

1.4-W MONO FILTER-FREE CLASS-D AUDIO POWER AMPLIFIER

FEATURES

- 1.4 W Into 8 Ω From a 5 V Supply at THD = 10% (Typ)
- Maximum Battery Life and Minimum Heat
 - Efficiency With an 8- Ω Speaker:
 - 84% at 400 mW
 - 79% at 100 mW
 - 2.8-mA Quiescent Current
 - 0.5- μ A Shutdown Current
- Capable of Driving an 8- Ω Speaker ($2.5\text{ V} \leq V_{DD} \leq 5.5\text{ V}$) and a 4- Ω Speaker ($2.5\text{ V} \leq V_{DD} \leq 4.2\text{ V}$)
- Only Three External Components
 - Optimized PWM Output Stage Eliminates LC Output Filter
 - Internally Generated 250-kHz Switching Frequency Eliminates Capacitor and Resistor
 - Improved PSRR (-71 dB at 217 Hz) and Wide Supply Voltage (2.5 V to 5.5 V) Eliminates Need for a Voltage Regulator
 - Fully Differential Design Reduces RF Rectification and Eliminates Bypass Capacitor
 - Improved CMRR Eliminates Two Input Coupling Capacitors
- Space Saving Package
 - 3 mm $\times$ 3 mm QFN package (DRB)
 - 2,5 mm $\times$ 2,5 mm MicroStar Junior™

BGA Package (ZQY)

- 3 mm $\times$ 5 mm MSOP PowerPAD™ Package (DGN)
- TPA2010D1 Available in 1,45 mm $\times$ 1,45 mm WCSP (YZF)
- Use TPA2006D1 for 1.8 V Logic Compatibility on Shutdown Pin

APPLICATIONS

- Ideal for Wireless or Cellular Handsets and PDAs

DESCRIPTION

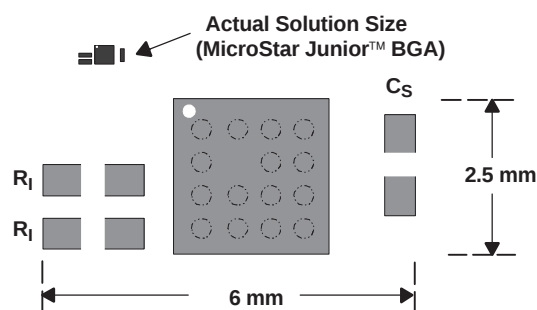
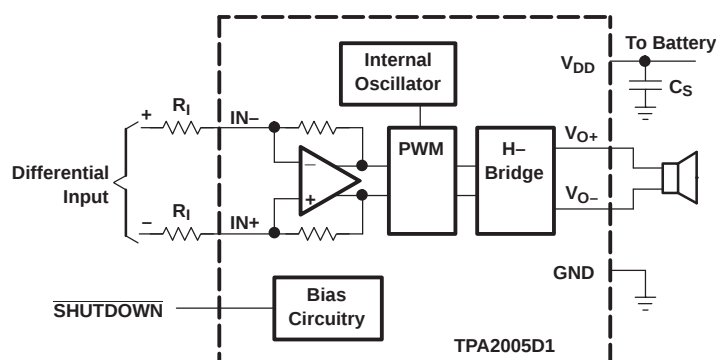
The TPA2005D1 is a 1.4-W high efficiency filter-free class-D audio power amplifier in a MicroStar Junior™ BGA, QFN, or MSOP package that requires only three external components.

Features like 84% efficiency, -71-dB PSRR at 217 Hz, improved RF-rectification immunity, and 15 mm² total PCB area make the TPA2005D1 ideal for cellular handsets. A fast start-up time of 9 ms with minimal pop makes the TPA2005D1 ideal for PDA applications.

In cellular handsets, the earpiece, speaker phone, and melody ringer can each be driven by the TPA2005D1. The device allows independent gain control by summing the signals from each function while minimizing noise to only 48 μ V_{RMS}.

The TPA2005D1 has short-circuit and thermal protection.

APPLICATION CIRCUIT



Please be aware that an important notice concerning availability, standard warranty, and use in critical applications of Texas Instruments semiconductor products and disclaimers thereto appears at the end of this data sheet.

MicroStar Junior, PowerPAD are trademarks of Texas Instruments.



These devices have limited built-in ESD protection. The leads should be shorted together or the device placed in conductive foam during storage or handling to prevent electrostatic damage to the MOS gates.

ORDERING INFORMATION

T _A	PACKAGE ⁽¹⁾	PART NUMBER	SYMBOL
-40°C to 85°C	MicroStar Junior™ (GQY)	TPA2005D1GQYR ⁽²⁾	PB051
	MicroStar Junior™ (ZQY) ⁽³⁾	TPA2005D1ZQYR ⁽²⁾	AAFI
	8-pin QFN (DRB)	TPA2005D1DRBR ⁽²⁾	BIQ
	8-pin MSOP (DGN)	TPA2005D1DGN(R)	BAL

- (1) For the most current package and ordering information, see the Package Option Addendum at the end of this document, or see the TI website at www.ti.com.
- (2) The GQY, ZQY, and DRB packages are only available taped and reeled. An R at the end of the part number indicates the devices are taped and reeled.
- (3) The GQY is the standard MicroStar Junior™ package. The ZQY is lead-free option, and is qualified for 260° lead-free assembly.

ABSOLUTE MAXIMUM RATINGS

over operating free-air temperature range unless otherwise noted⁽¹⁾

		UNIT
V _{DD}	Supply voltage ⁽²⁾	
	In active mode	-0.3 V to 6 V
	In <u>SHUTDOWN</u> mode	-0.3 V to 7 V
V _I	Input voltage	-0.3 V to V _{DD} + 0.3 V
	Continuous total power dissipation	See Dissipation Rating Table
T _A	Operating free-air temperature	-40°C to 85°C
T _J	Operating junction temperature	-40°C to 85°C
T _{stg}	Storage temperature	-65°C to 150°C
R _L	Load resistance	
	2.5 ≤ V _{DD} ≤ 4.2 V	3.2 Ω (Minimum)
	4.2 < V _{DD} ≤ 6 V	6.4 Ω (Minimum)

- (1) Stresses beyond those listed under "absolute maximum ratings" may cause permanent damage to the device. These are stress ratings only, and functional operation of the device at these or any other conditions beyond those indicated under "recommended operating conditions" is not implied. Exposure to absolute-maximum-rated conditions for extended periods may affect device reliability.
- (2) For the MSOP (DGN) package option, the maximum V_{DD} should be limited to 5 V if short-circuit protection is desired.

RECOMMENDED OPERATING CONDITIONS

		MIN	NOM	MAX	UNIT
V _{DD}	Supply voltage	2.5		5.5	V
V _{IH}	High-level input voltage	<u>SHUTDOWN</u>		V _{DD}	V
V _{IL}	Low-level input voltage	<u>SHUTDOWN</u>		0.8	V
R _I	Input resistor	Gain ≤ 20 V/V (26 dB)		15	kΩ
V _{IC}	Common mode input voltage range	V _{DD} = 2.5 V, 5.5 V, CMRR ≤ -49 dB		V _{DD} -0.8	V
T _A	Operating free-air temperature	-40		85	°C

DISSIPATION RATINGS

PACKAGE	DERATING FACTOR	T _A ≤ 25°C POWER RATING	T _A = 70°C POWER RATING	T _A = 85°C POWER RATING
GQY, ZQY	16 mW/°C	2 W	1.28 W	1.04 W
DRB	21.8 mW/°C	2.7 W	1.7 W	1.4 W
DGN	17.1 mW/°C	2.13 W	1.36 W	1.11 W

ELECTRICAL CHARACTERISTICS

 $T_A = 25^\circ\text{C}$ (unless otherwise noted)

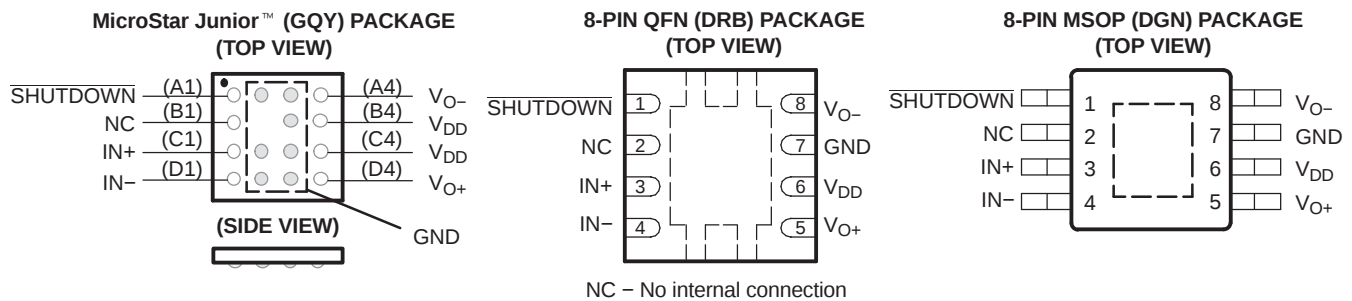
PARAMETER	TEST CONDITIONS	MIN	TYP	MAX	UNIT
$ V_{OS} $ Output offset voltage (measured differentially)	$V_I = 0\text{ V}$, $A_V = 2\text{ V/V}$, $V_{DD} = 2.5\text{ V to } 5.5\text{ V}$			25	mV
PSRR Power supply rejection ratio	$V_{DD} = 2.5\text{ V to } 5.5\text{ V}$		-75	-55	dB
CMRR Common mode rejection ratio	$V_{DD} = 2.5\text{ V to } 5.5\text{ V}$, $V_{IC} = V_{DD}/2\text{ to } 0.5\text{ V}$, $V_{IC} = V_{DD}/2\text{ to } V_{DD} - 0.8\text{ V}$		-68	-49	dB
$ I_{IH} $ High-level input current	$V_{DD} = 5.5\text{ V}$, $V_I = 5.8\text{ V}$			50	μA
$ I_{IL} $ Low-level input current	$V_{DD} = 5.5\text{ V}$, $V_I = 0.3\text{ V}$			1	μA
$I_{(Q)}$ Quiescent current	$V_{DD} = 5.5\text{ V}$, no load		3.4	4.5	mA
	$V_{DD} = 3.6\text{ V}$, no load		2.8		
	$V_{DD} = 2.5\text{ V}$, no load		2.2	3.2	
$I_{(SD)}$ Shutdown current	$V_{(SHUTDOWN)} = 0.8\text{ V}$, $V_{DD} = 2.5\text{ V to } 5.5\text{ V}$		0.5	2	μA
$r_{DS(on)}$ Static drain-source on-state resistance	$V_{DD} = 2.5\text{ V}$		770		m Ω
	$V_{DD} = 3.6\text{ V}$		590		
	$V_{DD} = 5.5\text{ V}$		500		
Output impedance in SHUTDOWN	$V_{(SHUTDOWN)} = 0.8\text{ V}$		>1		k Ω
$f_{(sw)}$ Switching frequency	$V_{DD} = 2.5\text{ V to } 5.5\text{ V}$	200	250	300	kHz
Gain		$2 \times \frac{142\text{ k}\Omega}{R_I}$	$2 \times \frac{150\text{ k}\Omega}{R_I}$	$2 \times \frac{158\text{ k}\Omega}{R_I}$	$\frac{\text{V}}{\text{V}}$

OPERATING CHARACTERISTICS

 $T_A = 25^\circ\text{C}$, Gain = 2 V/V, $R_L = 8\text{ }\Omega$ (unless otherwise noted)

PARAMETER	TEST CONDITIOINS	MIN	TYP	MAX	UNIT
P_O Output power	THD + N= 1%, $f = 1\text{ kHz}$, $R_L = 8\Omega$	$V_{DD} = 5\text{ V}$	1.18		W
		$V_{DD} = 3.6\text{ V}$	0.58		
		$V_{DD} = 2.5\text{ V}$	0.26		
	THD + N= 10%, $f = 1\text{ kHz}$, $R_L = 8\Omega$	$V_{DD} = 5\text{ V}$	1.45		W
		$V_{DD} = 3.6\text{ V}$	0.75		
		$V_{DD} = 2.5\text{ V}$	0.35		
THD+N Total harmonic distortion plus noise	$P_O = 1\text{ W}$, $f = 1\text{ kHz}$, $R_L = 8\text{ }\Omega$	$V_{DD} = 5\text{ V}$	0.18%		
	$P_O = 0.5\text{ W}$, $f = 1\text{ kHz}$, $R_L = 8\text{ }\Omega$	$V_{DD} = 3.6\text{ V}$	0.19%		
	$P_O = 200\text{ mW}$, $f = 1\text{ kHz}$, $R_L = 8\text{ }\Omega$	$V_{DD} = 2.5\text{ V}$	0.20%		
k_{SVR} Supply ripple rejection ratio	$f = 217\text{ Hz}$, $V_{(RIPPLE)} = 200\text{ mV}_{pp}$ Inputs ac-grounded with $C_I = 2\text{ }\mu\text{F}$	$V_{DD} = 3.6\text{ V}$	-71		dB
SNR Signal-to-noise ratio	$P_O = 1\text{ W}$, $R_L = 8\Omega$	$V_{DD} = 5\text{ V}$	97		dB
V_n Output voltage noise	$V_{DD} = 3.6\text{ V}$, $f = 20\text{ Hz to } 20\text{ kHz}$, Inputs ac-grounded with $C_I = 2\text{ }\mu\text{F}$	No weighting	48		μV_{RMS}
		A weighting	36		
CMRR Common mode rejection ratio	$V_{IC} = 1\text{ V}_{pp}$, $f = 217\text{ Hz}$	$V_{DD} = 3.6\text{ V}$	-63		dB
Z_I Input impedance		142	150	158	k Ω
Start-up time from shutdown	$V_{DD} = 3.6\text{ V}$		9		ms

PIN ASSIGNMENTS



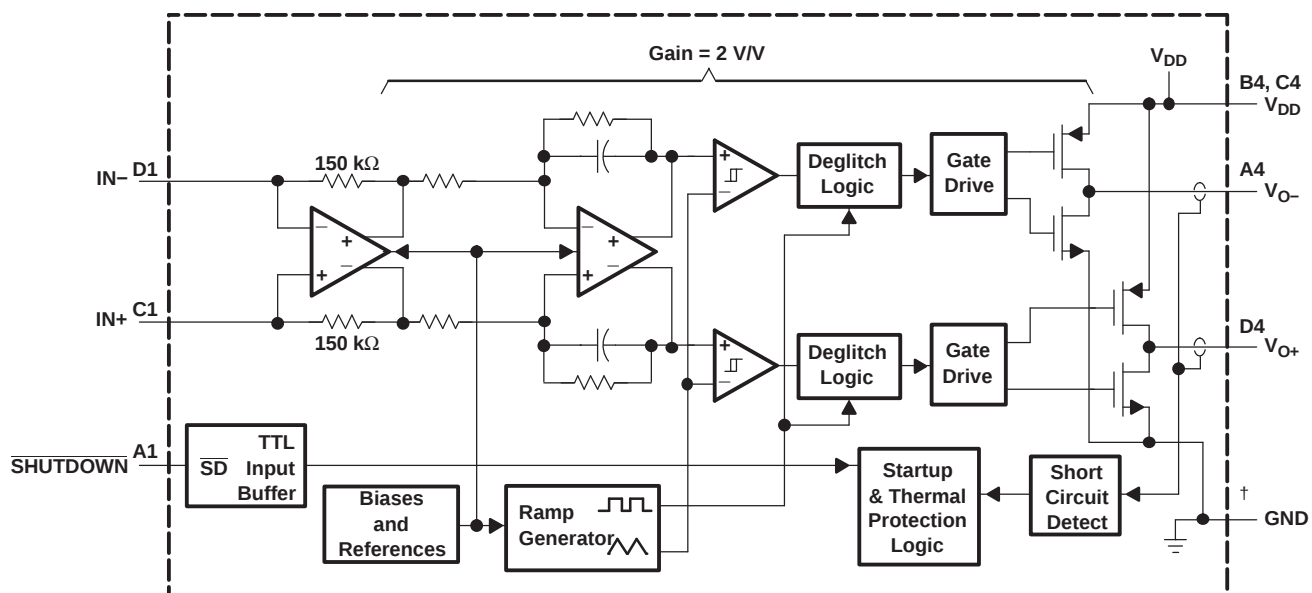
NOTES A. The shaded terminals are used for electrical and thermal connections to the ground plane. All the shaded terminals need to be electrical connected to ground. No connect (NC) terminals still need a pad and trace.

B. The thermal pad of the DRB and DGN packages must be electrically and thermally connected to a ground plane.

Terminal Functions

TERMINAL			I/O	DESCRIPTION
NAME	ZQY, GQY	DRB, DGN		
IN-	D1	4	I	Negative differential input
IN+	C1	3	I	Positive differential input
V _{DD}	B4, C4	6	I	Power supply
V _{O+}	D4	5	O	Positive BTL output
GND	A2, A3, B3, C2, C3, D2, D3	7	I	High-current ground
V _{O-}	A4	8	O	Negative BTL output
SHUTDOWN	A1	1	I	Shutdown terminal (active low logic)
NC	B1	2		No internal connection
Thermal Pad				Must be soldered to a grounded pad on the PCB.

FUNCTIONAL BLOCK DIAGRAM



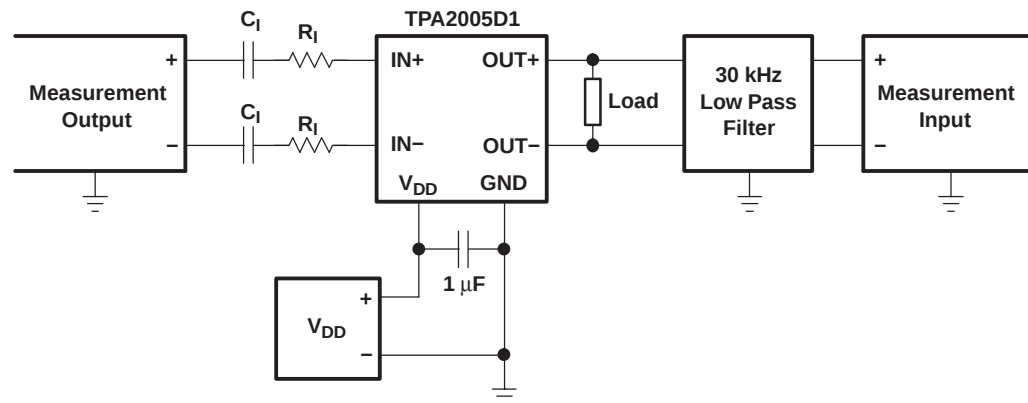
† A2, A3, B3, C2, C3, D2, D3
(terminal labels for MicroStar Junior™ package)

TYPICAL CHARACTERISTICS

Table of Graphs

			FIGURE
Efficiency	vs Output power		1, 2
P_D	Power dissipation	vs Output power	3
Supply current	vs Output power		4, 5
$I_{(Q)}$	Quiescent current	vs Supply voltage	6
$I_{(SD)}$	Shutdown current	vs Shutdown voltage	7
P_O	Output power	vs Supply voltage	8
		vs Load resistance	9, 10
THD+N	Total harmonic distortion plus noise	vs Output power	11, 12
		vs Frequency	13, 14, 15, 16
		vs Common-mode input voltage	17
k_{SVR}	Supply voltage rejection ratio	vs Frequency	18, 19, 20
		vs Common-mode input voltage	21
	GSM power supply rejection	vs Time	22
		vs Frequency	23
CMRR	Common-mode rejection ratio	vs Frequency	24
		vs Common-mode input voltage	25

TEST SET-UP FOR GRAPHS



Notes:

- (1) C_1 was Shorted for any Common-Mode input voltage measurement
- (2) A 33- μ H inductor was placed in series with the load resistor to emulate a small speaker for efficiency measurements.
- (3) The 30-kHz low-pass filter is required even if the analyzer has a low-pass filter. An RC filter (100 Ω , 47 nF) is used on each output for the data sheet graphs.

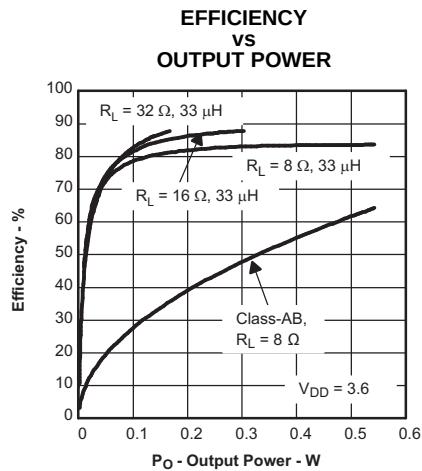


Figure 1.

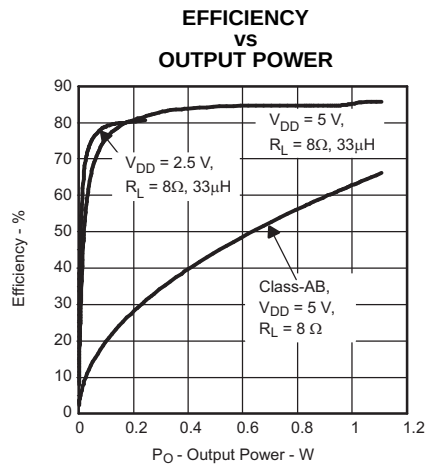


Figure 2.

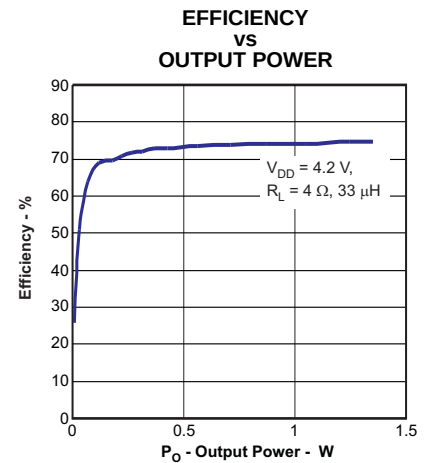


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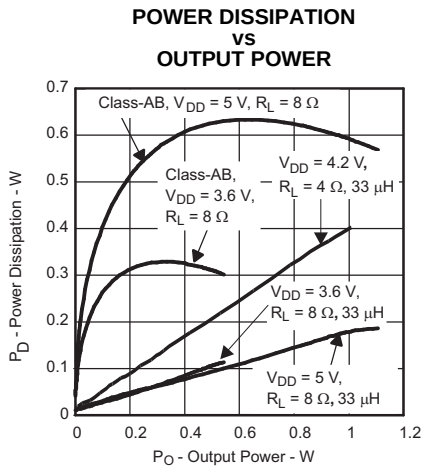


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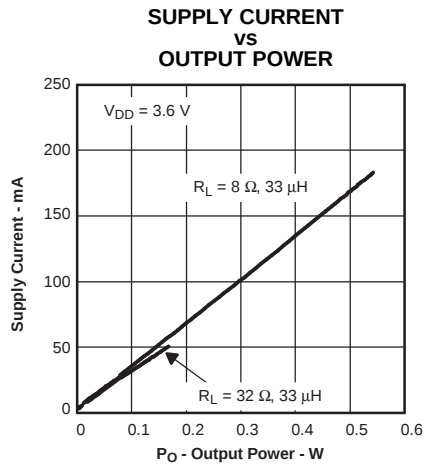


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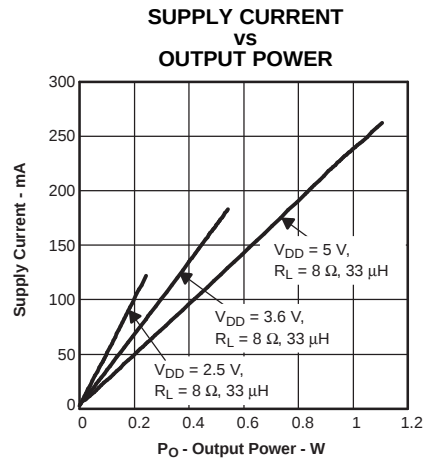


Figure 6.

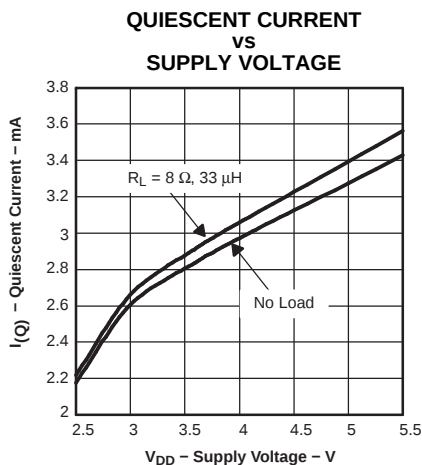


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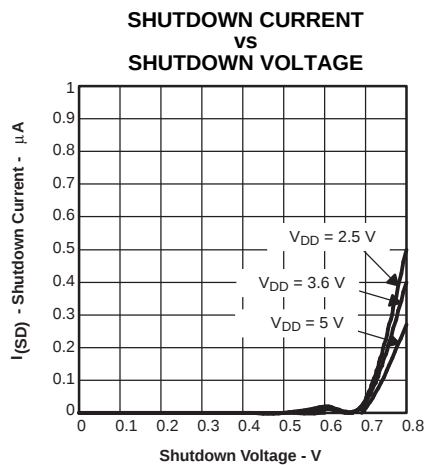


Figure 8.

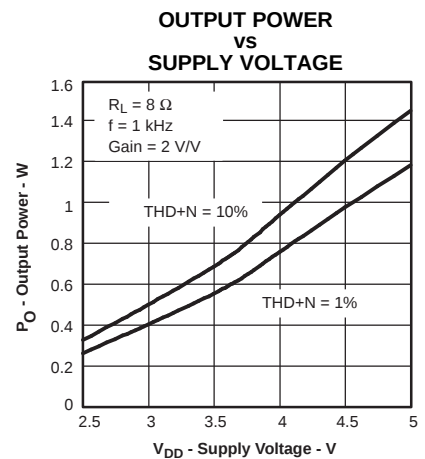


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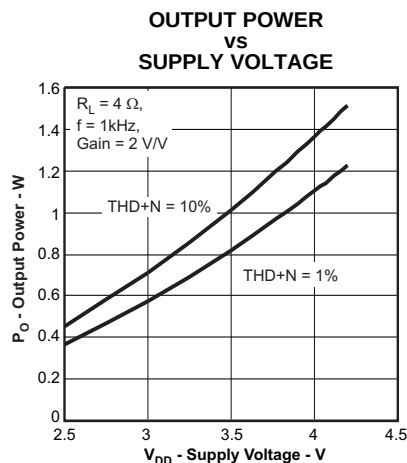


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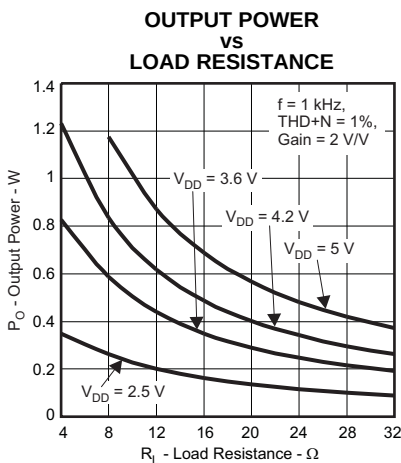


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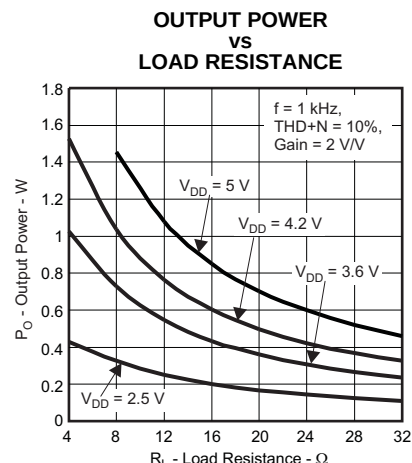


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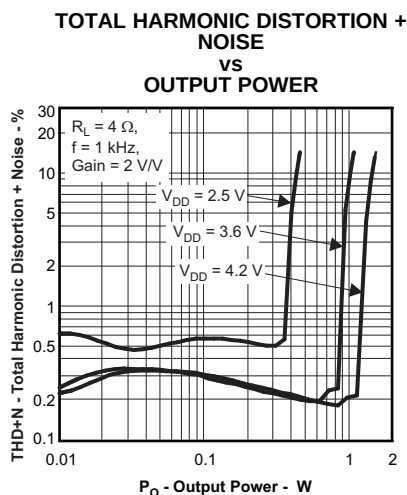


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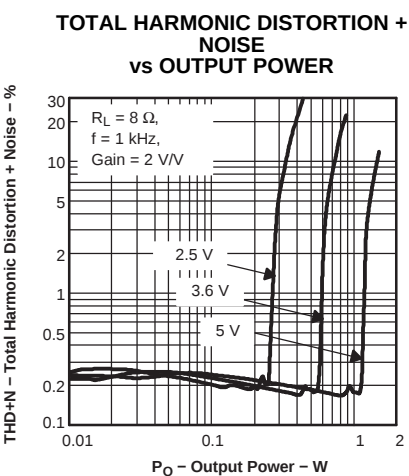


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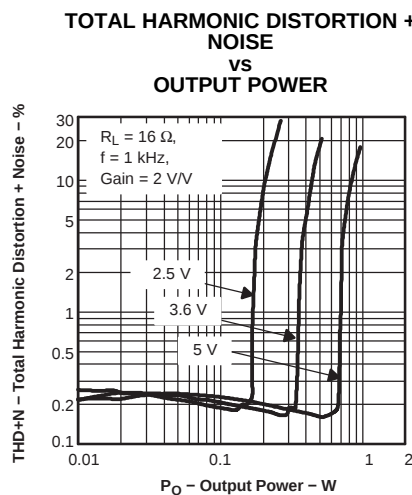


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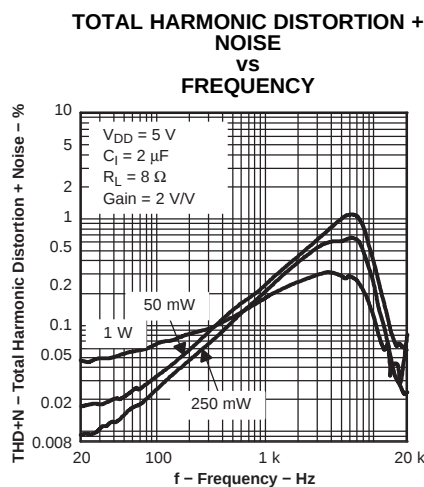


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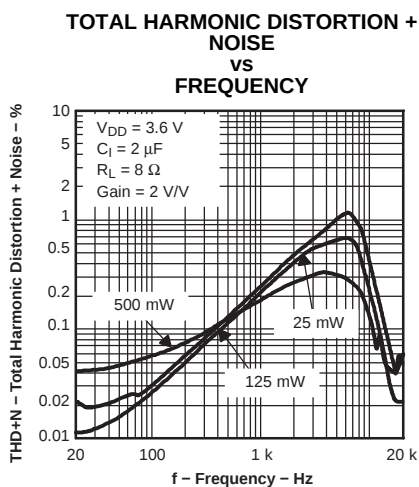


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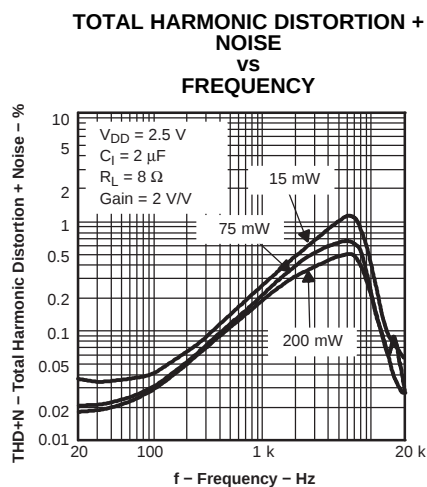


Figure 18.

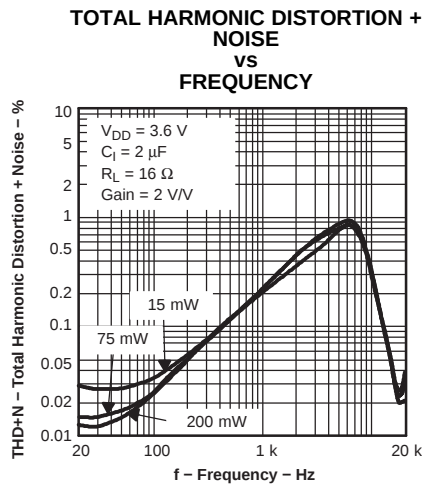


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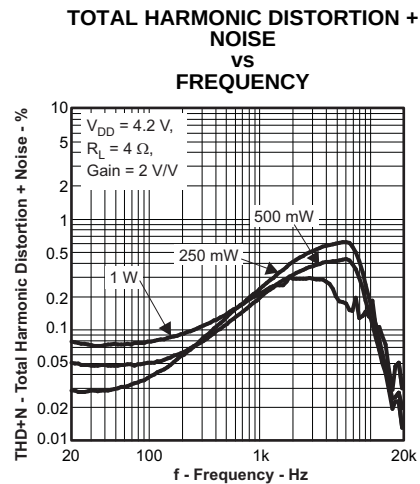


Figure 20.

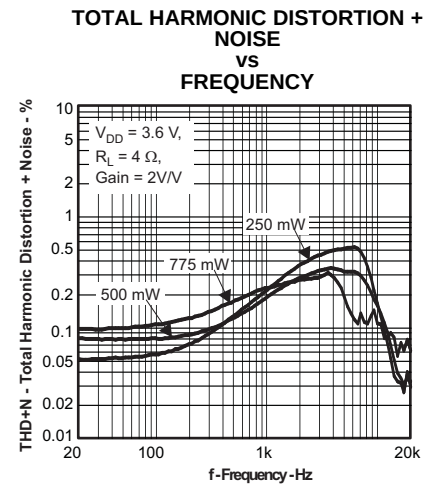


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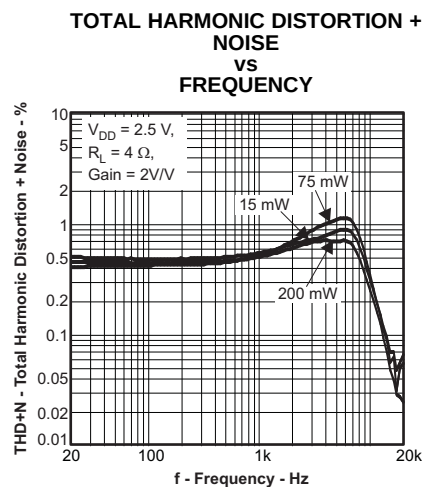


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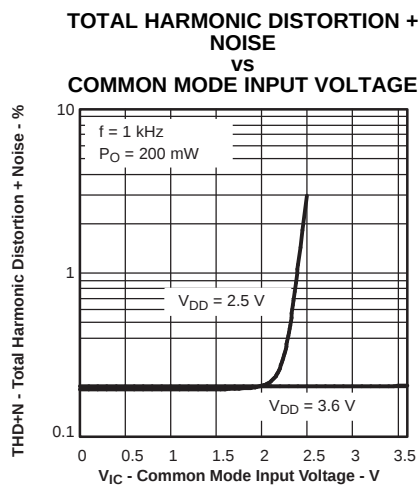


Figure 23.

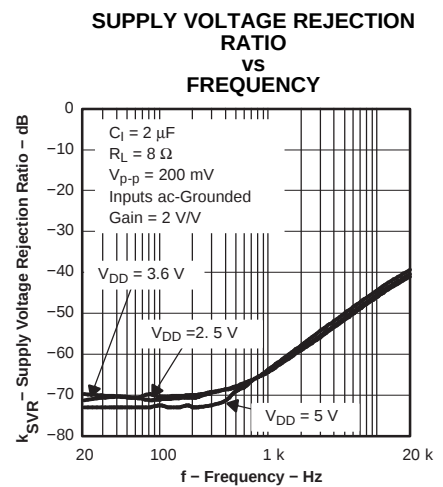


Figure 24.

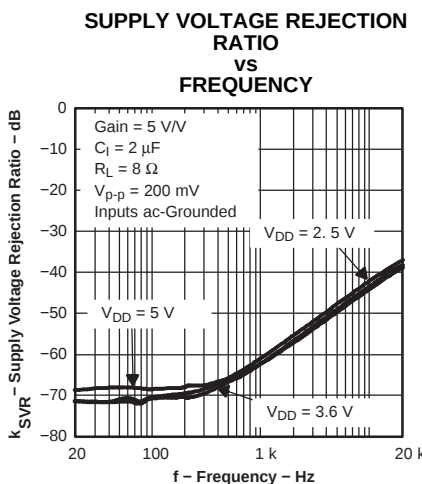


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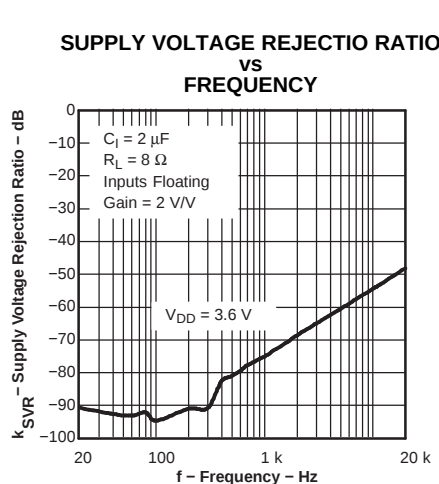


Figure 26.

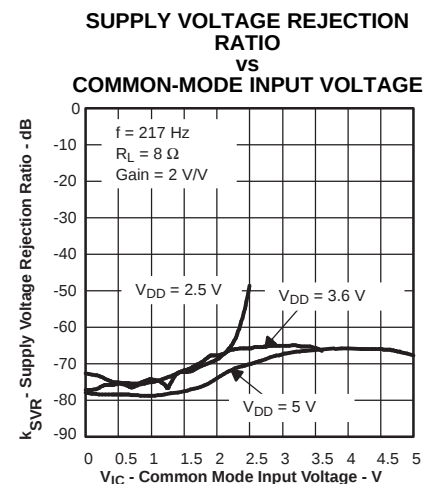


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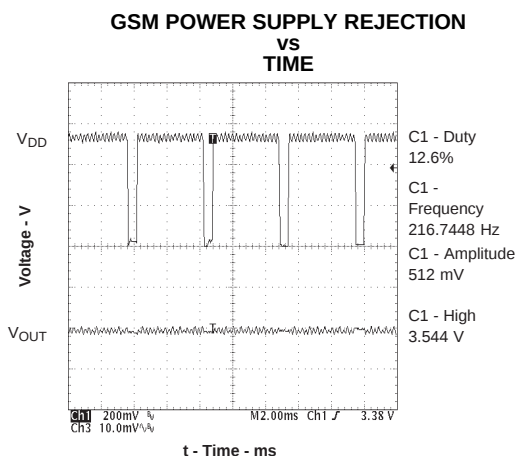


Figure 28.

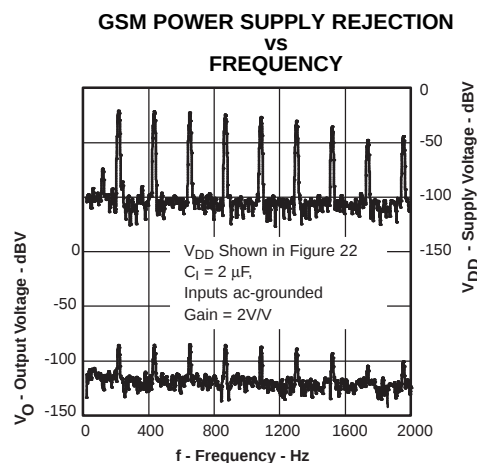


Figure 29.

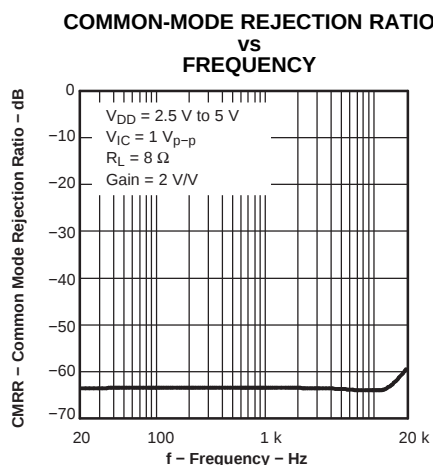


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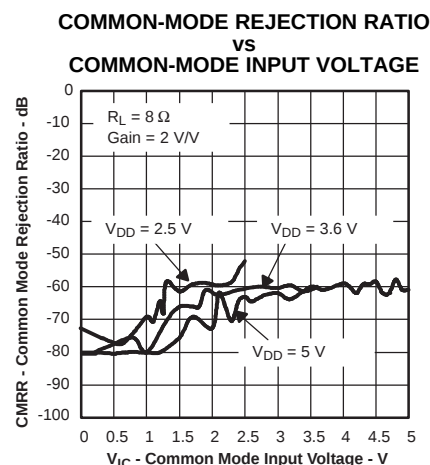


Figure 31.

APPLICATION INFORMATION

FULLY DIFFERENTIAL AMPLIFIER

The TPA2005D1 is a fully differential amplifier with differential inputs and outputs. The fully differential amplifier consists of a differential amplifier and a common-mode amplifier. The differential amplifier ensures that the amplifier outputs a differential voltage on the output that is equal to the differential input times the gain. The common-mode feedback ensures that the common-mode voltage at the output is biased around $V_{DD}/2$ regardless of the common-mode voltage at the input. The fully differential TPA2005D1 can still be used with a single-ended input; however, the TPA2005D1 should be used with differential inputs when in a noisy environment, like a wireless handset, to ensure maximum noise rejection.

Advantages of Fully Differential Amplifiers

- Input-coupling capacitors not required:
 - The fully differential amplifier allows the inputs to be biased at voltage other than mid-supply. For example, if a codec has a midsupply lower than the midsupply of the TPA2005D1, the common-mode feedback circuit will adjust, and the TPA2005D1 outputs will still be biased at midsupply of the TPA2005D1. The inputs of the TPA2005D1 can be biased from 0.5 V to $V_{DD} - 0.8$ V. If the inputs are biased outside of that range, input-coupling capacitors are required.
- Midsupply bypass capacitor, $C_{(BYPASS)}$, not required:
 - The fully differential amplifier does not require a bypass capacitor. This is because any shift in the midsupply affects both positive and negative channels equally and cancels at the differential output.
- Better RF-immunity:
 - GSM handsets save power by turning on and shutting off the RF transmitter at a rate of 217 Hz. The transmitted signal is picked-up on input and output traces. The fully differential amplifier cancels the signal much better than the typical audio amplifier.

COMPONENT SELECTION

Figure 32 shows the TPA2005D1 typical schematic with differential inputs and Figure 33 shows the TPA2005D1 with differential inputs and input capacitors, and Figure 34 shows the TPA2005D1 with single-ended inputs. Differential inputs should be used whenever possible because the single-ended inputs are much more susceptible to noise.

Table 1. Typical Component Values

REF DES	VALUE	EIA SIZE	MANUFACTURER	PART NUMBER
R_I	150 k Ω (0.5%)	0402	Panasonic	ERJ2RHD154V
C_S	1 μ F (+22%, -80%)	0402	Murata	GRP155F50J105Z
$C_I^{(1)}$	3.3 nF (10%)	0201	Murata	GRP033B10J332K

(1) C_I is only needed for single-ended input or if V_{ICM} is not between 0.5 V and $V_{DD} - 0.8$ V. $C_I = 3.3$ nF (with $R_I = 150$ k Ω) gives a high-pass corner frequency of 321 Hz.

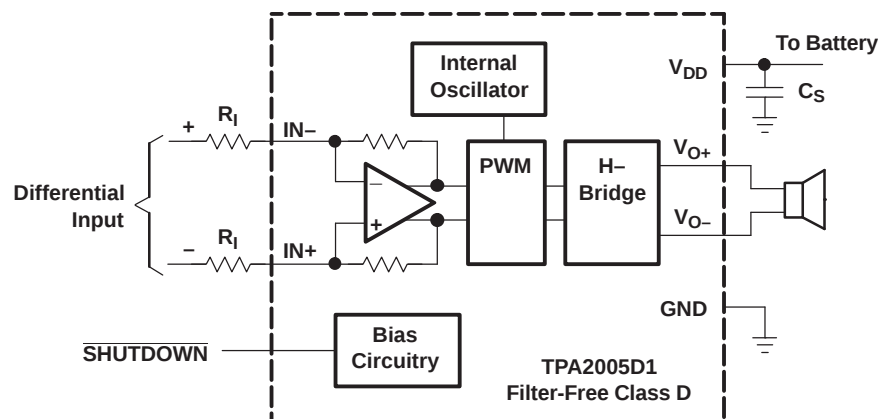


Figure 32. Typical TPA2005D1 Application Schematic With Differential Input for a Wireless Phone

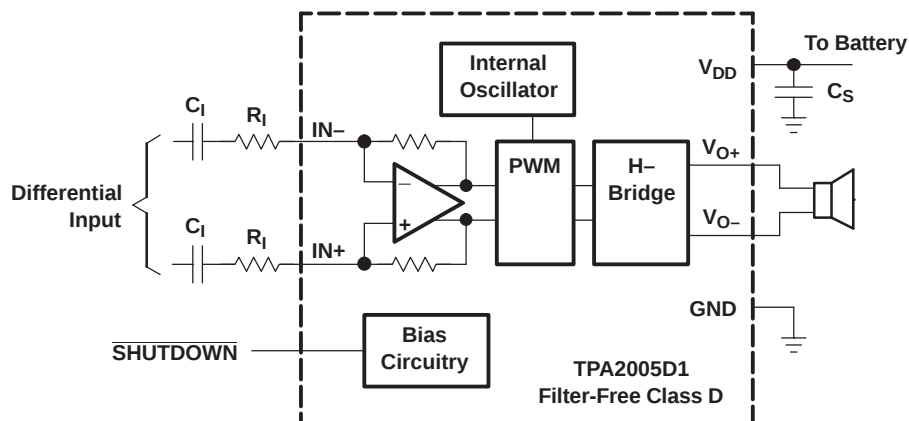


Figure 33. TPA2005D1 Application Schematic With Differential Input and Input Capacitors

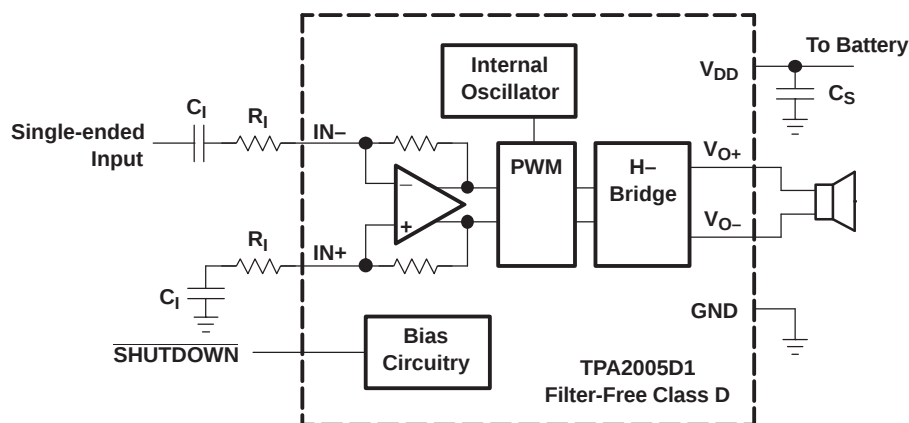


Figure 34. TPA2005D1 Application Schematic With Single-Ended Input

Input Resistors (R_I)

The input resistors (R_I) set the gain of the amplifier according to equation [Equation 1](#).

$$\text{Gain} = 2 \times \frac{150 \text{ k}\Omega}{R_I} \quad (1)$$

Resistor matching is important in fully differential amplifiers. The balance of the output on the reference voltage depends on matched ratios of the resistors. CMRR, PSRR, and cancellation of the second harmonic distortion diminish if resistor mismatch occurs. Therefore, it is recommended to use 1% tolerance resistors or better to keep the performance optimized. Matching is more important than overall tolerance. Resistor arrays with 1% matching can be used with a tolerance greater than 1%.

Place the input resistors close to the TPA2005D1 to limit noise injection on the high-impedance nodes.

For optimal performance the gain should be set to 2 V/V or lower. Lower gain allows the TPA2005D1 to operate at its best, and keeps a high voltage at the input making the inputs less susceptible to noise.

Decoupling Capacitor (C_S)

The TPA2005D1 is a high-performance class-D audio amplifier that requires adequate power supply decoupling to ensure the efficiency is high and total harmonic distortion (THD) is low. For higher frequency transients, spikes, or digital hash on the line, a good low equivalent-series-resistance (ESR) ceramic capacitor, typically 1 μF , placed as close as possible to the device V_{DD} lead works best. Placing this decoupling capacitor close to the TPA2005D1 is important for the efficiency of the class-D amplifier, because any resistance or inductance in the trace between the device and the capacitor can cause a loss in efficiency. For filtering lower-frequency noise signals, a 10 μF or greater capacitor placed near the audio power amplifier would also help, but it is not required in most applications because of the high PSRR of this device.

Input Capacitors (C_I)

The TPA2005D1 does not require input coupling capacitors if the design uses a differential source that is biased from 0.5 V to $V_{DD} - 0.8 \text{ V}$ (shown in [Figure 32](#)). If the input signal is not biased within the recommended common-mode input range, if needing to use the input as a high pass filter (shown in [Figure 33](#)), or if using a single-ended source (shown in [Figure 34](#)), input coupling capacitors are required.

The input capacitors and input resistors form a high-pass filter with the corner frequency, f_c , determined in equation [Equation 2](#).

$$f_c = \frac{1}{(2\pi R_I C_I)} \quad (2)$$

The value of the input capacitor is important to consider as it directly affects the bass (low frequency) performance of the circuit. Speakers in wireless phones cannot usually respond well to low frequencies, so the corner frequency can be set to block low frequencies in this application.

Equation [Equation 3](#) is reconfigured to solve for the input coupling capacitance.

$$C_I = \frac{1}{(2\pi R_I f_c)} \quad (3)$$

If the corner frequency is within the audio band, the capacitors should have a tolerance of 10% or better, because any mismatch in capacitance causes an impedance mismatch at the corner frequency and below, and causes pop. Any capacitor in the audio path should have a rating of X7R or better.

For a flat low-frequency response, use large input coupling capacitors (1 μF). However, in a GSM phone the ground signal is fluctuating at 217 Hz, but the signal from the codec does not have the same 217 Hz fluctuation. The difference between the two signals is amplified, sent to the speaker, and heard as a 217 Hz hum.

SUMMING INPUT SIGNALS WITH THE TPA2005D1

Most wireless phones or PDAs need to sum signals at the audio power amplifier or just have two signal sources that need separate gain. The TPA2005D1 makes it easy to sum signals or use separate signal sources with different gains. Many phones now use the same speaker for the earpiece and ringer, where the wireless phone would require a much lower gain for the phone earpiece than for the ringer. PDAs and phones that have stereo headphones require summing of the right and left channels to output the stereo signal to the mono speaker.

Summing Two Differential Input Signals

Two extra resistors are needed for summing differential signals (a total of 5 components). The gain for each input source can be set independently (see equations [Equation 4](#) and [Equation 5](#), and [Figure 35](#)).

$$\text{Gain 1} = \frac{V_O}{V_{I1}} = 2 \times \frac{150 \text{ k}\Omega}{R_{I1}} \left(\frac{\text{V}}{\text{V}} \right) \quad (4)$$

$$\text{Gain 2} = \frac{V_O}{V_{I2}} = 2 \times \frac{150 \text{ k}\Omega}{R_{I2}} \left(\frac{\text{V}}{\text{V}} \right) \quad (5)$$

If summing left and right inputs with a gain of 1 V/V, use $R_{I1} = R_{I2} = 300 \text{ k}\Omega$.

If summing a ring tone and a phone signal, set the ring-tone gain to Gain 2 = 2 V/V, and the phone gain to gain 1 = 0.1 V/V. The resistor values would be. . .

- $R_{I1} = 3 \text{ M}\Omega$, and $R_{I2} = 150 \text{ k}\Omega$.

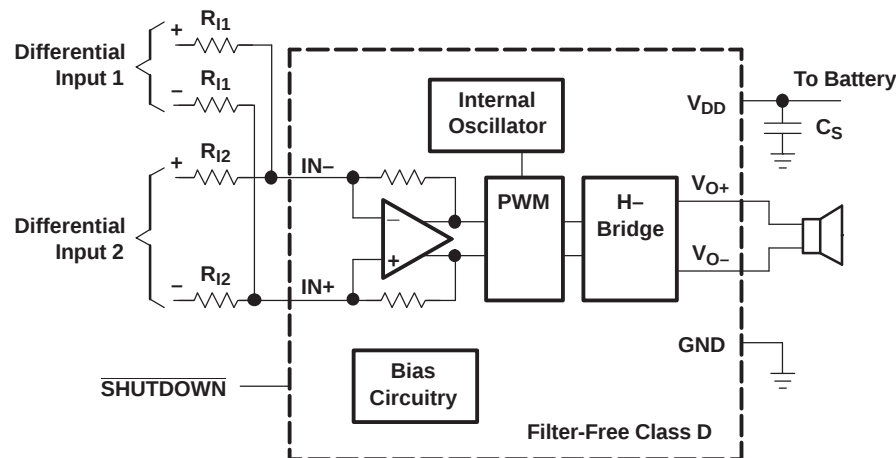


Figure 35. Application Schematic With TPA2005D1 Summing Two Differential Inputs

Summing a Differential Input Signal and a Single-Ended Input Signal

[Figure 36](#) shows how to sum a differential input signal and a single-ended input signal. Ground noise can couple in through IN+ with this method. It is better to use differential inputs. The corner frequency of the single-ended input is set by C_{I2} , shown in [Equation 8](#). To assure that each input is balanced, the single-ended input must be driven by a low-impedance source even if the input is not in use.

$$\text{Gain 1} = \frac{V_O}{V_{I1}} = 2 \times \frac{150 \text{ k}\Omega}{R_{I1}} \left(\frac{\text{V}}{\text{V}} \right) \quad (6)$$

$$\text{Gain 2} = \frac{V_O}{V_{I2}} = 2 \times \frac{150 \text{ k}\Omega}{R_{I2}} \left(\frac{\text{V}}{\text{V}} \right) \quad (7)$$

$$C_{I2} = \frac{1}{(2\pi R_{I2} f_{c2})} \quad (8)$$

If summing a ring tone and a phone signal, the phone signal should use a differential input signal while the ring tone might be limited to a single-ended signal. Phone gain is set at gain 1 = 0.1 V/V, and the ring-tone gain is set to gain 2 = 2 V/V, the resistor values would be...

- $R_{I1} = 3 \text{ M}\Omega$, and $R_{I2} = 150 \text{ k}\Omega$.

The high pass corner frequency of the single-ended input is set by C_{I2} . If the desired corner frequency is less than 20 Hz.

$$C_{I2} > \frac{1}{(2\pi \cdot 150\text{k}\Omega \cdot 20\text{Hz})} \quad (9)$$

$$C_{I2} > 53\text{pF} \quad (10)$$

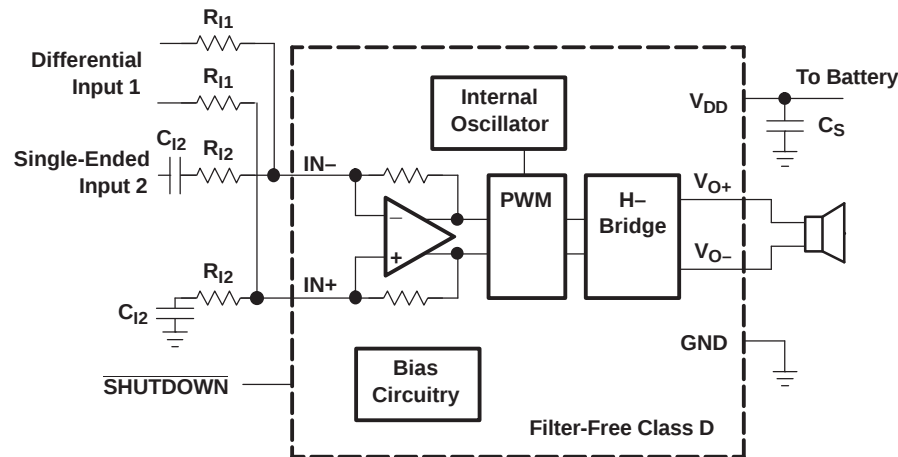


Figure 36. Application Schematic With TPA2005D1 Summing Differential Input and Single-Ended Input Signals

Summing Two Single-Ended Input Signals

Four resistors and three capacitors are needed for summing single-ended input signals. The gain and corner frequencies (f_{c1} and f_{c2}) for each input source can be set independently (see equations [Equation 11](#) through [Equation 14](#), and [Figure 37](#)). Resistor, R_P , and capacitor, C_P , are needed on the $IN+$ terminal to match the impedance on the $IN-$ terminal. The single-ended inputs must be driven by low impedance sources even if one of the inputs is not outputting an ac signal.

$$\text{Gain 1} = \frac{V_O}{V_{I1}} = 2 \times \frac{150 \text{ k}\Omega}{R_{I1}} \left(\frac{\text{V}}{\text{V}} \right) \quad (11)$$

$$\text{Gain 2} = \frac{V_O}{V_{I2}} = 2 \times \frac{150 \text{ k}\Omega}{R_{I2}} \left(\frac{\text{V}}{\text{V}} \right) \quad (12)$$

$$C_{I1} = \frac{1}{(2\pi R_{I1} f_{c1})} \quad (13)$$

$$C_{I2} = \frac{1}{(2\pi R_{I2} f_{c2})} \quad (14)$$

$$C_P = C_{I1} + C_{I2} \quad (15)$$

$$R_P = \frac{R_{I1} \times R_{I2}}{(R_{I1} + R_{I2})} \quad (16)$$

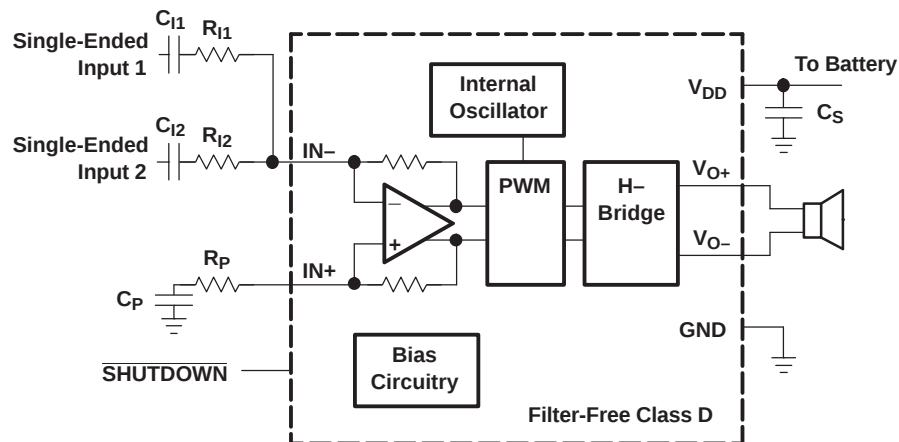


Figure 37. Application Schematic With TPA2005D1 Summing Two Single-Ended Inputs

EFFICIENCY AND THERMAL INFORMATION

The maximum ambient temperature depends on the heat-sinking ability of the PCB system. The derating factor for the 2,5-mm x 2,5-mm MicroStar Junior package is shown in the dissipation rating table. Converting this to θ_{JA} :

$$\theta_{JA} = \frac{1}{\text{Derating Factor}} = \frac{1}{0.016} = 62.5^\circ\text{C/W} \quad (17)$$

Given θ_{JA} of 62.5°C/W , the maximum allowable junction temperature of 150°C , and the maximum internal dissipation of 0.2 W (worst case 5-V supply), the maximum ambient temperature can be calculated with equation [Equation 18](#).

$$T_{A\text{Max}} = T_{J\text{Max}} - \theta_{JA} P_{D\text{max}} = 150 - 62.5 (0.2) = 137.5^\circ\text{C} \quad (18)$$

Equation [Equation 18](#) shows that the calculated maximum ambient temperature is 137.5°C at maximum power dissipation with a 5-V supply; however, the maximum ambient temperature of the package is limited to 85°C . Because of the efficiency of the TPA2005D1, it can be operated under all conditions to an ambient temperature of 85°C . The TPA2005D1 is designed with thermal protection that turns the device off when the junction temperature surpasses 150°C to prevent damage to the IC. Also, using speakers more resistive than 8- Ω dramatically increases the thermal performance by reducing the output current and increasing the efficiency of the amplifier.

BOARD LAYOUT

Component Location

Place all the external components close to the TPA2005D1. The input resistors need to be close to the TPA2005D1 input pins so noise does not couple on the high impedance nodes between the input resistors and the input amplifier of the TPA2005D1. Placing the decoupling capacitor, C_S , close to the TPA2005D1 is important for the efficiency of the class-D amplifier. Any resistance or inductance in the trace between the device and the capacitor can cause a loss in efficiency.

Trace Width

Make the high current traces going to pins VDD, GND, V_{O+} and V_{O-} of the TPA2005D1 have a minimum width of 0,7 mm. If these traces are too thin, the TPA2005D1's performance and output power will decrease. The input traces do not need to be wide, but do need to run side-by-side to enable common-mode noise cancellation.

MicroStar Junior™ BGA Layout

Use the following MicroStar Junior BGA ball diameters:

- 0,25 mm diameter solder mask
- 0,28 mm diameter solder paste mask/stencil
- 0,38 mm diameter copper trace

Figure 38 shows how to lay out a board for the TPA2005D1 MicroStar Junior BGA.

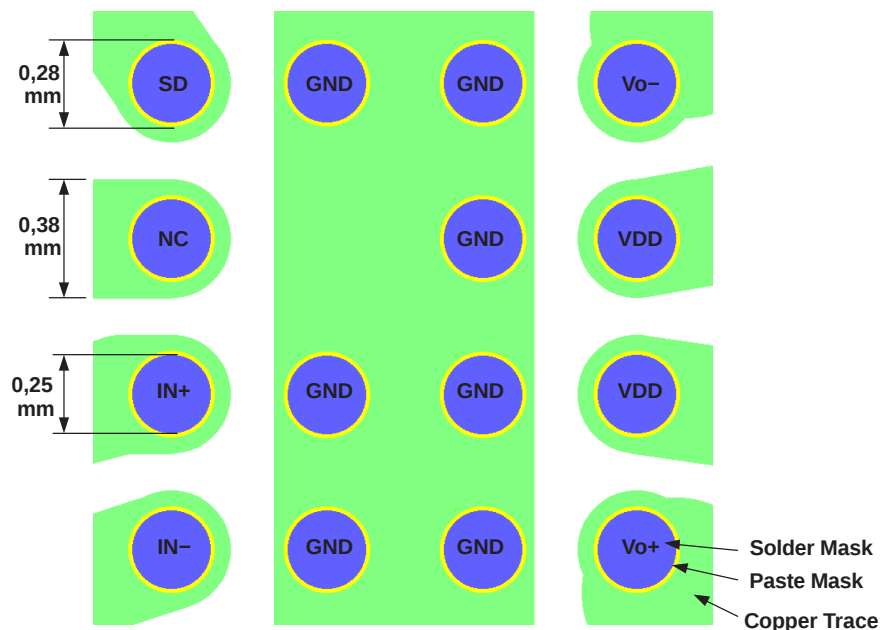


Figure 38. TPA2005D1 MicroStar Junior BGA Board Layout (Top View)

ELIMINATING THE OUTPUT FILTER WITH THE TPA2005D1

This section focuses on why the user can eliminate the output filter with the TPA2005D1.

Effect on Audio

The class-D amplifier outputs a pulse-width modulated (PWM) square wave, which is the sum of the switching waveform and the amplified input audio signal. The human ear acts as a band-pass filter such that only the frequencies between approximately 20 Hz and 20 kHz are passed. The switching frequency components are much greater than 20 kHz, so the only signal heard is the amplified input audio signal.

Traditional Class-D Modulation Scheme

The traditional class-D modulation scheme, which is used in the TPA005Dxx family, has a differential output where each output is 180 degrees out of phase and changes from ground to the supply voltage, V_{DD} . Therefore, the differential pre-filtered output varies between positive and negative V_{DD} , where filtered 50% duty cycle yields 0 volts across the load. The traditional class-D modulation scheme with voltage and current waveforms is shown in Figure 39. Note that even at an average of 0 volts across the load (50% duty cycle), the current to the load is high causing a high loss and thus causing a high supply current.

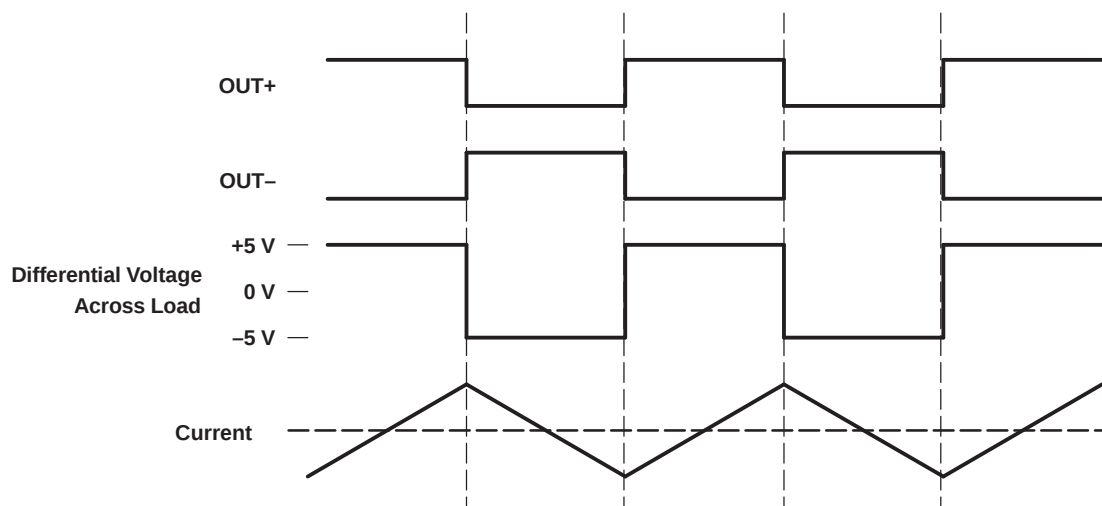


Figure 39. Traditional Class-D Modulation Scheme's Output Voltage and Current Waveforms Into an Inductive Load With no Input

TPA2005D1 Modulation Scheme

The TPA2005D1 uses a modulation scheme that still has each output switching from 0 to the supply voltage. However, OUT+ and OUT- are now in phase with each other with no input. The duty cycle of OUT+ is greater than 50% and OUT- is less than 50% for positive voltages. The duty cycle of OUT+ is less than 50% and OUT- is greater than 50% for negative voltages. The voltage across the load sits at 0 volts throughout most of the switching period greatly reducing the switching current, which reduces any I^2R losses in the load.

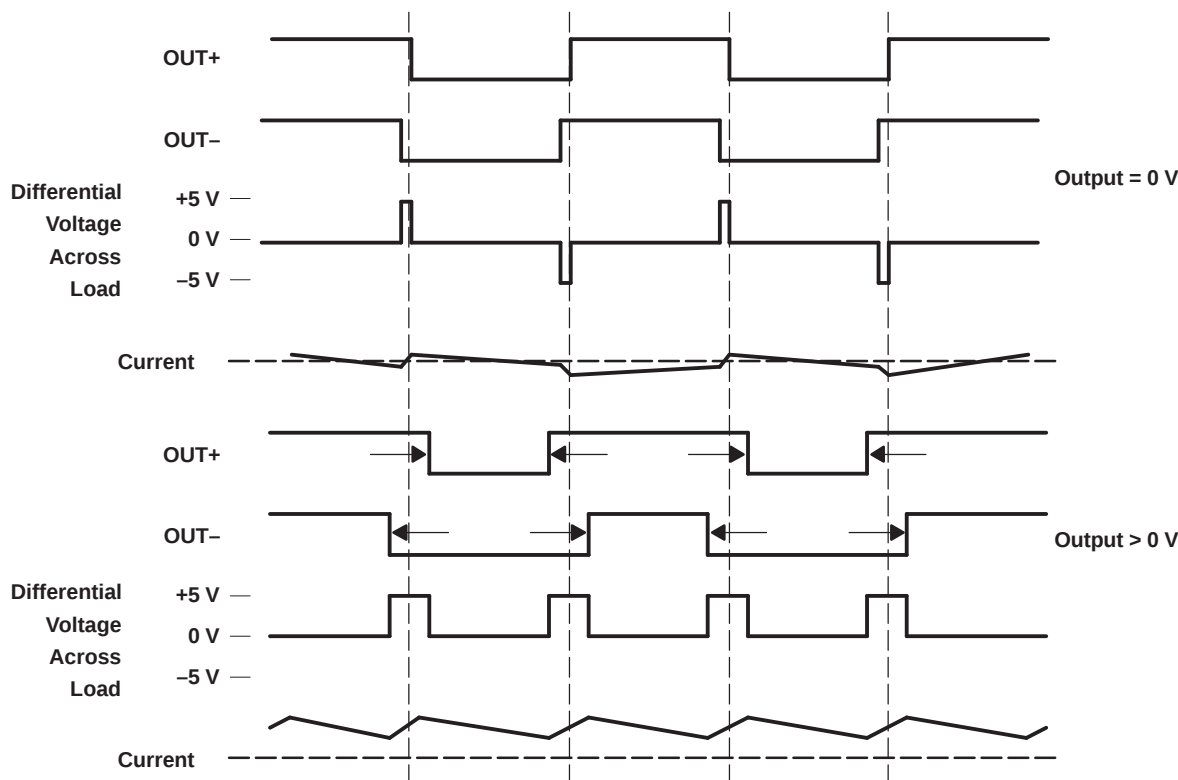


Figure 40. The TPA2005D1 Output Voltage and Current Waveforms Into an Inductive Load

Efficiency: Why You Must Use a Filter With the Traditional Class-D Modulation Scheme

The main reason that the traditional class-D amplifier needs an output filter is that the switching waveform results in maximum current flow. This causes more loss in the load, which causes lower efficiency. The ripple current is large for the traditional modulation scheme because the ripple current is proportional to voltage multiplied by the time at that voltage. The differential voltage swing is $2 \times V_{DD}$ and the time at each voltage is half the period for the traditional modulation scheme. An ideal LC filter is needed to store the ripple current from each half cycle for the next half cycle, while any resistance causes power dissipation. The speaker is both resistive and reactive, whereas an LC filter is almost purely reactive.

The TPA2005D1 modulation scheme has little loss in the load without a filter because the pulses are short and the change in voltage is V_{DD} instead of $2 \times V_{DD}$. As the output power increases, the pulses widen making the ripple current larger. Ripple current could be filtered with an LC filter for increased efficiency, but for most applications the filter is not needed.

An LC filter with a cutoff frequency less than the class-D switching frequency allows the switching current to flow through the filter instead of the load. The filter has less resistance than the speaker that results in less power dissipated, which increases efficiency.

Effects of Applying a Square Wave Into a Speaker

If the amplitude of a square wave is high enough and the frequency of the square wave is within the bandwidth of the speaker, a square wave could cause the voice coil to jump out of the air gap and/or scar the voice coil. A 250-kHz switching frequency, however, is not significant because the speaker cone movement is proportional to $1/f^2$ for frequencies beyond the audio band. Therefore, the amount of cone movement at the switching frequency is small. However, damage could occur to the speaker if the voice coil is not designed to handle the additional power. To size the speaker for added power, the ripple current dissipated in the load needs to be calculated by subtracting the theoretical supplied power, $P_{SUP, THEORETICAL}$, from the actual supply power, P_{SUP} , at maximum output power, P_{OUT} . The switching power dissipated in the speaker is the inverse of the measured efficiency, $\eta_{MEASURED}$, minus the theoretical efficiency, $\eta_{THEORETICAL}$.

$$P_{\text{SPKR}} = P_{\text{SUP}} - P_{\text{SUP THEORETICAL}} \quad (\text{at max output power}) \quad (19)$$

$$P_{\text{SPKR}} = \frac{P_{\text{SUP}}}{P_{\text{OUT}}} - \frac{P_{\text{SUP THEORETICAL}}}{P_{\text{OUT}}} \quad (\text{at max output power}) \quad (20)$$

$$P_{\text{SPKR}} = P_{\text{OUT}} \left(\frac{1}{\eta_{\text{MEASURED}}} - \frac{1}{\eta_{\text{THEORETICAL}}} \right) \quad (\text{at max output power}) \quad (21)$$

$$\eta_{\text{THEORETICAL}} = \frac{R_L}{R_L + 2r_{\text{DS(on)}}} \quad (\text{at max output power}) \quad (22)$$

The maximum efficiency of the TPA2005D1 with a 3.6 V supply and an 8-Ω load is 86% from equation Equation 22. Using equation Equation 21 with the efficiency at maximum power (84%), we see that there is an additional 17 mW dissipated in the speaker. The added power dissipated in the speaker is not an issue as long as it is taken into account when choosing the speaker.

When to Use an Output Filter

Design the TPA2005D1 without an output filter if the traces from amplifier to speaker are short. The TPA2005D1 passed FCC and CE radiated emissions with no shielding with speaker trace wires 100 mm long or less. Wireless handsets and PDAs are great applications for class-D without a filter.

A ferrite bead filter can often be used if the design is failing radiated emissions without an LC filter, and the frequency sensitive circuit is greater than 1 MHz. This is good for circuits that just have to pass FCC and CE because FCC and CE only test radiated emissions greater than 30 MHz. If choosing a ferrite bead, choose one with high impedance at high frequencies, but low impedance at low frequencies.

Use an LC output filter if there are low frequency (< 1 MHz) EMI sensitive circuits and/or there are long leads from amplifier to speaker.

Figure 41 and Figure 42 show typical ferrite bead and LC output filters.

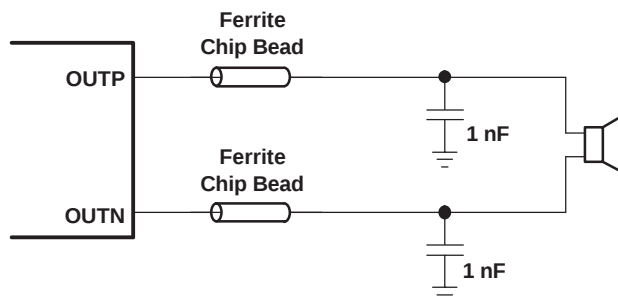


Figure 41. Typical Ferrite Chip Bead Filter (Chip bead example: NEC/Tokin: N2012ZPS121)

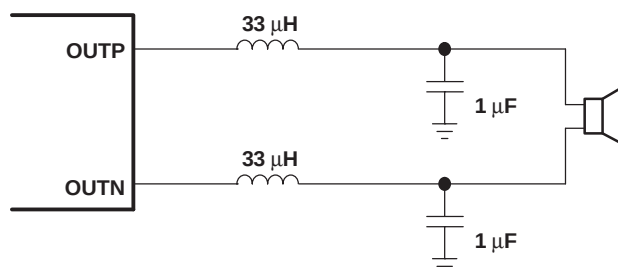


Figure 42. Typical LC Output Filter, Cutoff Frequency of 27 kHz

PACKAGING INFORMATION

Orderable Device	Status (1)	Package Type	Package Drawing	Pins	Package Qty	Eco Plan (2)	Lead/Ball Finish	MSL Peak Temp (3)	Op Temp (°C)	Top-Side Markings (4)	Samples
TPA2005D1DGN	ACTIVE	MSOP- PowerPAD	DGN	8	80	Green (RoHS & no Sb/Br)	CU NIPDAUAG	Level-1-260C-UNLIM	-40 to 85	BAL	Samples
TPA2005D1DGNG4	ACTIVE	MSOP- PowerPAD	DGN	8	80	Green (RoHS & no Sb/Br)	CU NIPDAUAG	Level-1-260C-UNLIM	-40 to 85	BAL	Samples
TPA2005D1DGNR	ACTIVE	MSOP- PowerPAD	DGN	8	2500	Green (RoHS & no Sb/Br)	CU NIPDAUAG	Level-1-260C-UNLIM	-40 to 85	BAL	Samples
TPA2005D1DGNRG4	ACTIVE	MSOP- PowerPAD	DGN	8	2500	Green (RoHS & no Sb/Br)	CU NIPDAUAG	Level-1-260C-UNLIM	-40 to 85	BAL	Samples
TPA2005D1DRBR	ACTIVE	SON	DRB	8	3000	Green (RoHS & no Sb/Br)	CU NIPDAU	Level-2-260C-1 YEAR	-40 to 85	BIQ	Samples
TPA2005D1DRBRG4	ACTIVE	SON	DRB	8	3000	Green (RoHS & no Sb/Br)	CU NIPDAU	Level-2-260C-1 YEAR	-40 to 85	BIQ	Samples
TPA2005D1GQYR	ACTIVE	BGA MICROSTAR JUNIOR	GQY	15	2500	TBD	SNPB	Level-2-235C-1 YEAR	-40 to 85	PB051	Samples
TPA2005D1ZQYR	ACTIVE	BGA MICROSTAR JUNIOR	ZQY	15	2500	Green (RoHS & no Sb/Br)	SNAGCU	Level-2-260C-1 YEAR	-40 to 85	AAFI	Samples
TPA2005D1ZQYRG1	ACTIVE	BGA MICROSTAR JUNIOR	ZQY	15	2500	Green (RoHS & no Sb/Br)	SNAGCU	Level-2-260C-1 YEAR	-40 to 85	AAFI	Samples

(1) The marketing status values are defined as follows:

ACTIVE: Product device recommended for new designs.

LIFEBUY: TI has announced that the device will be discontinued, and a lifetime-buy period is in effect.

NRND: Not recommended for new designs. Device is in production to support existing customers, but TI does not recommend using this part in a new design.

PREVIEW: Device has been announced but is not in production. Samples may or may not be available.

OBSOLETE: TI has discontinued the production of the device.

(2) Eco Plan - The planned eco-friendly classification: Pb-Free (RoHS), Pb-Free (RoHS Exempt), or Green (RoHS & no Sb/Br) - please check <http://www.ti.com/productcontent> for the latest availability information and additional product content details.

TBD: The Pb-Free/Green conversion plan has not been defined.

Pb-Free (RoHS): TI's terms "Lead-Free" or "Pb-Free" mean semiconductor products that are compatible with the current RoHS requirements for all 6 substances, including the requirement that lead not exceed 0.1% by weight in homogeneous materials. Where designed to be soldered at high temperatures, TI Pb-Free products are suitable for use in specified lead-free processes.

Pb-Free (RoHS Exempt): This component has a RoHS exemption for either 1) lead-based flip-chip solder bumps used between the die and package, or 2) lead-based die adhesive used between the die and leadframe. The component is otherwise considered Pb-Free (RoHS compatible) as defined above.

Green (RoHS & no Sb/Br): TI defines "Green" to mean Pb-Free (RoHS compatible), and free of Bromine (Br) and Antimony (Sb) based flame retardants (Br or Sb do not exceed 0.1% by weight in homogeneous material)

⁽³⁾ MSL, Peak Temp. -- The Moisture Sensitivity Level rating according to the JEDEC industry standard classifications, and peak solder temperature.

⁽⁴⁾ Only one of markings shown within the brackets will appear on the physical device.

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OTHER QUALIFIED VERSIONS OF TPA2005D1 :

- Automotive: [TPA2005D1-Q1](#)

NOTE: Qualified Version Definitions:

- Automotive - Q100 devices qualified for high-reliability automotive applications targeting zero defects

TAPE AND REEL INFORMATION
REEL DIMENSIONS

TAPE DIMENSIONS


A0	Dimension designed to accommodate the component width
B0	Dimension designed to accommodate the component length
K0	Dimension designed to accommodate the component thickness
W	Overall width of the carrier tape
P1	Pitch between successive cavity centers

TAPE AND REEL INFORMATION

*All dimensions are nominal

Device	Package Type	Package Drawing	Pins	SPQ	Reel Diameter (mm)	Reel Width W1 (mm)	A0 (mm)	B0 (mm)	K0 (mm)	P1 (mm)	W (mm)	Pin1 Quadrant
TPA2005D1DGNR	MSOP-Power PAD	DGN	8	2500	330.0	12.4	5.3	3.4	1.4	8.0	12.0	Q1
TPA2005D1DRBR	SON	DRB	8	3000	330.0	12.4	3.3	3.3	1.1	8.0	12.0	Q2
TPA2005D1DRBR	SON	DRB	8	3000	330.0	12.4	3.3	3.3	1.1	8.0	12.0	Q2
TPA2005D1ZQYR	BGA MICROSTAR JUNIOR	ZQY	15	2500	330.0	8.4	2.8	2.8	1.25	4.0	8.0	Q1

TAPE AND REEL BOX DIMENSIONS

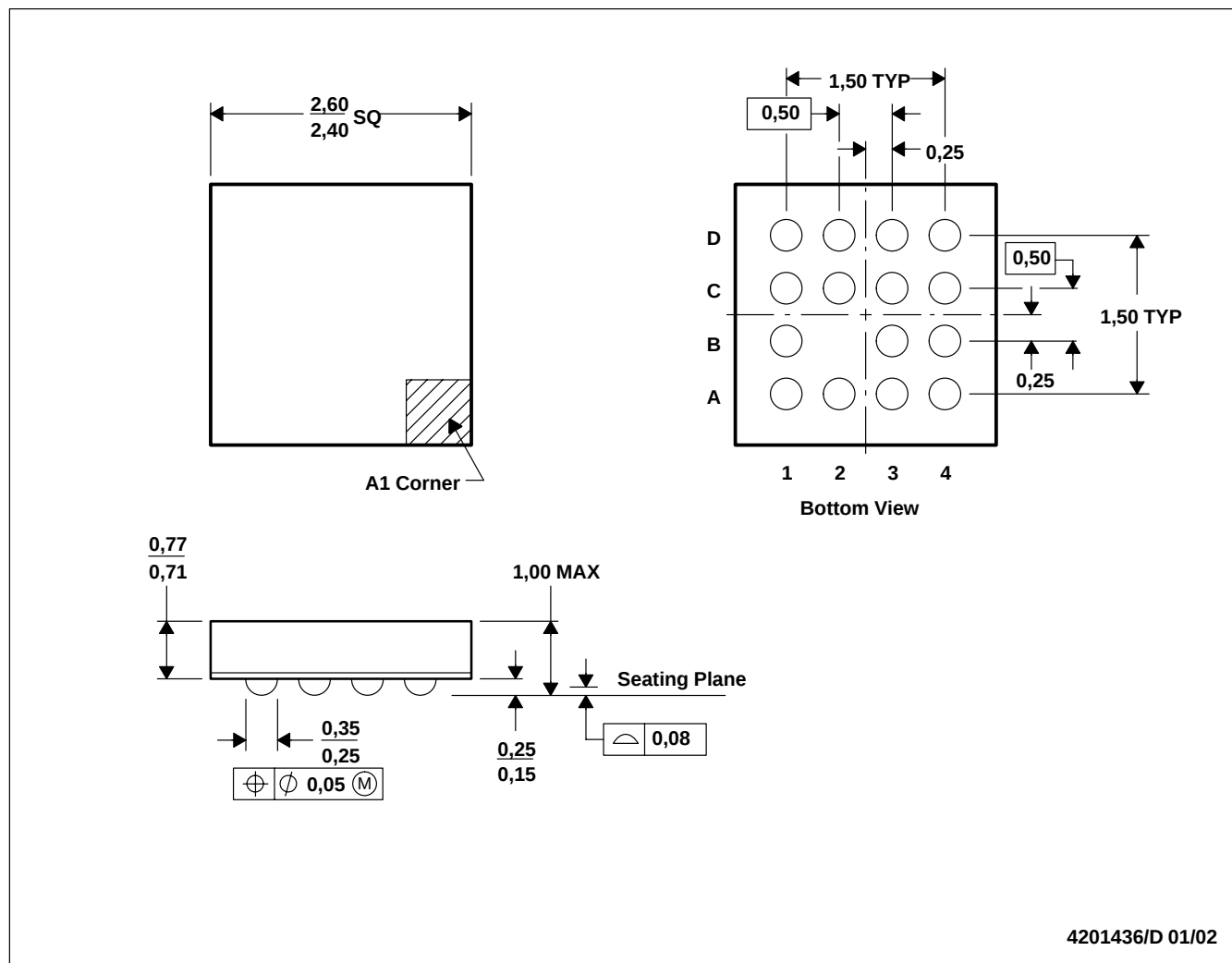


*All dimensions are nominal

Device	Package Type	Package Drawing	Pins	SPQ	Length (mm)	Width (mm)	Height (mm)
TPA2005D1DGNR	MSOP-PowerPAD	DGN	8	2500	364.0	364.0	27.0
TPA2005D1DRBR	SON	DRB	8	3000	367.0	367.0	35.0
TPA2005D1DRBR	SON	DRB	8	3000	367.0	367.0	35.0
TPA2005D1ZQYR	BGA MICROSTAR JUNIOR	ZQY	15	2500	338.1	338.1	20.6

GQY (S-PBGA-N15)

PLASTIC BALL GRID ARRAY



- NOTES: A. All linear dimensions are in millimeters.
 B. This drawing is subject to change without notice.
 C. MicroStar Junior™ configuration
 D. Falls within JEDEC MO-225

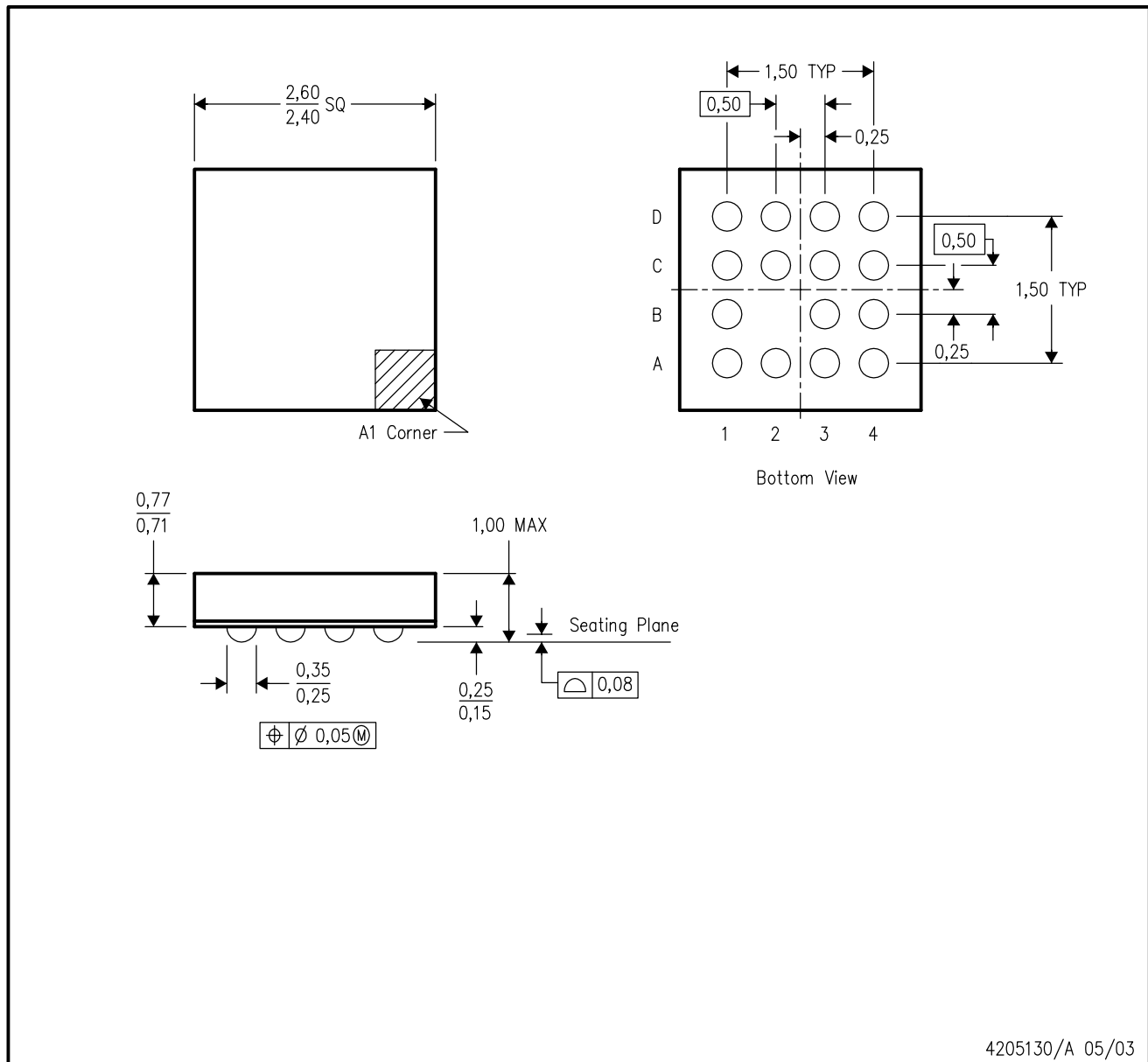
MicroStar Junior is a trademark of Texas Instruments.



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ZQY (S-PBGA-N15)

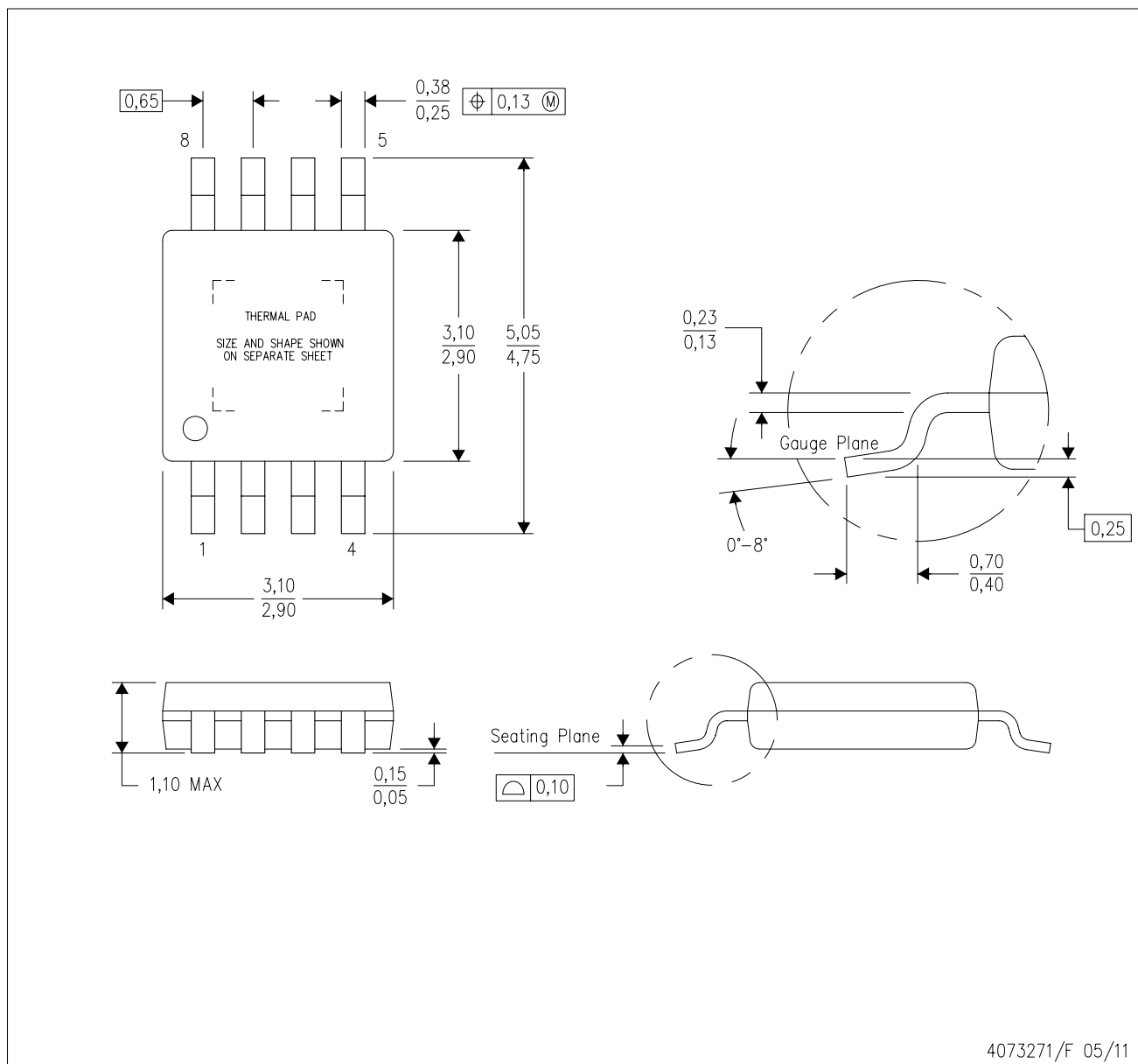
PLASTIC BALL GRID ARRAY



- NOTES:
- A. All linear dimensions are in millimeters.
 - B. This drawing is subject to change without notice.
 - C. MicroStar Junior configuration
 - D. Falls within JEDEC MO-225
 - E. This package is lead-free.

DGN (S-PDSO-G8)

PowerPAD™ PLASTIC SMALL OUTLINE



- NOTES:
- All linear dimensions are in millimeters.
 - This drawing is subject to change without notice.
 - Body dimensions do not include mold flash or protrusion.
 - This package is designed to be soldered to a thermal pad on the board. Refer to Technical Brief, PowerPad Thermally Enhanced Package, Texas Instruments Literature No. SLMA002 for information regarding recommended board layout. This document is available at www.ti.com <<http://www.ti.com>>.
 - See the additional figure in the Product Data Sheet for details regarding the exposed thermal pad features and dimensions.
 - Falls within JEDEC MO-187 variation AA-T

PowerPAD is a trademark of Texas Instruments.

DGN (S-PDSO-G8)

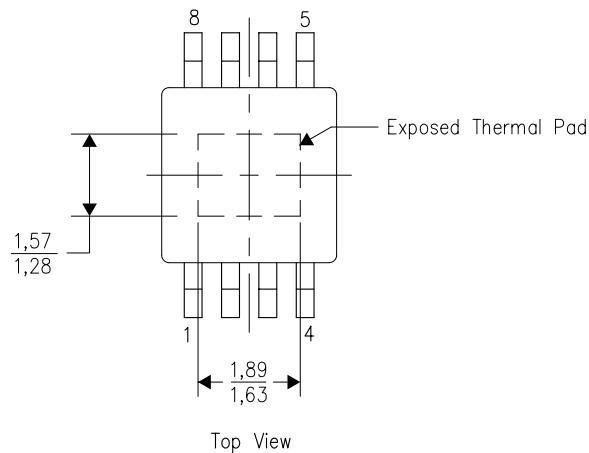
PowerPAD™ PLASTIC SMALL OUTLINE

THERMAL INFORMATION

This PowerPAD™ package incorporates an exposed thermal pad that is designed to be attached to a printed circuit board (PCB). The thermal pad must be soldered directly to the PCB. After soldering, the PCB can be used as a heatsink. In addition, through the use of thermal vias, the thermal pad can be attached directly to the appropriate copper plane shown in the electrical schematic for the device, or alternatively, can be attached to a special heatsink structure designed into the PCB. This design optimizes the heat transfer from the integrated circuit (IC).

For additional information on the PowerPAD package and how to take advantage of its heat dissipating abilities, refer to Technical Brief, PowerPAD Thermally Enhanced Package, Texas Instruments Literature No. SLMA002 and Application Brief, PowerPAD Made Easy, Texas Instruments Literature No. SLMA004. Both documents are available at www.ti.com.

The exposed thermal pad dimensions for this package are shown in the following illustration.



Exposed Thermal Pad Dimensions

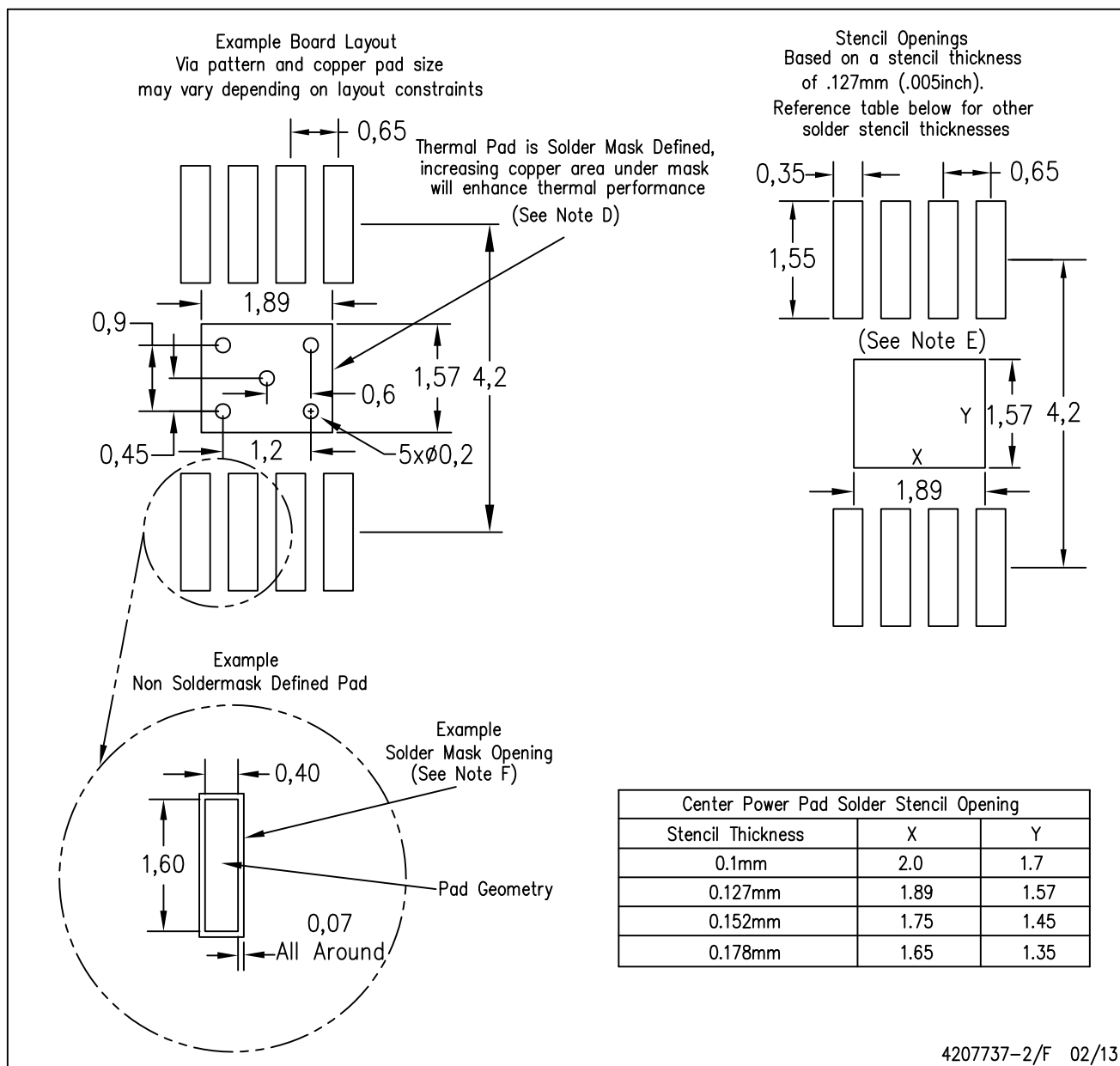
4206323-2/1 12/11

NOTE: All linear dimensions are in millimeters

PowerPAD is a trademark of Texas Instruments

DGN (R-PDSO-G8)

PowerPAD™ PLASTIC SMALL OUTLINE



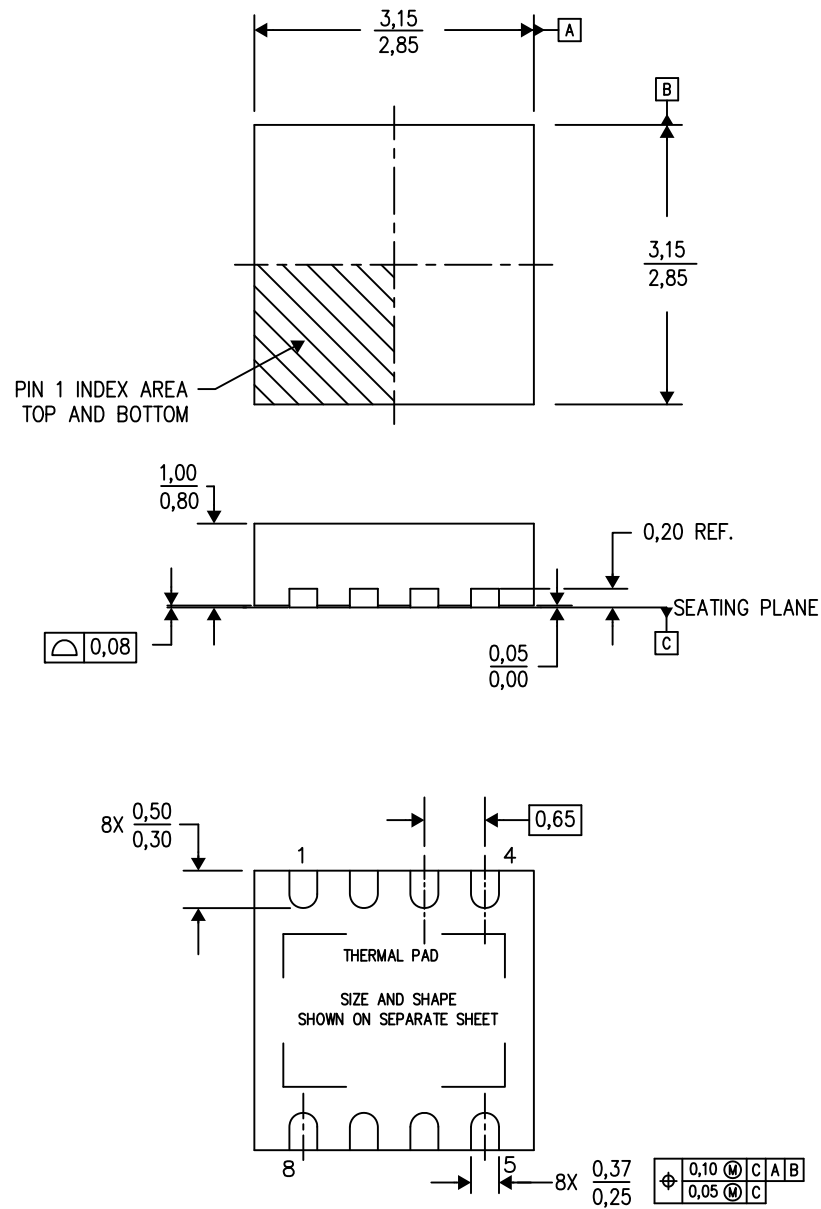
4207737-2/F 02/13

- NOTES:
- All linear dimensions are in millimeters.
 - This drawing is subject to change without notice.
 - Customers should place a note on the circuit board fabrication drawing not to alter the center solder mask defined pad.
 - This package is designed to be soldered to a thermal pad on the board. Refer to Technical Brief, PowerPad Thermally Enhanced Package, Texas Instruments Literature No. SLMA002, SLMA004, and also the Product Data Sheets for specific thermal information, via requirements, and recommended board layout. These documents are available at www.ti.com <<http://www.ti.com>>.
 - Laser cutting apertures with trapezoidal walls and also rounding corners will offer better paste release. Customers should contact their board assembly site for stencil design recommendations. Example stencil design based on a 50% volumetric metal load solder paste. Refer to IPC-7525 for other stencil recommendations.
 - Customers should contact their board fabrication site for solder mask tolerances between and around signal pads.

PowerPAD is a trademark of Texas Instruments

DRB (S-PVSON-N8)

PLASTIC SMALL OUTLINE NO-LEAD



Bottom View

4203482-2/K 06/12

- NOTES:
- All linear dimensions are in millimeters. Dimensioning and tolerancing per ASME Y14.5M-1994.
 - This drawing is subject to change without notice.
 - Small Outline No-Lead (SON) package configuration.
 - The package thermal pad must be soldered to the board for thermal and mechanical performance.
 - See the additional figure in the Product Data Sheet for details regarding the exposed thermal pad features and dimensions.

DRB (S-PVSON-N8)

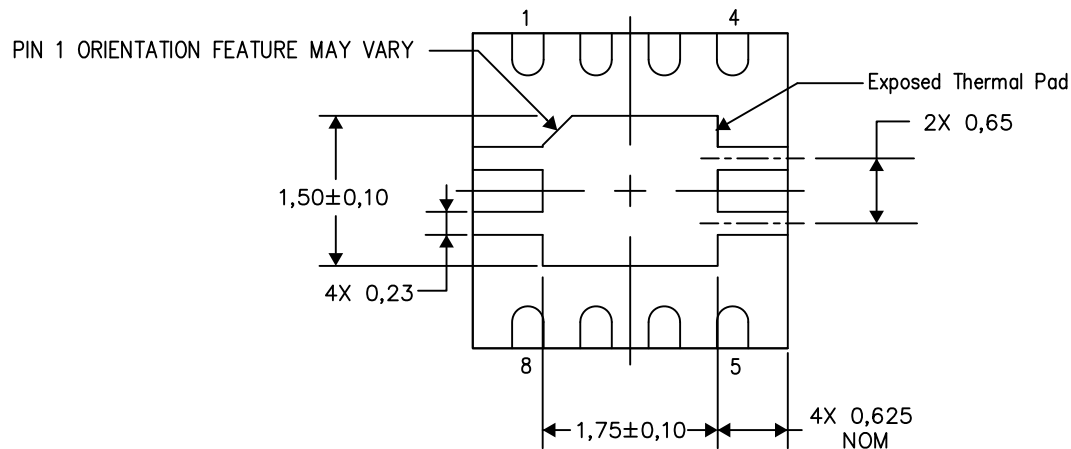
PLASTIC SMALL OUTLINE NO-LEAD

THERMAL INFORMATION

This package incorporates an exposed thermal pad that is designed to be attached directly to an external heatsink. The thermal pad must be soldered directly to the printed circuit board (PCB). After soldering, the PCB can be used as a heatsink. In addition, through the use of thermal vias, the thermal pad can be attached directly to the appropriate copper plane shown in the electrical schematic for the device, or alternatively, can be attached to a special heatsink structure designed into the PCB. This design optimizes the heat transfer from the integrated circuit (IC).

For information on the Quad Flatpack No-Lead (QFN) package and its advantages, refer to Application Report, QFN/SON PCB Attachment, Texas Instruments Literature No. SLUA271. This document is available at www.ti.com.

The exposed thermal pad dimensions for this package are shown in the following illustration.



Bottom View

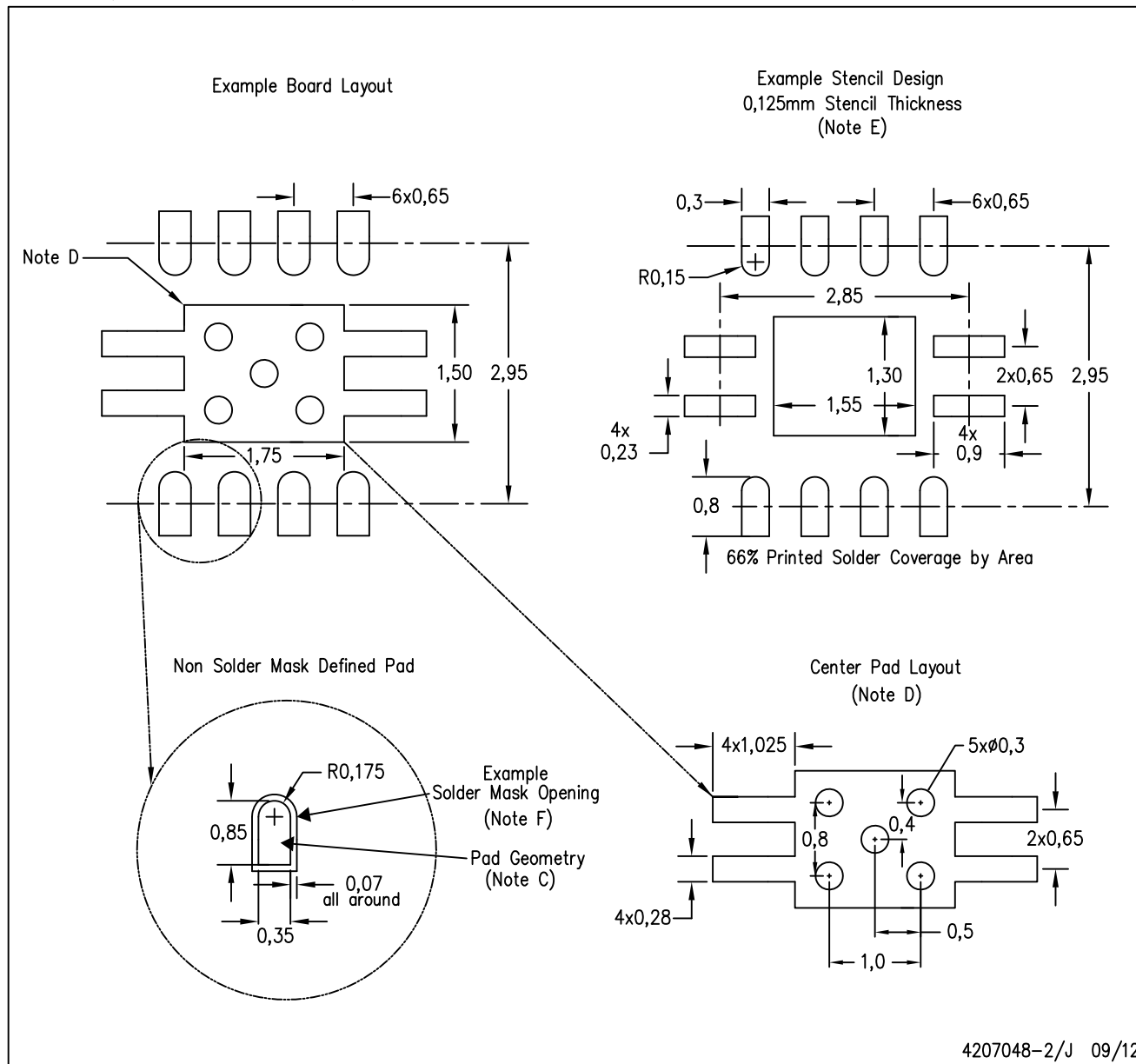
Exposed Thermal Pad Dimensions

4206340-2/N 09/12

NOTE: All linear dimensions are in millimeters

DRB (S-PVSON-N8)

PLASTIC SMALL OUTLINE NO-LEAD



- NOTES:
- All linear dimensions are in millimeters.
 - This drawing is subject to change without notice.
 - Publication IPC-7351 is recommended for alternate designs.
 - This package is designed to be soldered to a thermal pad on the board. Refer to Application Note, QFN Packages, Texas Instruments Literature No. SLUA271, and also the Product Data Sheets for specific thermal information, via requirements, and recommended board layout. These documents are available at www.ti.com <<http://www.ti.com>>.
 - Laser cutting apertures with trapezoidal walls and also rounding corners will offer better paste release. Customers should contact their board assembly site for stencil design recommendations. Refer to IPC 7525 for stencil design considerations.
 - Customers should contact their board fabrication site for solder mask tolerances.

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