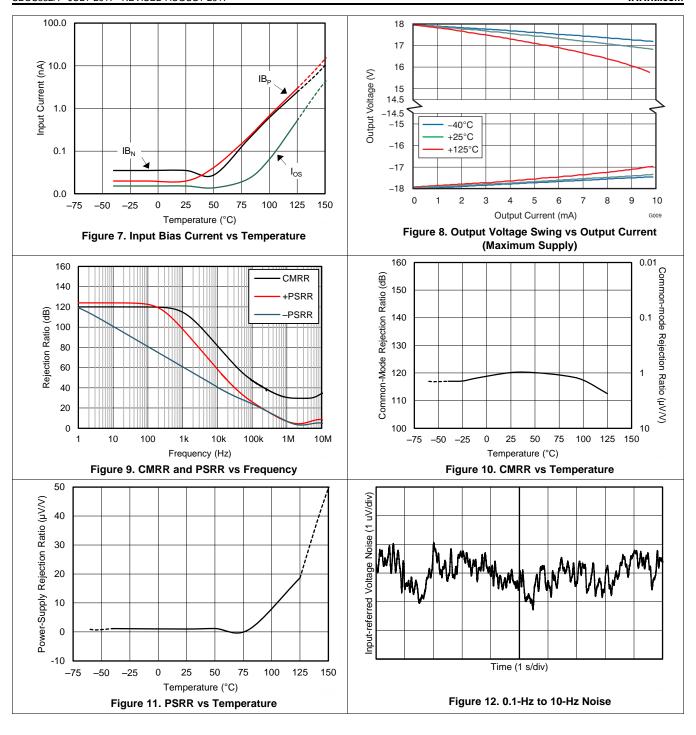
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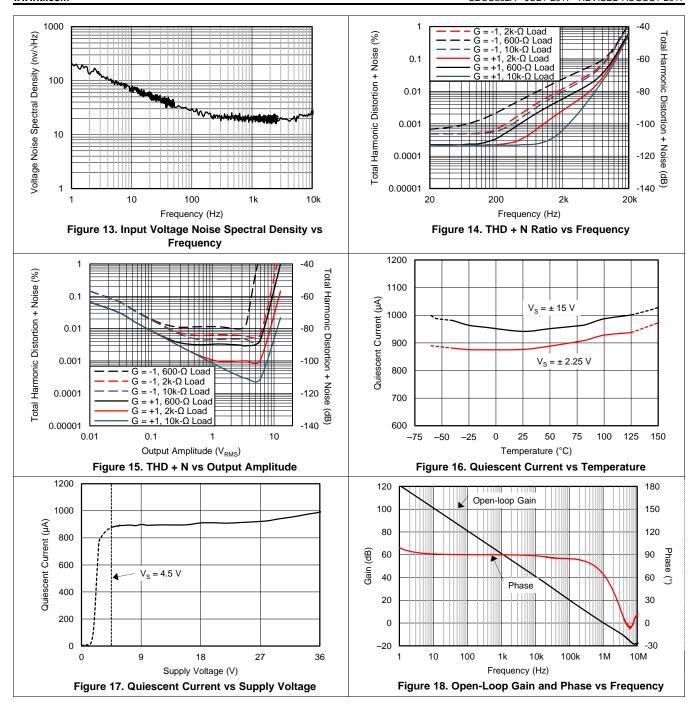




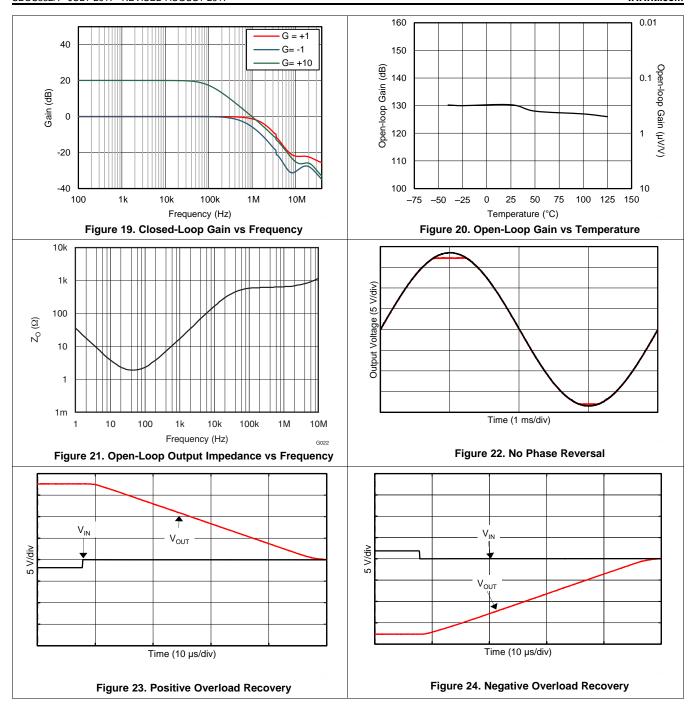




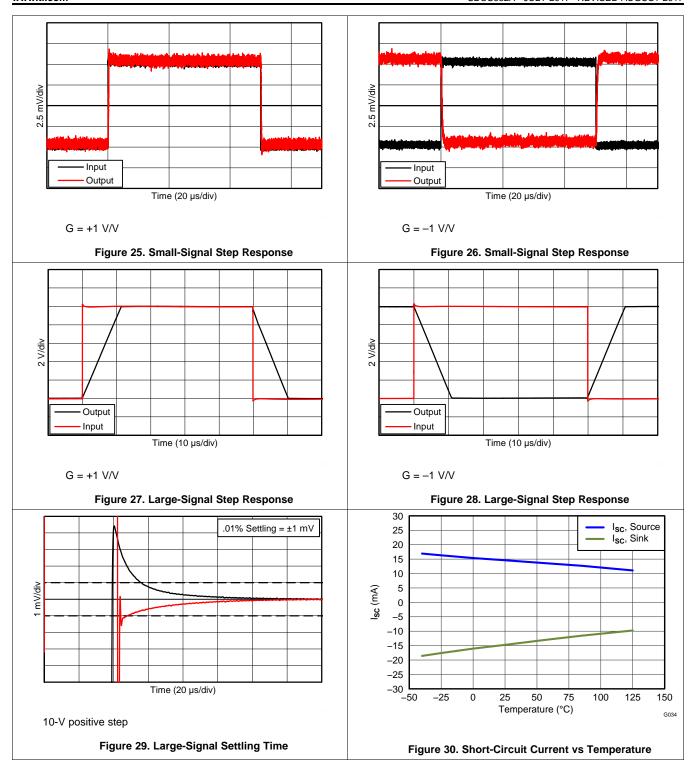






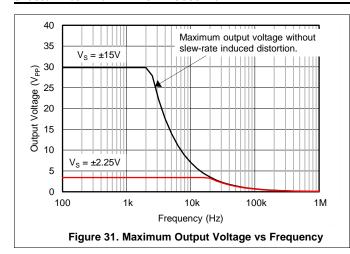


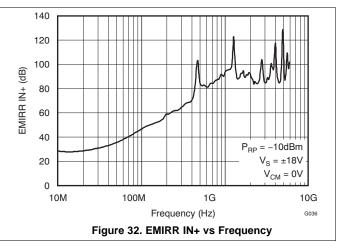




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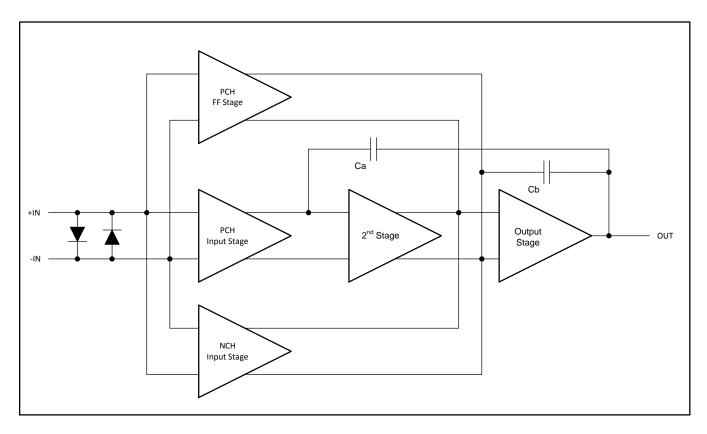


## 7 Detailed Description

#### 7.1 Overview

The TLV07 operational amplifier provides high overall performance, making the device suitable for many general-purpose applications. The excellent offset drift of only 0.9  $\mu$ V/°C provides excellent stability over the entire temperature range. In addition, the device offers very good overall performance with high CMRR, PSRR, and A<sub>OL</sub>.

## 7.2 Functional Block Diagram



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#### 7.3 Feature Description

### 7.3.1 Operating Characteristics

The TLV07 op amp is specified for operation from 2.7 V to 36 V (±1.35 V to ±18 V). Many of the specifications apply from –40°C to +125°C. Parameters that can exhibit significant variance with regard to operating voltage or temperature are shown in *Typical Characteristics*.

#### 7.3.2 Phase-Reversal Protection

The TLV07 has an internal phase-reversal protection. Many operational amplifiers exhibit a phase reversal when the input drives beyond the linear common-mode range. This condition is most often encountered in noninverting circuits when the input drives beyond the specified common-mode voltage range, which causes the output to reverse into the opposite rail. The input of the TLV07 prevents phase reversal with excessive common-mode voltage. Instead, the output limits into the appropriate rail. This performance is shown in Figure 33.

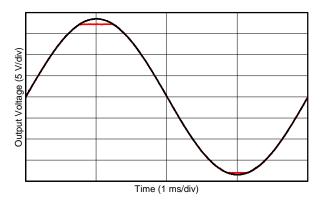


Figure 33. No Phase Reversal

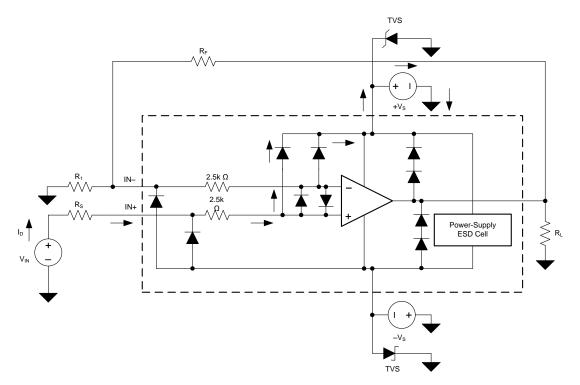
#### 7.3.3 Electrical Overstress

Designers often ask questions about the capability of an operational amplifier to withstand electrical overstress. The questions typically focus on the device inputs, but may involve the supply voltage pins or even the output pin. Each of these different pin functions have electrical stress limits determined by the voltage breakdown characteristics of the particular semiconductor fabrication process and specific circuits connected to the pin. Internal electrostatic discharge (ESD) protection is built into the circuits to protect the circuits from accidental ESD events before and during product assembly.

A good understanding of this basic ESD circuitry and the relevance of the circuitry to an electrical overstress event is helpful. Figure 34 shows the ESD circuits contained in the TLV07 (indicated by the dashed line area). The ESD protection circuitry involves several current-steering diodes connected from the input and output pins and routed back to the internal power-supply lines, where the diodes meet at the power-supply ESD cell, an absorption device, internal to the operational amplifier. This protection circuitry is intended to remain inactive during normal circuit operation.



#### **Feature Description (continued)**



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Figure 34. Equivalent Internal ESD Circuitry Relative to a Typical Circuit Application

An ESD event produces a short-duration, high-voltage pulse that is transformed into a short-duration, high-current pulse when discharging through a semiconductor device. The ESD protection circuits are designed to provide a current path around the operational amplifier core to prevent damage. The energy absorbed by the protection circuitry is then dissipated as heat.

When an ESD voltage develops across two or more amplifier device pins, current flows through one or more steering diodes. Depending on the path that the current takes, the absorption device can activate. The absorption device has a trigger, or threshold voltage, that is above the normal operating voltage of the TLV07, but below the device breakdown voltage level. When this threshold is exceeded, the absorption device quickly activates and clamps the voltage across the supply rails to a safe level.

When the operational amplifier connects into a circuit (see Figure 34), the ESD protection components are intended to remain inactive and do not become involved in the application circuit operation. However, circumstances may arise where an applied voltage exceeds the operating voltage range of a given pin. If this condition occurs, there is a risk that some internal ESD protection circuits can turn on and conduct current. Any such current flow occurs through steering-diode paths and rarely involves the absorption device.

Figure 34 shows a specific example where the input voltage  $(V_{IN})$  exceeds the positive supply voltage (V+) by 500 mV or more. Much of what happens in the circuit depends on the supply characteristics. If V+ can sink the current, one of the upper input steering diodes conducts and directs current to V+. Excessively high current levels can flow with increasingly higher  $V_{IN}$ . As a result, the data sheet specifications recommend that applications limit the input current to 10 mA.

If the supply is not capable of sinking the current,  $V_{IN}$  sources current to the operational amplifier and becomes the source of positive supply voltage. The danger in this case is that the voltage can rise to levels that exceed the operational amplifier absolute maximum ratings.

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#### **Feature Description (continued)**

Another common question involves what happens to the amplifier if an input signal is applied to the input when the power supplies (V+ or V-) are at 0 V. This question depends on the supply characteristic when at 0 V, or at a level below the input signal amplitude. If the supplies appear as high impedance, then the input source supplies the operational amplifier current through the current-steering diodes. This state is not a normal bias condition; most likely, the amplifier does not operate normally. If the supplies are low impedance, then the current through the steering diodes can become quite high. The current level depends on the ability of the input source to deliver current, and any resistance in the input path.

If there is any uncertainty about the ability of the supply to absorb this current, add external Zener diodes to the supply pins; see Figure 34. Select the Zener voltage so that the diode does not turn on during normal operation. However, the Zener voltage must be low enough so that the Zener diode conducts if the supply pin begins to rise above the safe-operating, supply-voltage level.

The TLV07 input pins are protected from excessive differential voltage with back-to-back diodes; see Figure 34. In most circuit applications, the input protection circuitry has no effect. However, in low-gain or G=1 circuits, fast-ramping input signals can forward-bias these diodes because the output of the amplifier cannot respond rapidly enough to the input ramp. If the input signal is fast enough to create this forward-bias condition, limit the input signal current to 10 mA or less. If the input signal current is not inherently limited, use an input series resistor to limit the input signal current.

#### 7.4 Device Functional Modes

#### 7.4.1 Overload Recovery

Overload recovery is defined as the time required for the op amp output to recover from the saturated state to the linear state. The output devices of the op amp enter the saturation region when the output voltage exceeds the rated operating voltage resulting from the high input voltage or the high gain. After the device enters the saturation region, the charge carriers in the output devices must have time to return back to the normal state. After the charge carriers return back to the equilibrium state, the device begins to slew at the normal slew rate. As a result, the propagation delay (in case of an overload condition) is the sum of the overload recovery time and the slew time. The overload recovery time for the TLV07 is approximately 2 µs.



## **Application and Implementation**

#### NOTE

Information in the following applications sections is not part of the TI component specification, and TI does not warrant its accuracy or completeness. TI's customers are responsible for determining suitability of components for their purposes. Customers should validate and test their design implementation to confirm system functionality.

## 8.1 Application Information

The TLV07 op amp provides high overall performance in a large number of general-purpose applications. As with all amplifiers, applications with noisy or high-impedance power supplies require decoupling capacitors placed close to the device pins. In most cases, 0.1-µF capacitors are adequate. Follow the additional recommendations in Layout Guidelines to achieve the maximum performance from this device. Many applications may introduce capacitive loading to the output of the amplifier, potentially causing instability. Add an isolation resistor between the amplifier output and the capacitive load to stabilize the amplifier. Typical Application shows the design process for selecting this resistor.

#### 8.2 Typical Application

This circuit can drive capacitive loads such as cable shields, reference buffers, MOSFET gates, and diodes. The circuit uses an isolation resistor (R<sub>ISO</sub>) to stabilize the output of an op amp. R<sub>ISO</sub> modifies the open-loop gain of the system to ensure the circuit has sufficient phase margin.

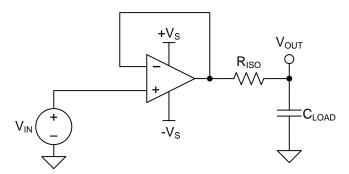


Figure 35. Unity-Gain Buffer With R<sub>ISO</sub> Stability Compensation

#### 8.2.1 Design Requirements

The design requirements are:

- Supply voltage: 30 V (±15 V)
- Capacitive loads: 100 pF, 1000 pF, 0.01  $\mu$ F, 0.1  $\mu$ F, and 1  $\mu$ F
- Phase margin: 45° and 60°

#### 8.2.2 Detailed Design Procedure

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Figure 35 shows a unity-gain buffer driving a capacitive load. Equation 1 shows the transfer function for the circuit in Figure 35. Figure 35 does not show the open-loop output resistance of the op amp (R<sub>O</sub>).

$$T(s) = \frac{1 + C_{LOAD} \times R_{ISO} \times s}{1 + (R_o + R_{ISO}) \times C_{LOAD} \times s}$$
(1)

The transfer function shown in Equation 1 has a pole and a zero. (R<sub>O</sub> + R<sub>ISO</sub>) and C<sub>LOAD</sub> determine the frequency of the pole (fp). The RISO and CLOAD components determine the frequency of the zero (fz). A stable system is obtained by selecting  $R_{ISO}$  such that the rate of closure (ROC) between the open-loop gain ( $A_{OL}$ ) and  $1/\beta$  is 20 dB/decade.

## **Typical Application (continued)**

ROC stability analysis is typically simulated. The validity of the analysis depends on multiple factors, especially the accurate modeling of R <sub>O</sub>. In addition to simulating the ROC, a robust stability analysis includes a measurement of overshoot percentage and ac gain peaking of the circuit using a function generator, oscilloscope, and gain and phase analyzer. These measurements then calculate phase margin. Table 2 shows the overshoot percentage and ac gain peaking that correspond to phase margins of 45° and 60°. For more details on this design and other alternative devices that can be used in place of the TLV07, see *Capacitive Load Drive Solution Using an Isolation Resistor* 

Table 2. Phase Margin versus Overshoot and AC Gain Peaking

PHASE MARGIN	OVERSHOOT	AC GAIN PEAKING
45°	23.3%	2.35 dB
60°	8.8%	0.28 dB

#### 8.2.3 Application Curve

The values of R<sub>ISO</sub> that yield phase margins of 45° and 60° for various capacitive loads are determined using the described methodology Figure 36 shows the results.

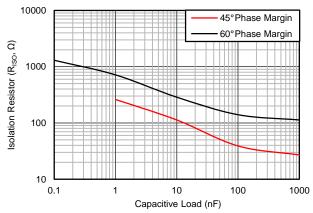


Figure 36. Isolation Resistor Required for Various Capacitive Loads to Achieve a Target Phase Margin

## 9 Power Supply Recommendations

The TLV07 is specified for operation from 2.7 V to 36 V (±1.35 V to ±18 V); many specifications apply from –40°C to +125°C. Parameters that can exhibit significant variance with regard to operating voltage or temperature are presented in *Typical Characteristics*.

#### **CAUTION**

Supply voltages larger than 40 V can permanently damage the device; see *Absolute Maximum Ratings*.

Place 0.1-μF bypass capacitors close to the power-supply pins to reduce errors coupling in from noisy or highimpedance power supplies. For more detailed information on bypass capacitor placement, see *Layout Guidelines*.



## 10 Layout

## 10.1 Layout Guidelines

For best operational performance of the device, use good printed-circuit board (PCB) layout practices, including:

- Noise can propagate into analog circuitry through the power pins of the circuit as a whole and the op amp itself. Bypass capacitors reduce the coupled noise by providing low-impedance power sources local to the analog circuitry.
  - Connect low-ESR, 0.1-µF ceramic bypass capacitors between each supply pin and ground, placed as close to the device as possible. A single bypass capacitor from V+ to ground is applicable for singlesupply applications.
- Separate grounding for analog and digital portions of circuitry is one of the simplest and most-effective
  methods of noise suppression. One or more layers on multilayer PCBs are typically devoted to ground
  planes. A ground plane helps distribute heat and reduces EMI noise pickup. Take care to physically
  separate digital and analog grounds, paying attention to the flow of the ground current.
- In order to reduce parasitic coupling, run the input traces as far away from the supply or output traces as possible. If these traces cannot be kept separate, crossing the sensitive trace perpendicularly is much better than in parallel with the noisy trace.
- Place the external components as close to the device as possible. As shown in Figure 38, keeping R<sub>F</sub> and R<sub>G</sub> close to the inverting input minimizes parasitic capacitance.
- Keep the length of input traces as short as possible. Always remember that the input traces are the most sensitive part of the circuit.
- Consider a driven, low-impedance guard ring around the critical traces. A guard ring can significantly reduce leakage currents from nearby traces that are at different potentials.



## 10.2 Layout Example

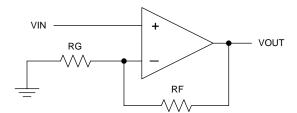


Figure 37. Schematic Representation of a Non-inverting Amplifier

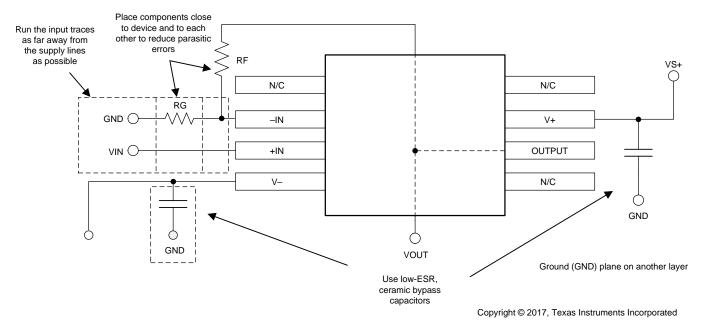


Figure 38. Operational Amplifier Board Layout for a Noninverting Configuration



## 11 Device and Documentation Support

#### 11.1 Device Support

## 11.1.1 Third-Party Products Disclaimer

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#### 11.1.2 Development Support

#### 11.1.2.1 TINA-TI™ (Free Software Download)

TINA<sup>TM</sup> is a simple, powerful, and easy-to-use circuit simulation program based on a SPICE engine. TINA-TI<sup>TM</sup> is a free, fully-functional version of the TINA software, preloaded with a library of macro models in addition to a range of both passive and active models. TINA-TI provides all the conventional dc, transient, and frequency domain analysis of SPICE, as well as additional design capabilities.

Available as a free download from the WEBENCH® Design Center, TINA-TI offers extensive post-processing capability that allows users to format results in a variety of ways. Virtual instruments offer the ability to select input waveforms and probe circuit nodes, voltages, and waveforms, creating a dynamic quick-start tool.

#### NOTE

These files require that either the TINA software (from DesignSoft™) or TINA-TI software be installed. Download the free TINA-TI software from the TINA-TI folder.

#### 11.1.2.2 DIP Adapter EVM

The DIP Adapter EVM tool provides an easy, low-cost way to prototype small surface mount devices. The evaluation tool these TI packages: D or U (SOIC-8), PW (TSSOP-8), DGK (MSOP-8), DBV (SOT23-6, SOT23-5 and SOT23-3), DCK (SC70-6 and SC70-5), and DRL (SOT563-6). The DIP Adapter EVM may also be used with terminal strips or may be wired directly to existing circuits.

#### 11.1.2.3 Universal Op Amp EVM

The Universal Op Amp EVM is a series of general-purpose, blank circuit boards that simplify prototyping circuits for a variety of device package types. The evaluation module board design allows many different circuits to be constructed easily and quickly. Five models are offered, with each model intended for a specific package type. PDIP, SOIC, MSOP, TSSOP and SOT-23 packages are all supported.

#### **NOTE**

These boards are unpopulated, so users must provide their own devices. TI recommends requesting several op amp device samples when ordering the Universal Op Amp EVM.

#### 11.1.2.4 TI Precision Designs

TI Precision Designs are analog solutions created by Ti's precision analog applications experts and offer the theory of operation, component selection, simulation, complete PCB schematic and layout, bill of materials, and measured performance of many useful circuits. TI Precision Designs are available online at <a href="http://www.ti.com/ww/en/analog/precision-designs/">http://www.ti.com/ww/en/analog/precision-designs/</a>.



#### **Device Support (continued)**

### 11.1.2.5 WEBENCH® Filter Designer

WEBENCH® Filter Designer is a simple, powerful, and easy-to-use active filter design program. The WEBENCH® Filter Designer allows the user to create optimized filter designs using a selection of TI operational amplifiers and passive components from TI's vendor partners.

Available as a web-based tool from the WEBENCH® Design Center, WEBENCH® Filter Designer allows the user to design, optimize, and simulate complete multistage active filter solutions within minutes.

### 11.2 Documentation Support

#### 11.2.1 Related Documentation

For related documentation, see the following (available for download from www.ti.com):

- Feedback Plots Define Op Amp AC Performance
- Capacitive Load Drive Solution Using an Isolation Resistor

## 11.3 Community Resources

The following links connect to TI community resources. Linked contents are provided "AS IS" by the respective contributors. They do not constitute TI specifications and do not necessarily reflect TI's views; see TI's Terms of Lise

TI E2E™ Online Community T's Engineer-to-Engineer (E2E) Community. Created to foster collaboration among engineers. At e2e.ti.com, you can ask questions, share knowledge, explore ideas and help solve problems with fellow engineers.

**Design Support** *TI's Design Support* Quickly find helpful E2E forums along with design support tools and contact information for technical support.

#### 11.4 Trademarks

TINA-TI, E2E are trademarks of Texas Instruments. WEBENCH is a registered trademark of Texas Instruments. TINA, DesignSoft are trademarks of DesignSoft, Inc.

#### 11.5 Electrostatic Discharge Caution



These devices have limited built-in ESD protection. The leads should be shorted together or the device placed in conductive foam during storage or handling to prevent electrostatic damage to the MOS gates.

#### 11.6 Glossary

SLYZ022 — TI Glossary.

This glossary lists and explains terms, acronyms, and definitions.

## 12 Mechanical, Packaging, and Orderable Information

The following pages include mechanical, packaging, and orderable information. This information is the most current data available for the designated devices. This data is subject to change without notice and revision of this document. For browser-based versions of this data sheet, refer to the left-hand navigation.



## PACKAGE OPTION ADDENDUM

6-Feb-2020

#### PACKAGING INFORMATION

Orderable Device	Status	Package Type	Package Drawing	Pins	Package Qty	Eco Plan	Lead/Ball Finish	MSL Peak Temp	Op Temp (°C)	Device Marking (4/5)	Samples
TLV07IDR	ACTIVE	SOIC	D	8	2500	Green (RoHS & no Sb/Br)	NIPDAU	Level-2-260C-1 YEAR	-40 to 125	TLV07	Samples

(1) The marketing status values are defined as follows:

ACTIVE: Product device recommended for new designs.

LIFEBUY: TI has announced that the device will be discontinued, and a lifetime-buy period is in effect.

NRND: Not recommended for new designs. Device is in production to support existing customers, but TI does not recommend using this part in a new design.

PREVIEW: Device has been announced but is not in production. Samples may or may not be available.

**OBSOLETE:** TI has discontinued the production of the device.

(2) RoHS: TI defines "RoHS" to mean semiconductor products that are compliant with the current EU RoHS requirements for all 10 RoHS substances, including the requirement that RoHS substance do not exceed 0.1% by weight in homogeneous materials. Where designed to be soldered at high temperatures, "RoHS" products are suitable for use in specified lead-free processes. TI may reference these types of products as "Pb-Free".

RoHS Exempt: TI defines "RoHS Exempt" to mean products that contain lead but are compliant with EU RoHS pursuant to a specific EU RoHS exemption.

**Green:** TI defines "Green" to mean the content of Chlorine (CI) and Bromine (Br) based flame retardants meet JS709B low halogen requirements of <=1000ppm threshold. Antimony trioxide based flame retardants must also meet the <=1000ppm threshold requirement.

- (3) MSL, Peak Temp. The Moisture Sensitivity Level rating according to the JEDEC industry standard classifications, and peak solder temperature.
- (4) There may be additional marking, which relates to the logo, the lot trace code information, or the environmental category on the device.
- (5) Multiple Device Markings will be inside parentheses. Only one Device Marking contained in parentheses and separated by a "~" will appear on a device. If a line is indented then it is a continuation of the previous line and the two combined represent the entire Device Marking for that device.
- (6) Lead/Ball Finish Orderable Devices may have multiple material finish options. Finish options are separated by a vertical ruled line. Lead/Ball Finish values may wrap to two lines if the finish value exceeds the maximum column width.

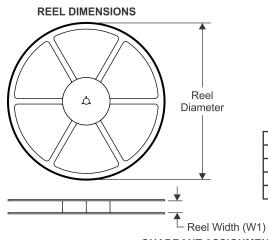
**Important Information and Disclaimer:** The information provided on this page represents TI's knowledge and belief as of the date that it is provided. TI bases its knowledge and belief on information provided by third parties, and makes no representation or warranty as to the accuracy of such information. Efforts are underway to better integrate information from third parties. TI has taken and continues to take reasonable steps to provide representative and accurate information but may not have conducted destructive testing or chemical analysis on incoming materials and chemicals. TI and TI suppliers consider certain information to be proprietary, and thus CAS numbers and other limited information may not be available for release.

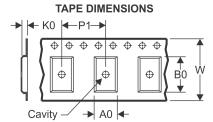
In no event shall TI's liability arising out of such information exceed the total purchase price of the TI part(s) at issue in this document sold by TI to Customer on an annual basis.

## PACKAGE MATERIALS INFORMATION

www.ti.com 25-Oct-2017

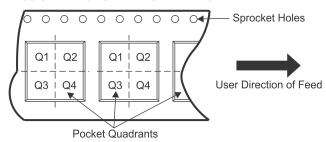
## TAPE AND REEL INFORMATION





	Dimension designed to accommodate the component width
	Dimension designed to accommodate the component length
K0	Dimension designed to accommodate the component thickness
W	Overall width of the carrier tape
P1	Pitch between successive cavity centers

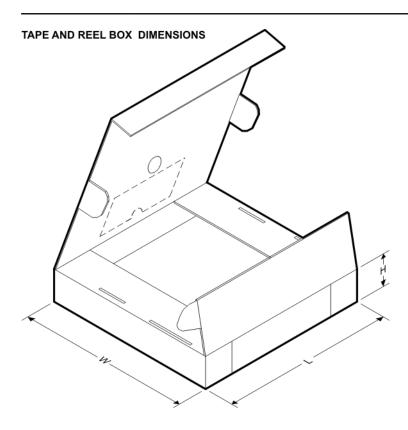
QUADRANT ASSIGNMENTS FOR PIN 1 ORIENTATION IN TAPE



#### \*All dimensions are nominal

ar amorbiolo are norminar												
Device	Package Type	Package Drawing		SPQ	Reel Diameter (mm)	Reel Width W1 (mm)	A0 (mm)	B0 (mm)	K0 (mm)	P1 (mm)	W (mm)	Pin1 Quadrant
TLV07IDR	SOIC	D	8	2500	330.0	12.5	6.4	5.2	2.1	8.0	12.0	Q1
TLV07IDR	SOIC	D	8	2500	330.0	12.4	6.4	5.2	2.1	8.0	12.0	Q1

www.ti.com 25-Oct-2017



#### \*All dimensions are nominal

Device	Package Type	Package Drawing	Pins	SPQ	Length (mm)	Width (mm)	Height (mm)
TLV07IDR	SOIC	D	8	2500	340.5	338.1	20.6
TLV07IDR	SOIC	D	8	2500	367.0	367.0	35.0



SMALL OUTLINE INTEGRATED CIRCUIT



### NOTES:

- 1. Linear dimensions are in inches [millimeters]. Dimensions in parenthesis are for reference only. Controlling dimensions are in inches. Dimensioning and tolerancing per ASME Y14.5M.
- 2. This drawing is subject to change without notice.
- 3. This dimension does not include mold flash, protrusions, or gate burrs. Mold flash, protrusions, or gate burrs shall not exceed .006 [0.15] per side.
- 4. This dimension does not include interlead flash.
- 5. Reference JEDEC registration MS-012, variation AA.



SMALL OUTLINE INTEGRATED CIRCUIT



NOTES: (continued)

6. Publication IPC-7351 may have alternate designs.

7. Solder mask tolerances between and around signal pads can vary based on board fabrication site.



SMALL OUTLINE INTEGRATED CIRCUIT



NOTES: (continued)

- 8. Laser cutting apertures with trapezoidal walls and rounded corners may offer better paste release. IPC-7525 may have alternate design recommendations.
- 9. Board assembly site may have different recommendations for stencil design.



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