

LM2586 4V 至 40V、3A 升压宽 V_{IN} 反激式稳压器

1 特性

- 无需外部组件
- 标准电感器和变压器系列
- NPN 输出开关电流为 3A，可切断 65V 电压
- 宽输入电压范围：4V 至 40V
- 可调开关频率：100kHz 至 200kHz
- 外部关断功能
- 关断时消耗电流小于 60 μ A
- 频率同步
- 可改进瞬态响应、线路调节和电流限制的电流模式操作
- 内部软启动功能可降低启动过程中的浪涌电流
- 通过电流限制、欠压锁定和热关断为输出晶体管提供保护
- 不同线路和负载条件下的最高系统输出电压容差为 $\pm 4\%$
- 使用 LM2586 并借助 **WEBENCH® 电源设计器** 创建定制设计方案

2 典型应用

- 反激式稳压器
- 正向转换器
- 多输出稳压器
- 简单升压稳压器

3 说明

LM2586 系列稳压器是专为反激式、升压和正向转换器应用而设计的单片集成电路。该器件提供 4 种不同的输出电压版本：3.3V、5V、12V 和可调节电压。

这些稳压器需要的外部组件很少，因此具有成本效益，并且易于使用。数据表中包含了典型的升压和反激式稳压器电路。另外还列出了二极管和电容器以及标准电感器和反激式变压器系列的选择指南，这些器件专用于与上述开关稳压器协同工作。

该电源开关是一款 3A NPN 器件，可切断 65V 电压。电源开关由电流和热限制电路以及欠压锁定电路进行保护。此 IC 包含可调频率振荡器，其频率可编程为高达 200kHz。该振荡器还可与其他器件同步，从而可以在同一开关频率下运行多个器件。

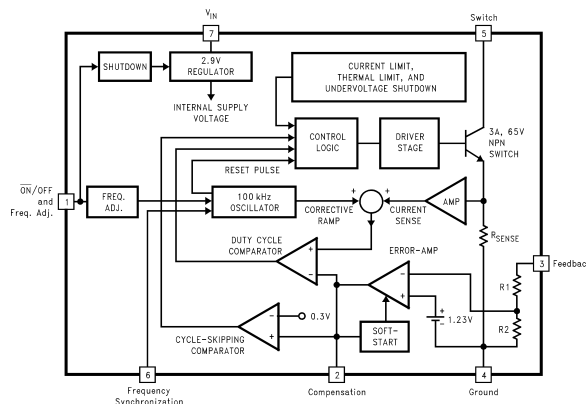
其他功能包括在启动期间降低浪涌电流的软启动模式、用于改进抑制输入电压和输出负载瞬态的电流模式控制功能，以及逐周期电流限制。该器件还具有关断引脚，因此可以从外部关闭。在额定输入电压和输出负载条件下，电源系统可确保 $\pm 4\%$ 的输出电压容差。

器件信息⁽¹⁾

器件型号	封装	封装尺寸（标称值）
LM2586	TO-220 (7)	10.1mm × 8.89mm
	DDPAK/TO-263 (7)	14.986mm × 10.16mm

(1) 如需了解所有可用封装，请参阅数据表末尾的可订购产品附录。

方框图



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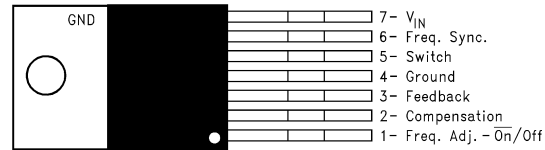
4 修订历史记录

注：之前版本的页码可能与当前版本有所不同。

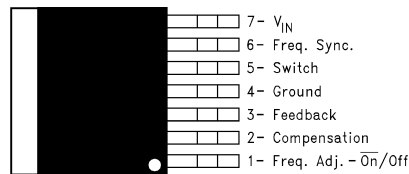
Changes from Revision D (April 2013) to Revision E		Page
•	仅有编辑更改，无技术性修订	1
Changes from Revision C (April 2013) to Revision D		Page
•	Changed layout of National Semiconductor data sheet to TI format	34

5 Pin Configurations

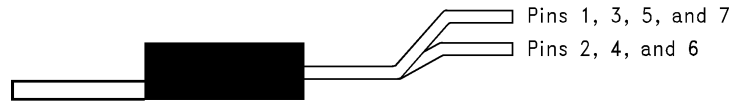
**NDZ Package
7-Pin TO-220
Top View, Bent, Staggered Leads**



**KTW Package
7-Pin DDPAK/TO-263
Top View**



**NDZ Package
7-Pin TO-220
Side View; Bent, Staggered Leads**



**KTW Package
7-Pin DDPAK/TO-263
Side View**



6 Specifications

6.1 Absolute Maximum Ratings ⁽¹⁾⁽²⁾

Input Voltage	$-0.4V \leq V_{IN} \leq 45V$
Switch Voltage	$-0.4V \leq V_{SW} \leq 65V$
Switch Current ⁽³⁾	Internally Limited
Compensation Pin Voltage	$-0.4V \leq V_{COMP} \leq 2.4V$
Feedback Pin Voltage	$-0.4V \leq V_{FB} \leq 2 V_{OUT}$
ON /OFF Pin Voltage	$-0.4V \leq V_{SH} \leq 6V$
Sync Pin Voltage	$-0.4V \leq V_{SYNC} \leq 2V$
Power Dissipation ⁽⁴⁾	Internally Limited
Storage Temperature Range	$-65^{\circ}C$ to $+150^{\circ}C$
Lead Temperature (Soldering, 10 sec.)	$260^{\circ}C$
Maximum Junction Temperature ⁽⁴⁾	$150^{\circ}C$

- (1) If Military/Aerospace specified devices are required, contact the Texas Instruments Sales Office/ Distributors for availability and specifications.
- (2) Absolute Maximum Ratings indicate limits beyond which damage to the device may occur. These ratings apply when the current is limited to less than 1.2 mA for pins 1, 2, 3, and 6. Operating ratings indicate conditions for which the device is intended to be functional, but device parameter specifications may not be ensured under these conditions. For ensured specifications and test conditions, see the [Electrical Characteristics](#).
- (3) Note that switch current and output current are not identical in a step-up regulator. Output current cannot be internally limited when the LM2586 is used as a step-up regulator. To prevent damage to the switch, the output current must be externally limited to 3A. However, output current is internally limited when the LM2586 is used as a flyback regulator (see the section for more information).
- (4) The junction temperature of the device (T_J) is a function of the ambient temperature (T_A), the junction-to-ambient thermal resistance (θ_{JA}), and the power dissipation of the device (P_D). A thermal shutdown will occur if the temperature exceeds the maximum junction temperature of the device: $P_D \times \theta_{JA} + T_{A(MAX)} \geq T_{J(MAX)}$. For a safe thermal design, check that the maximum power dissipated by the device is less than: $P_D \leq [T_{J(MAX)} - T_{A(MAX)}] / \theta_{JA}$. When calculating the maximum allowable power dissipation, derate the maximum junction temperature—this ensures a margin of safety in the thermal design.

6.2 ESD Ratings

			VALUE	UNIT
$V_{(ESD)}$	Electrostatic discharge (minimum)	Human-body model (HBM), per ANSI/ESDA/JEDEC JS-001 ⁽¹⁾ (C = 100 pF, R = 1.5 kΩ)	2000	V

- (1) JEDEC document JEP155 states that 500-V HBM allows safe manufacturing with a standard ESD control process.

6.3 Recommended Operating Ratings

Supply Voltage	$4V \leq V_{IN} \leq 40V$
Output Switch Voltage	$0V \leq V_{SW} \leq 60V$
Output Switch Current	$I_{SW} \leq 3A$
Junction Temp. Range	$-40^{\circ}C \leq T_J \leq +125^{\circ}C$

6.4 Thermal Information

THERMAL METRIC ⁽¹⁾		LM2585		UNIT
		KTW (DDPAK/TO-263)	NDZ (TO-220)	
		7 PINS	7 PINS	
$R_{\theta JA}$	Junction-to-ambient thermal resistance	56 ⁽²⁾	65 ⁽³⁾	°C/W
		35 ⁽⁴⁾	45 ⁽⁵⁾	
		26 ⁽⁶⁾	—	
$R_{\theta JC}$	Junction-to-case thermal resistance	2	2	°C/W

- (1) For more information about traditional and new thermal metrics, see the [Semiconductor and IC package thermal metrics application report](#).
- (2) Junction-to-ambient thermal resistance for the 7-lead TO-263 mounted horizontally against a PC board area of 0.136 square inches (the same size as the DDPK/TO-263 package) of 1 oz. (0.0014 in. thick) copper.
- (3) Junction-to-ambient thermal resistance (no external heat sink) for the 7-lead TO-220 package mounted vertically, with ½ inch leads in a socket, or on a PC board with minimum copper area.
- (4) Junction-to-ambient thermal resistance for the 7-lead TO-263 mounted horizontally against a PC board area of 0.4896 square inches (3.6 times the area of the DDPK/TO-263 package) of 1 oz. (0.0014 in. thick) copper.
- (5) Junction-to-ambient thermal resistance (no external heat sink) for the 7-lead TO-220 package mounted vertically, with ½ inch leads soldered to a PC board containing approximately 4 square inches of (1 oz.) copper area surrounding the leads.
- (6) Junction-to-ambient thermal resistance for the 7-lead TO-263 mounted horizontally against a PC board copper area of 1.0064 square inches (7.4 times the area of the DDPK/TO-2633 package) of 1 oz. (0.0014 in. thick) copper. Additional copper area reduces thermal resistance further.

6.5 Electrical Characteristics: 3.3 V

Specifications with standard type face are for $T_J = 25^{\circ}\text{C}$, and those in **bold type face** apply over full **Operating Temperature Range**. Unless otherwise specified, $V_{IN} = 5\text{V}$.

PARAMETER	TEST CONDITIONS	TYP	MIN	MAX	UNIT
SYSTEM PARAMETERS Test Circuit of Figure 54 ⁽¹⁾					
V_{OUT}	Output Voltage $V_{IN} = 4\text{V to }12\text{V}$ $I_{LOAD} = 0.3 \text{ to } 1.2\text{A}$	3.3	3.17/ 3.14	3.43/ 3.46	V
$\Delta V_{OUT}/\Delta V_{IN}$	Line Regulation $V_{IN} = 4\text{V to }12\text{V}$ $I_{LOAD} = 0.3\text{A}$	20		50/ 100	mV
$\Delta V_{OUT}/\Delta I_{LOAD}$	Load Regulation $V_{IN} = 12\text{V}$ $I_{LOAD} = 0.3\text{A to }1.2\text{A}$	20		50/ 100	mV
η	Efficiency $V_{IN} = 5\text{V}$, $I_{LOAD} = 0.3\text{A}$	76%			
UNIQUE DEVICE PARAMETERS ⁽²⁾					
V_{REF}	Output Reference Voltage Measured at Feedback Pin $V = 1.0\text{V}$	3.3	3.242/ 3.234	3.358/ 3.366	V
ΔV_{REF}	Reference Voltage Line Regulation $V_{IN} = 4\text{V to }40\text{V}$	2			mV
G_M	Error Amp Transconductance $I_{COMP} = -30 \mu\text{A to }+30 \mu\text{A}$ $V_{COMP} = 1\text{V}$	1.193	0.678	2.259	mmho
A_{VOL}	Error Amp Voltage Gain $V_{COMP} = 0.5\text{V to }1.6\text{V}$ $R_{COMP} = 1 \text{ M}\Omega$ ⁽³⁾	260	151/ 75		V/V

- (1) External components such as the diode, inductor, input and output capacitors can affect switching regulator performance. When the LM2586 is used as shown in [Figure 54](#) and [Figure 55](#), system performance will be as specified by the system parameters.
- (2) All room temperature limits are 100% production tested, and all limits at temperature extremes are specified via correlation using standard Statistical Quality Control (SQC) methods.
- (3) A 1.0 M Ω resistor is connected to the compensation pin (which is the error amplifier output) to ensure accuracy in measuring A_{VOL} .

6.6 Electrical Characteristics: 5 V

PARAMETER		TEST CONDITIONS	TYP	MIN	MAX	UNIT
SYSTEM PARAMETERS Test Circuit of COMPFigure 54 ⁽¹⁾						
V _{OUT}	Output Voltage	V _{IN} = 4V to 12V I _{LOAD} = 0.3A to 1.1A	5.0	4.80/4.75	5.20/5.25	V
ΔV _{OUT} /ΔV _{IN}	Line Regulation	V _{IN} = 4V to 12V I _{LOAD} = 0.3A	20		50/100	mV
ΔV _{OUT} /ΔI _{LOAD}	Load Regulation	V _{IN} = 12V I _{LOAD} = 0.3A to 1.1A	20		50/100	mV
η	Efficiency	V _{IN} = 12V, I _{LOAD} = 0.6A	80%			
UNIQUE DEVICE PARAMETERS ⁽²⁾						
V _{REF}	Output Reference Voltage	Measured at Feedback Pin V _{COMP} = 1 V	5.0	4.913/4.900	5.088/5.100	V
ΔV _{REF}	Reference Voltage Line Regulation	V _{IN} = 4V to 40V	3.3			mV
G _M	Error Amp Transconductance	I _{COMP} = −30 μA to +30 μA V _{COMP} = 1 V	0.750	0.447	1.491	mmho
A _{VOL}	Error Amp Voltage Gain	V _{COMP} = 0.5V to 1.6V R _{COMP} = 1 MΩ ⁽³⁾	165	99/49		V/V

- (1) External components such as the diode, inductor, input and output capacitors can affect switching regulator performance. When the LM2586 is used as shown in [Figure 54](#) and [Figure 55](#), system performance will be as specified by the system parameters.
- (2) All room temperature limits are 100% production tested, and all limits at temperature extremes are specified via correlation using standard Statistical Quality Control (SQC) methods.
- (3) A 1.0 M Ω resistor is connected to the compensation pin (which is the error amplifier output) to ensure accuracy in measuring A_{VOL} .

6.7 Electrical Characteristics: 12 V

PARAMETER		TEST CONDITIONS	TYP	MIN	MAX	UNIT
SYSTEM PARAMETERS Test Circuit of Figure 55 ⁽¹⁾						
V _{OUT}	Output Voltage	V _{IN} = 4V to 10V I _{LOAD} = 0.2A to 0.8A	12	11.52/ 11.40	12.48/ 12.60	V
ΔV _{OUT} /ΔV _{IN}	Line Regulation	V _{IN} = 4V to 10V I _{LOAD} = 0.2A	20		100/ 200	mV
ΔV _{OUT} /ΔI _{LOAD}	Load Regulation	V _{IN} = 10V I _{LOAD} = 0.2A to 0.8A	20		100/ 200	mV
η	Efficiency	V _{IN} = 10V, I _{LOAD} = 0.6A	93%			
UNIQUE DEVICE PARAMETERS ⁽²⁾						
V _{REF}	Output Reference Voltage	Measured at Feedback Pin V _{COMP} = 1.0V	12	11.79/ 11.76	12.21/ 12.24	V
ΔV _{REF}	Reference Voltage Line Regulation	V _{IN} = 4V to 40V	7.8			mV
G _M	Error Amp Transconductance	I _{COMP} = -30 μA to +30 μA V _{COMP} = 1.0V	0.328	0.186	0.621	mmho
A _{VOL}	Error Amp Voltage Gain	V _{COMP} = 0.5V to 1.6V R _{COMP} = 1.0 MΩ ⁽³⁾	70	41/21		V/V

- (1) External components such as the diode, inductor, input and output capacitors can affect switching regulator performance. When the LM2586 is used as shown in [Figure 54](#) and [Figure 55](#), system performance will be as specified by the system parameters.
- (2) All room temperature limits are 100% production tested, and all limits at temperature extremes are specified via correlation using standard Statistical Quality Control (SQC) methods.
- (3) A 1.0 MΩ resistor is connected to the compensation pin (which is the error amplifier output) to ensure accuracy in measuring A_{VOL}.

6.8 Electrical Characteristics: Adjustable

PARAMETER		TEST CONDITIONS	TYP	MIN	MAX	UNIT
SYSTEM PARAMETERS Test Circuit of Figure 55 ⁽¹⁾						
V _{OUT}	Output Voltage	V _{IN} = 4V to 10V I _{LOAD} = 0.2A to 0.8A	12.0	11.52/11.40	12.48/12.60	V
ΔV _{OUT} /ΔV _{IN}	Line Regulation	V _{IN} = 4V to 10V I _{LOAD} = 0.2A	20		100/200	mV
ΔV _{OUT} /ΔI _{LOAD}	Load Regulation	V _{IN} = 10V I _{LOAD} = 0.2A to 0.8A	20		100/200	mV
η	Efficiency	V _{IN} = 10V, I _{LOAD} = 0.6A	93			%
UNIQUE DEVICE PARAMETERS ⁽²⁾						
V _{REF}	Output Reference Voltage	Measured at Feedback Pin V _{COMP} = 1.0V	1.230	1.208/1.205	1.252/1.255	V
ΔV _{REF}	Reference Voltage Line Regulation	V _{IN} = 4V to 40V	1.5			mV
G _M	Error Amp Transconductance	I _{COMP} = -30 μA to +30 μA V _{COMP} = 1.0V	3.200	1.800	6.000	mmho
A _{VOL}	Error Amp Voltage Gain	V _{COMP} = 0.5V to 1.6V, R _{COMP} = 1.0 MΩ ⁽³⁾	670	400/200		V/V
I _B	Error Amp Input Bias Current	V _{COMP} = 1.0V	125		425/600	nA
COMMON DEVICE PARAMETERS for all versions ⁽²⁾						
I _S	Input Supply Current	Switch Off ⁽⁴⁾	11		15.5/16.5	mA
		I _{SWITCH} = 1.8A	50		100/115	mA
I _{S/D}	Shutdown Input Supply Current	V _{SH} = 3V	16		100/300	μA
V _{UV}	Input Supply Undervoltage Lockout	R _{LOAD} = 100Ω	3.30	3.05	3.75	V
f _O	Oscillator Frequency	Measured at Switch Pin R _{LOAD} = 100Ω, V _{COMP} = 1.0V Freq. Adj. Pin Open (Pin 1)	100	85/75	115/125	kHz
		R _{SET} = 22 kΩ	200			kHz
f _{SC}	Short-Circuit Frequency	Measured at Switch Pin R _{LOAD} = 100Ω V _{FEEDBACK} = 1.15V	25			kHz
V _{EAO}	Error Amplifier Output Swing	Upper Limit ⁽⁵⁾	2.8	2.6/2.4		V
		Lower Limit ⁽⁴⁾	0.25		0.40/0.55	V
I _{EAO}	Error Amp Output Current (Source or Sink)	See ⁽⁶⁾	165	110/70	260/320	μA
I _{SS}	Soft Start Current	V _{FEEDBACK} = 0.92V V _{COMP} = 1.0V	11.0	8.0/7.0	17.0/19.0	μA
D _{MAX}	Maximum Duty Cycle	R _{LOAD} = 100Ω ⁽⁵⁾	98%	93%/90%		
I _L	Switch Leakage Current	Switch Off V _{SWITCH} = 60V	15		300/600	μA
V _{SUS}	Switch Sustaining Voltage	dV/dT = 1.5V/ns		65		V
V _{SAT}	Switch Saturation Voltage	I _{SWITCH} = 3.0A	0.45		0.65/0.9	V

- (1) External components such as the diode, inductor, input and output capacitors can affect switching regulator performance. When the LM2586 is used as shown in [Figure 54](#) and [Figure 55](#), system performance will be as specified by the system parameters.
- (2) All room temperature limits are 100% production tested, and all limits at temperature extremes are specified via correlation using standard Statistical Quality Control (SQC) methods.
- (3) A 1.0 MΩ resistor is connected to the compensation pin (which is the error amplifier output) to ensure accuracy in measuring A_{VOL}.
- (4) To measure this parameter, the feedback voltage is set to a high value, depending on the output version of the device, to force the error amplifier output low and the switch off.
- (5) To measure this parameter, the feedback voltage is set to a low value, depending on the output version of the device, to force the error amplifier output high and the switch on.
- (6) To measure the worst-case error amplifier output current, the LM2586 is tested with the feedback voltage set to its low value ([Note 4](#)) and at its high value ([Note 5](#)).

Electrical Characteristics: Adjustable (continued)

PARAMETER		TEST CONDITIONS	TYP	MIN	MAX	UNIT
I _{CL}	NPN Switch Current Limit		4.0	3.0	7.0	A
V _{STH}	Synchronization Threshold Voltage	F _{SYNC} = 200 kHz V _{COMP} = 1V, V _{IN} = 5V	0.75	0.625/0.40	0.875/1.00	V
I _{SYNC}	Synchronization Pin Current	V _{IN} = 5V V _{COMP} = 1V, V _{SYNC} = V _{STH}	100		200	μA
V _{SHTH}	ON/OFF Pin (Pin 1) Threshold Voltage	V _{COMP} = 1V (7)	1.6	1.0/0.8	2.2/2.4	V
I _{SH}	ON/OFF Pin (Pin 1) Current	V _{COMP} = 1V V _{SH} = V _{SHTH}	40	15/10	65/75	μA

- (7) When testing the minimum value, do not sink current from this pin—isolate it with a diode. If current is drawn from this pin, the frequency adjust circuit will begin operation ([Figure 25](#)).

6.9 Typical Characteristics

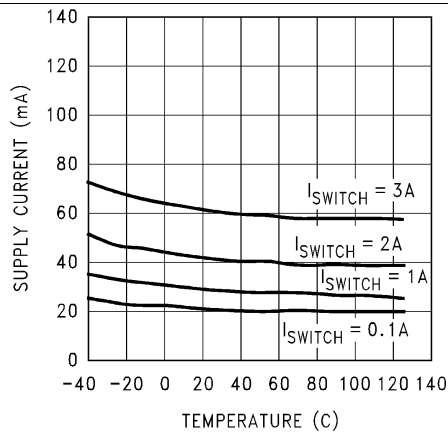


Figure 1. Supply Current vs Temperature

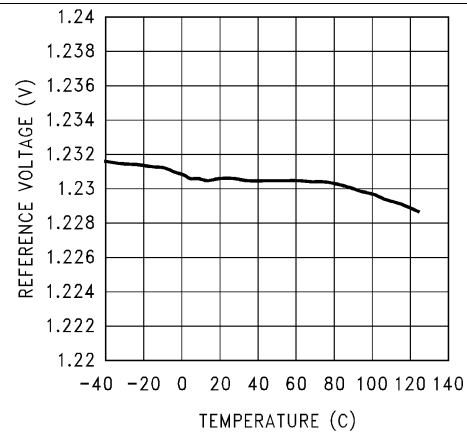


Figure 2. Reference Voltage vs Temperature

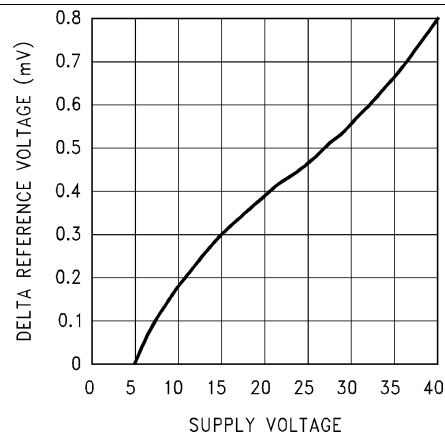


Figure 3. Δreference Voltage vs Supply Voltage

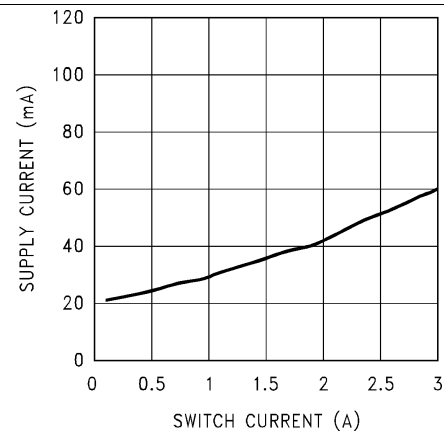


Figure 4. Supply Current vs Switch Current

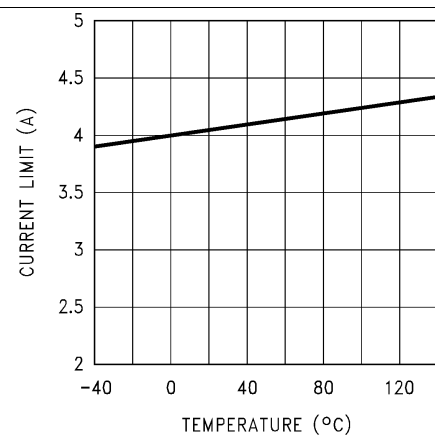


Figure 5. Current Limit vs Temperature

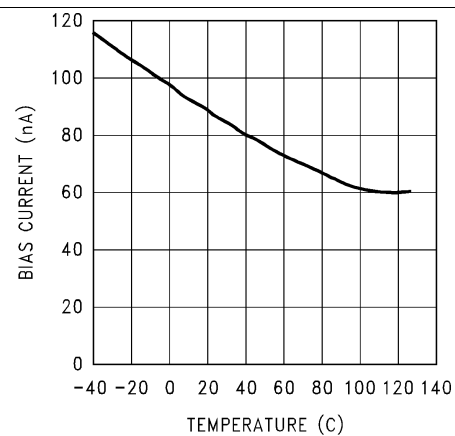


Figure 6. Feedback Pin Bias Current vs Temperature

Typical Characteristics (continued)

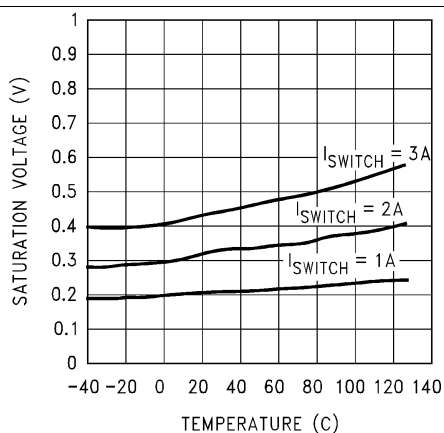


Figure 7. Switch Saturation Voltage vs Temperature

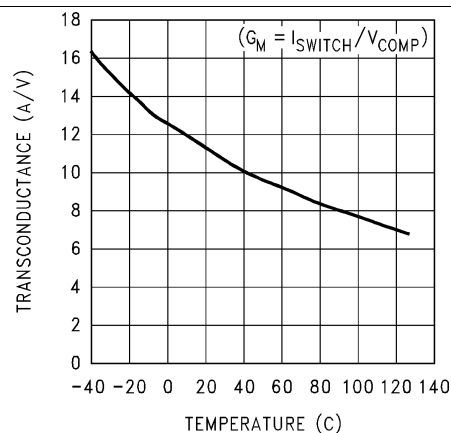


Figure 8. Switch Transconductance vs Temperature

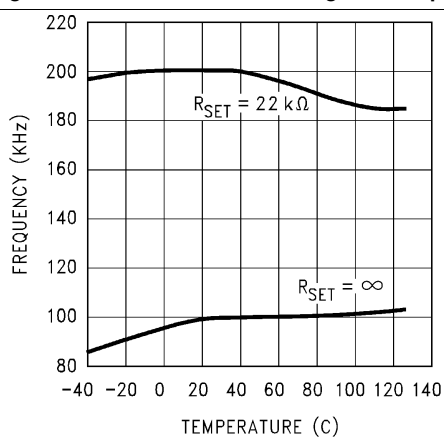


Figure 9. Oscillator Frequency vs Temperature

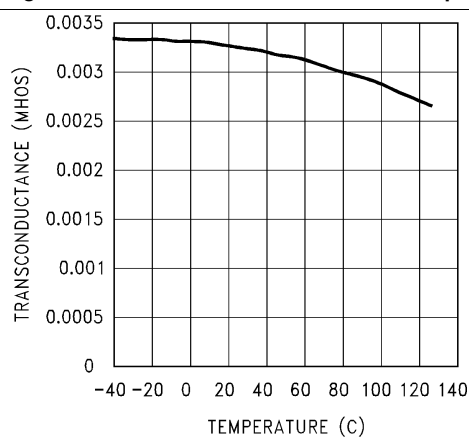


Figure 10. Error Amp Transconductance vs Temperature

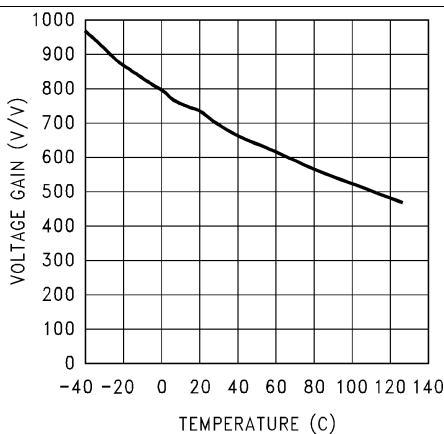


Figure 11. Error Amp Voltage Gain vs Temperature

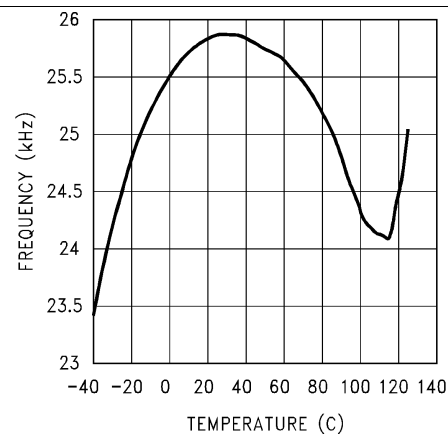


Figure 12. Short Circuit Frequency vs Temperature

Typical Characteristics (continued)

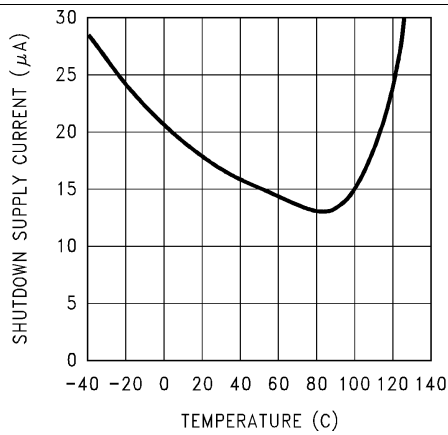


Figure 13. Shutdown Supply Current vs Temperature

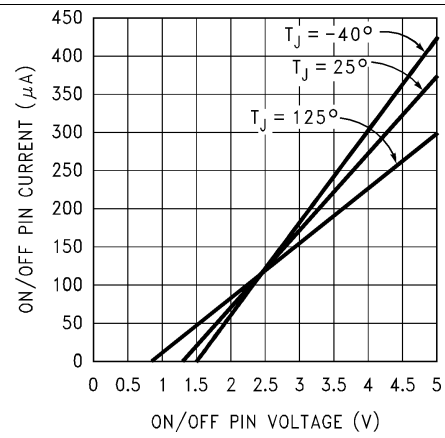


Figure 14. $\overline{\text{ON}}$ /Off Pin Current vs Voltage

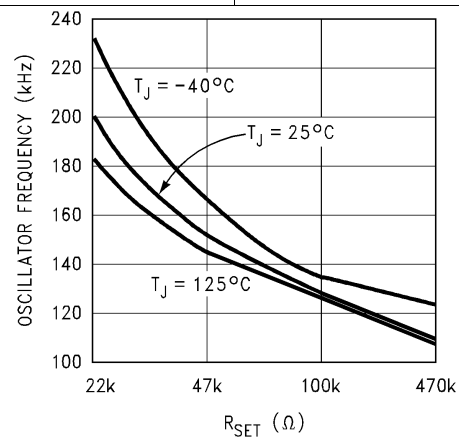


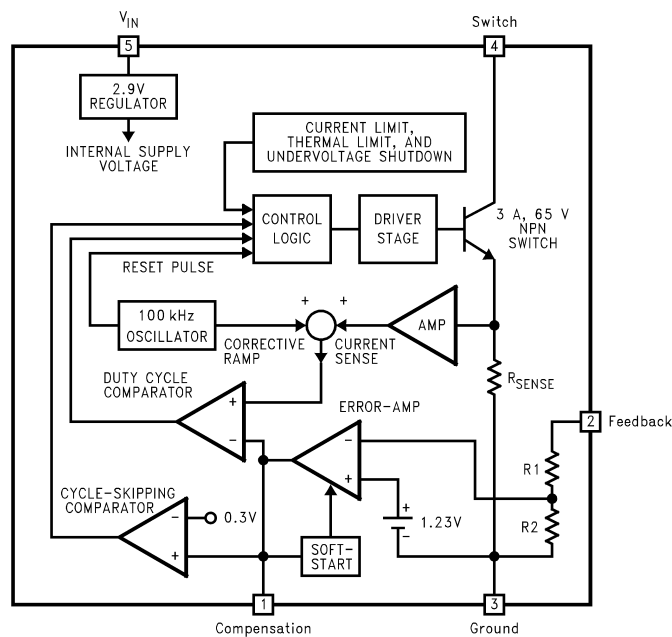
Figure 15. Oscillator Frequency vs Resistance

7 Detailed Description

7.1 Overview

The LM2586 series of regulators are monolithic integrated circuits specifically designed for flyback, step-up (boost), and forward converter applications. The device is available in 4 different output voltage versions: 3.3 V, 5 V, 12 V, and adjustable. Requiring a minimum number of external components, these regulators are cost effective, and simple to use. Included in the datasheet are typical circuits of boost and flyback regulators. Also listed are selector guides for diodes and capacitors and a family of standard inductors and flyback transformers designed to work with these switching regulators.

7.2 Functional Block Diagram



For Fixed Versions

3.3V, R1 = 3.4k, R2 = 2k

5V, R1 = 6.15k, R2 = 2k

12V, R1 = 8.73k, R2 = 1k

For Adj. Version

R1 = Short (0Ω), R2 = Open

7.3 Feature Description

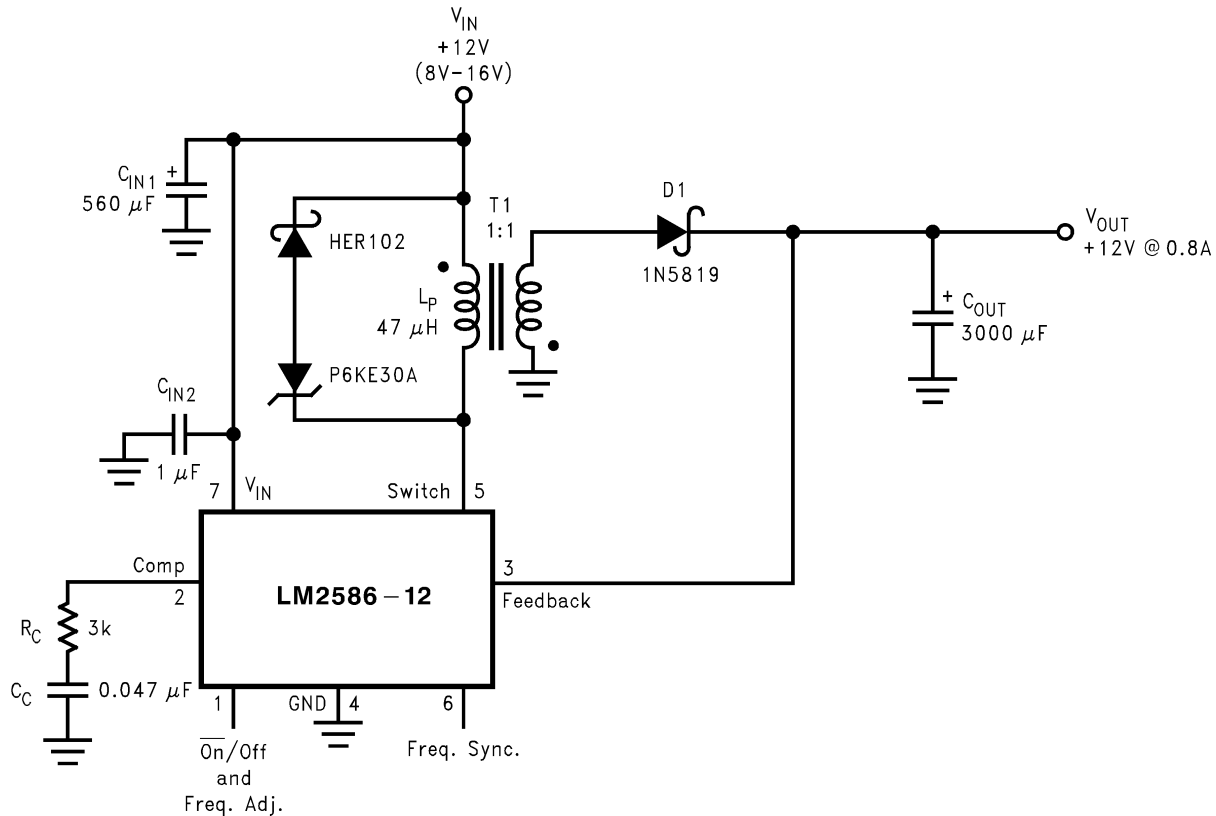
7.3.1 Flyback Regulator Operation

The LM2586 is ideally suited for use in the flyback regulator topology. The flyback regulator can produce a single output voltage, such as the one shown in [Figure 16](#), or multiple output voltages. In [Figure 16](#), the flyback regulator generates an output voltage that is inside the range of the input voltage. This feature is unique to flyback regulators and cannot be duplicated with buck or boost regulators.

The operation of a flyback regulator is as follows (refer to [Figure 16](#)): when the switch is on, current flows through the primary winding of the transformer, T1, storing energy in the magnetic field of the transformer. Note that the primary and secondary windings are out of phase, so no current flows through the secondary when current flows through the primary. When the switch turns off, the magnetic field collapses, reversing the voltage polarity of the primary and secondary windings. Now rectifier D1 is forward biased and current flows through it, releasing the energy stored in the transformer. This produces voltage at the output.

Feature Description (continued)

The output voltage is controlled by modulating the peak switch current. This is done by feeding back a portion of the output voltage to the error amp, which amplifies the difference between the feedback voltage and a 1.230V reference. The error amp output voltage is compared to a ramp voltage proportional to the switch current (in other words, inductor current during the switch on time). The comparator terminates the switch on time when the two voltages are equal, thereby controlling the peak switch current to maintain a constant output voltage.



As shown in Figure 16, the LM2586 can be used as a flyback regulator by using a minimum number of external components. The switching waveforms of this regulator are shown in . Typical performance characteristics observed during the operation of this circuit are shown in .

Figure 16. 12-V Flyback Regulator Design Example

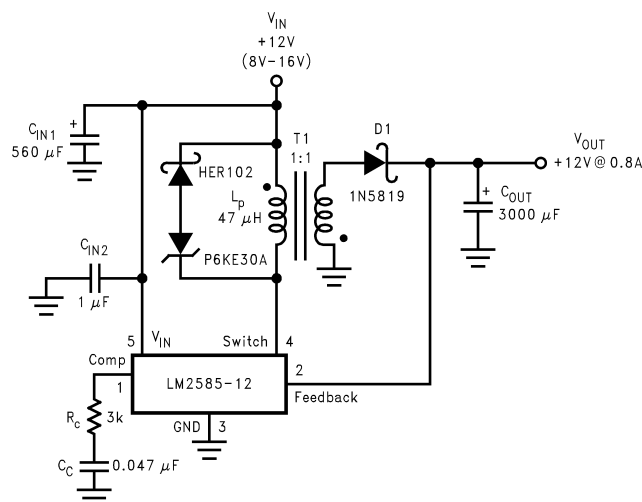
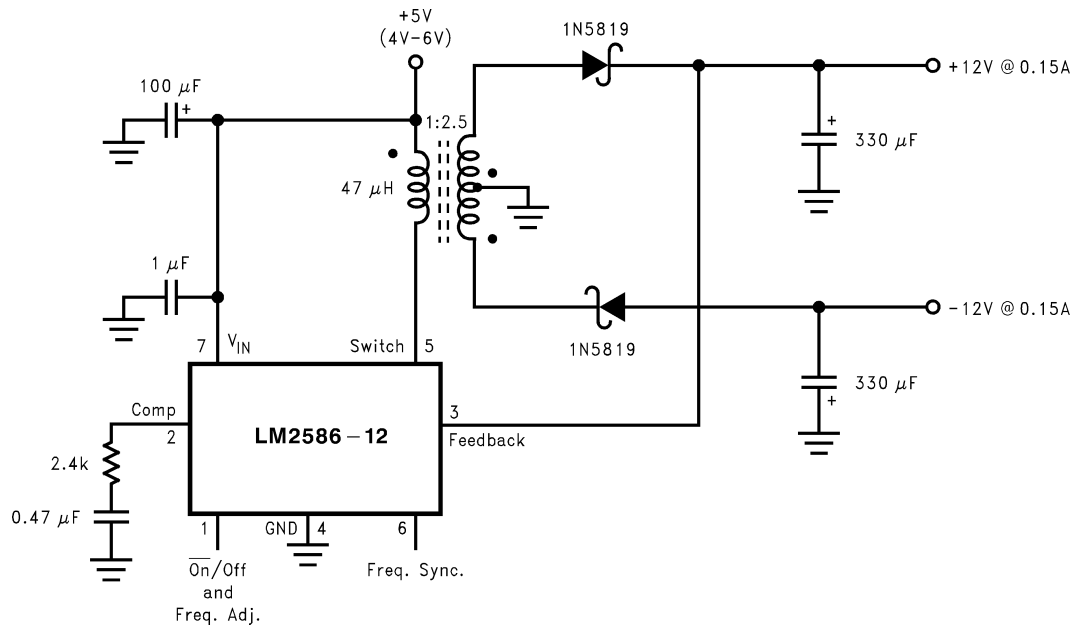
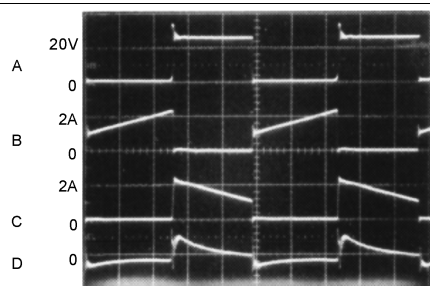


Figure 17. 12-V Flyback Regulator Design Example

Feature Description (continued)



- (1) As shown in Figure 17, the LM2585 can be used as a flyback regulator by using a minimum number of external components. The switching waveforms of this regulator are shown in Figure 18. Typical characteristics observed during the operation of this circuit are shown in Figure 19.



A: Switch Voltage, 20 V/div
B: Switch Current, 2 A/div
C: Output Rectifier Current, 2 A/div
D: Output Ripple Voltage, 50 mV/div
AC-Coupled
Horizontal: 2 μs/div

Figure 18. Switching Waveforms

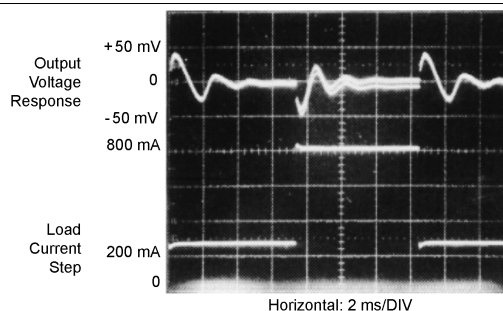


Figure 19. V_{OUT} Load Current Step Response

Feature Description (continued)

7.3.2 Step-Up (Boost) Regulator Operation

Figure 20 shows the LM2586 used as a step-up (boost) regulator. This is a switching regulator that produces an output voltage greater than the input supply voltage.

A brief explanation of how the LM2586 boost regulator works is as follows (refer to Figure 20). When the NPN switch turns on, the inductor current ramps up at the rate of V_{IN}/L , storing energy in the inductor. When the switch turns off, the lower end of the inductor flies above V_{IN} , discharging its current through diode (D) into the output capacitor (C_{OUT}) at a rate of $(V_{OUT} - V_{IN})/L$. Thus, energy stored in the inductor during the switch on time is transferred to the output during the switch off time. The output voltage is controlled by adjusting the peak switch current, as described in .

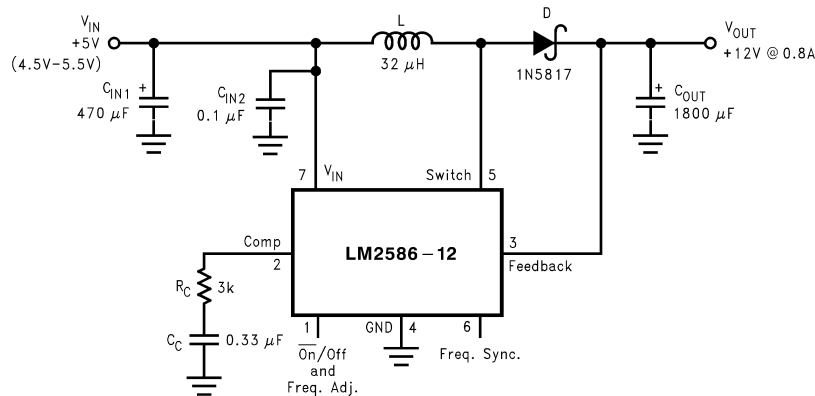
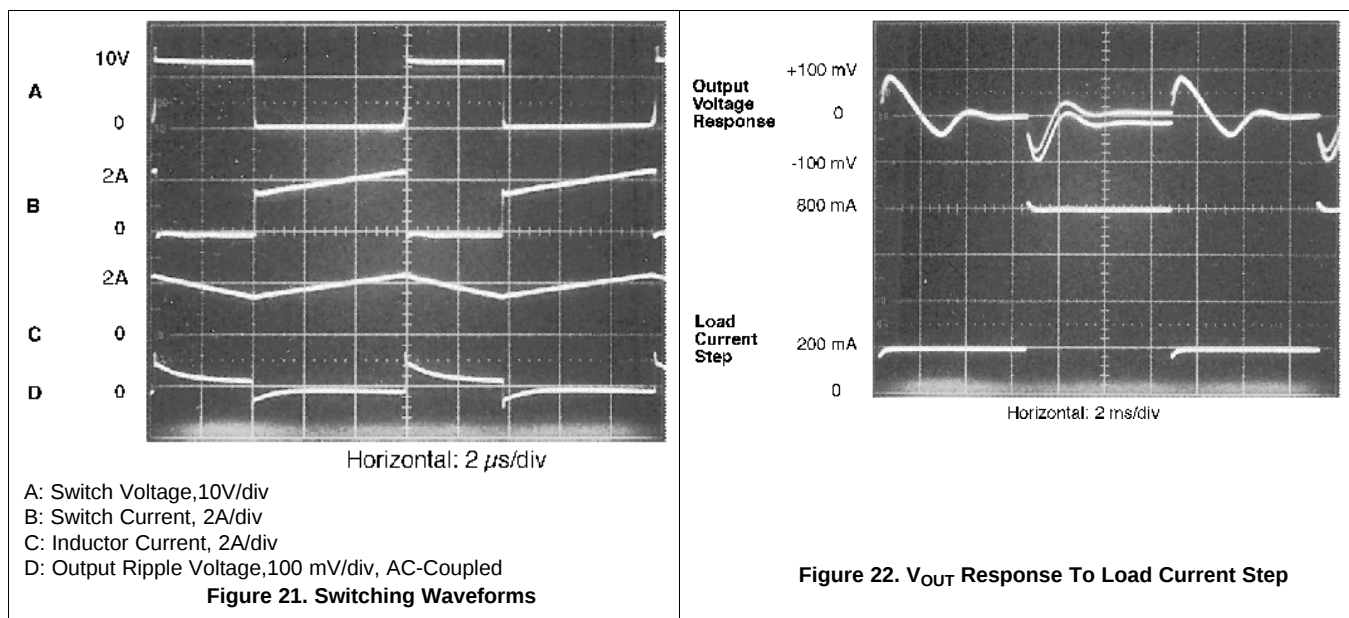


Figure 20. 12-V Boost Regulator

By adding a small number of external components (as shown in Figure 20), the LM2586 can be used to produce a regulated output voltage that is greater than the applied input voltage. The switching waveforms observed during the operation of this circuit are shown in Figure 21. Typical performance of this regulator is shown in Figure 22.



Feature Description (continued)

7.3.3 Programming Output Voltage (Selecting R1 And R2)

Referring to the adjustable regulator in Figure 26, the output voltage is programmed by the resistors R1 and R2 by the following formula:

$$V_{OUT} = V_{REF} (1 + R1/R2)$$

where

- $V_{REF} = 1.23V$ (1)

Resistors R1 and R2 divide the output voltage down so that it can be compared with the 1.23V internal reference. With R2 between 1k and 5k, R1 is:

$$R1 = R2 (V_{OUT}/V_{REF} - 1)$$

where

- $V_{REF} = 1.23V$ (2)

For best temperature coefficient and stability with time, use 1% metal film resistors.

7.3.4 Shutdown Control

A feature of the LM2586 is its ability to be shut down using the $\overline{ON}/OFF$ pin (pin 1). This feature conserves input power by turning off the device when it is not in use. For proper operation, an isolation diode is required (as shown in Figure 23).

The device will shut down when 3V or greater is applied on the $\overline{ON}/OFF$ pin, sourcing current into pin 1. In shut down mode, the device will draw typically 56 μA of supply current (16 μA to V_{IN} and 40 μA to the $\overline{ON}/OFF$ pin). To turn the device back on, leave pin 1 floating, using an (isolation) diode, as shown in Figure 23 (for normal operation, do not source or sink current to or from this pin—see the next section).

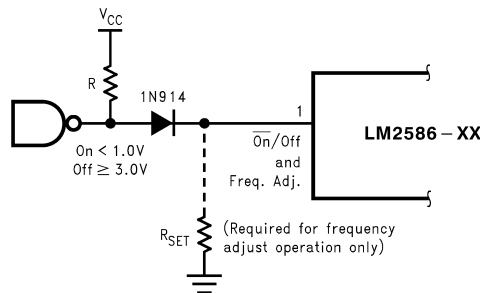


Figure 23. Shutdown Operation

7.3.5 Frequency Adjustment

The switching frequency of the LM2586 can be adjusted with the use of an external resistor. This feature allows the user to optimize the size of the magnetics and the output capacitor(s) by tailoring the operating frequency. A resistor connected from pin 1 (the Freq. Adj. pin) to ground will set the switching frequency from 100 kHz to 200 kHz (maximum). As shown in Figure 23, the pin can be used to adjust the frequency while still providing the shutdown function. A curve in Typical Characteristics the resistor value to the corresponding switching frequency. Table 1 shows resistor values corresponding to commonly used frequencies.

However, changing the LM2586 operating frequency from its nominal value of 100 kHz changes the magnetics selection and compensation component values.

Table 1. Frequency Setting Resistor Guide

$R_{SET}(k\Omega)$	Frequency (kHz)
Open	100
200	125
47	150
33	175

Feature Description (continued)

Table 1. Frequency Setting Resistor Guide (continued)

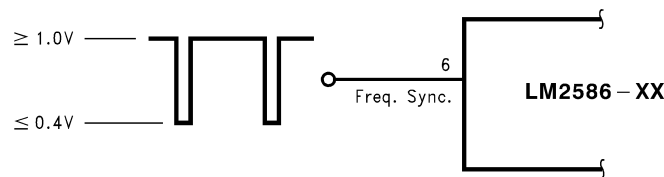
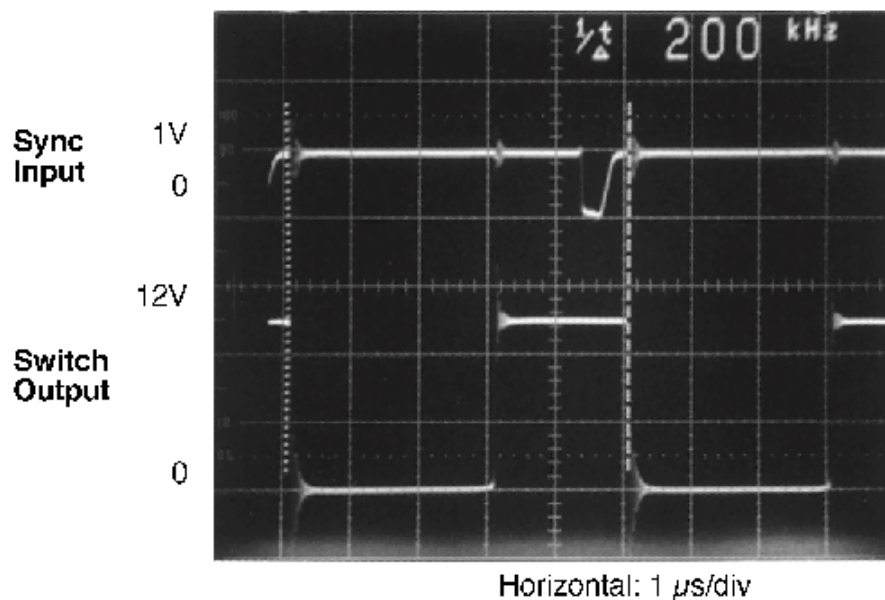
$R_{SET}(k\Omega)$	Frequency (kHz)
22	200

7.3.6 Frequency Synchronization

Another feature of the LM2586 is the ability to synchronize the switching frequency to an external source, using the sync pin (pin 6). This feature allows the user to parallel multiple devices to deliver more output power.

A negative falling pulse applied to the sync pin will synchronize the LM2586 to an external oscillator (see [Figure 24](#) and [Figure 25](#)).

Use of this feature enables the LM2586 to be synchronized to an external oscillator, such as a system clock. This operation allows multiple power supplies to operate at the same frequency, thus eliminating frequency-related noise problems.


Figure 24. Frequency Synchronization

Figure 25. Waveforms of a Synchronized 12-V Boost Regulator

The scope photo in [Figure 25](#) shows a LM2586 12-V boost regulator synchronized to a 200-kHz signal. There is a 700-ns delay between the falling edge of the sync signal and the turning on of the switch.

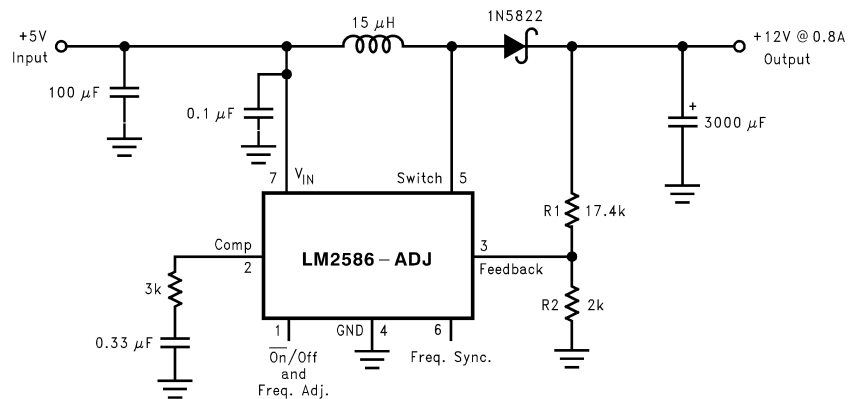


Figure 26. Boost Regulator

8 Application and Implementation

NOTE

Information in the following applications sections is not part of the TI component specification, and TI does not warrant its accuracy or completeness. TI's customers are responsible for determining suitability of components for their purposes. Customers should validate and test their design implementation to confirm system functionality.

8.1 Application Information

The LM2586 series of regulators are monolithic integrated circuits specifically designed for flyback, step-up (boost), and forward converter applications. Requiring a minimum number of external components, these regulators are cost effective, and simple to use. Included in the datasheet are typical circuits of boost and flyback regulators. Also listed are selector guides for diodes and capacitors and a family of standard inductors and flyback transformers designed to work with these switching regulators.

8.2 Typical Applications

8.2.1 Typical Flyback Regulator Applications

Figure 27 through Figure 32 show six typical flyback applications, varying from single output to triple output. Each drawing contains the part number(s) and manufacturer(s) for every component except the transformer. For the transformer part numbers and manufacturers' names, see Table 2. For applications with different output voltages—requiring the LM2586-ADJ—or different output configurations that do not match the standard configurations, refer to the *Switchers Made Simple* software.

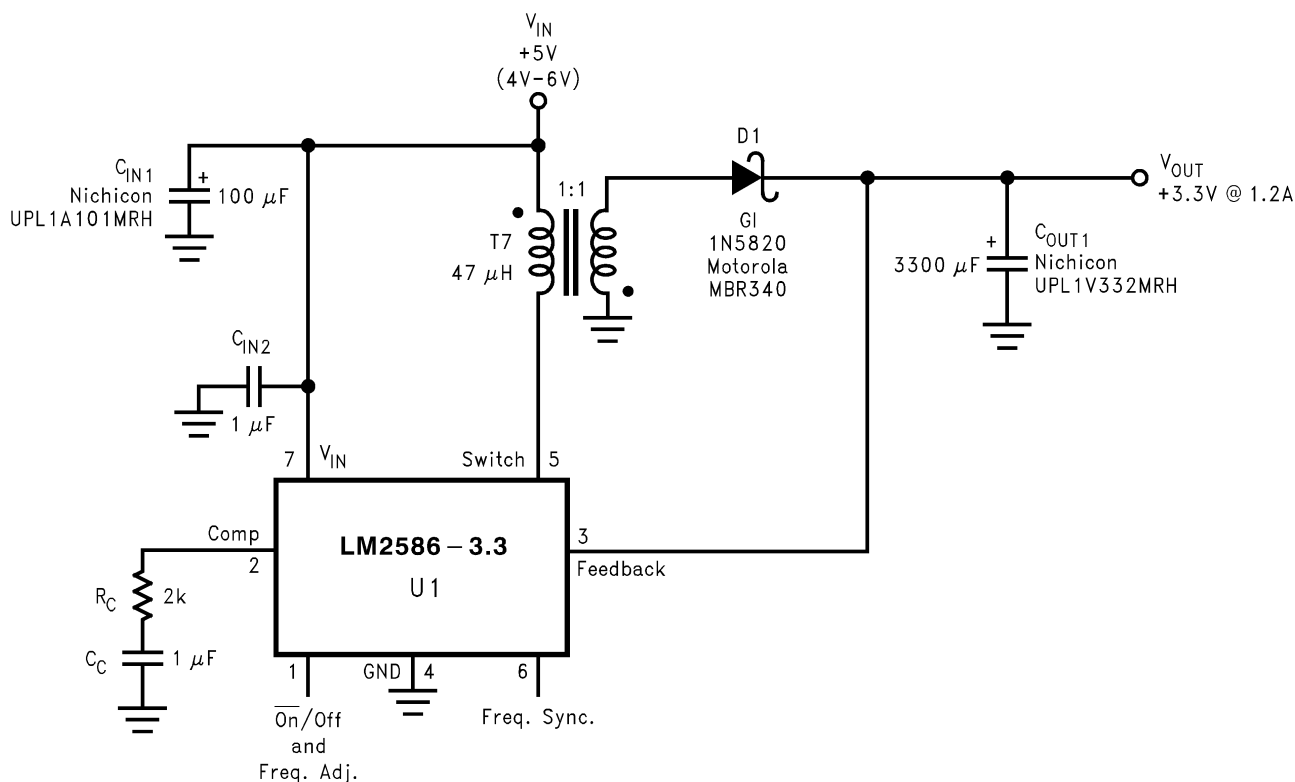


Figure 27. Single-Output Flyback Regulator

Typical Applications (continued)

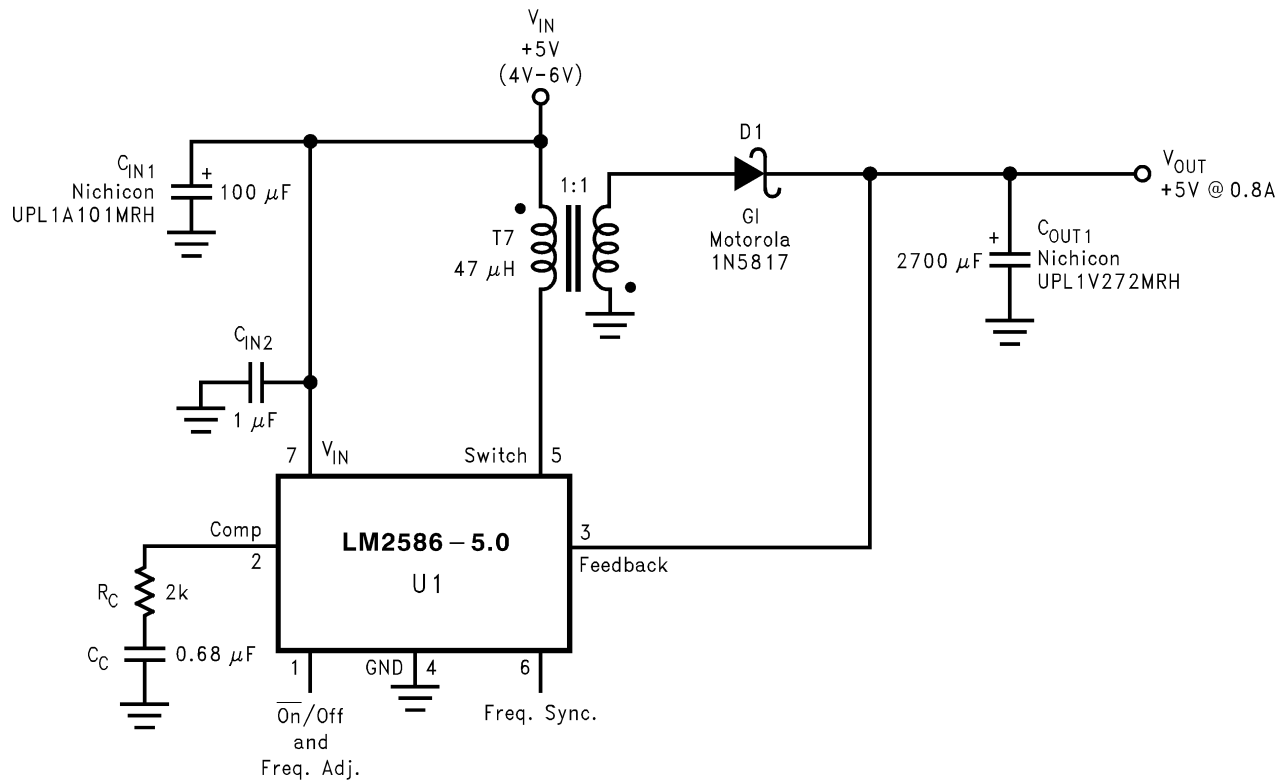
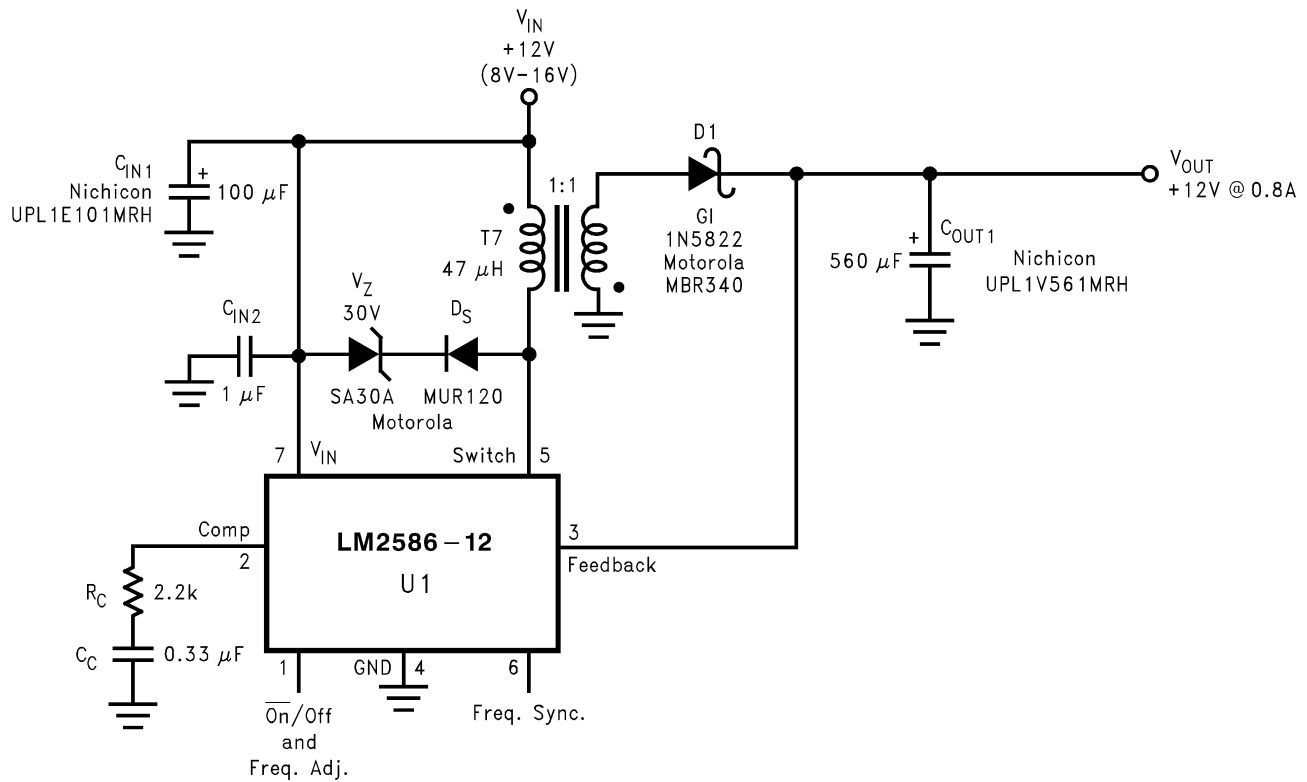


Figure 28. Single-Output Flyback Regulator

Typical Applications (continued)

Figure 29. Single-Output Flyback Regulator

Typical Applications (continued)

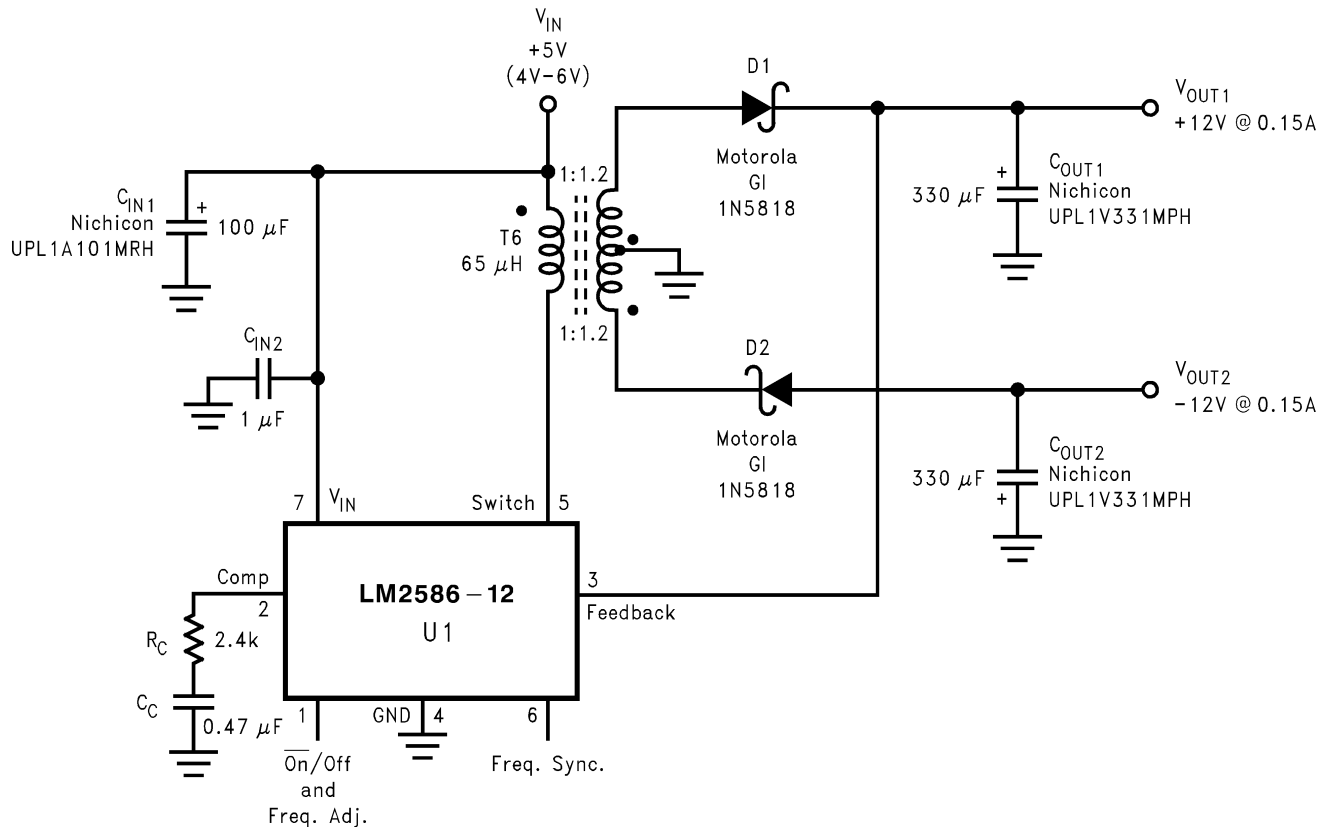


Figure 30. Dual-Output Flyback Regulator

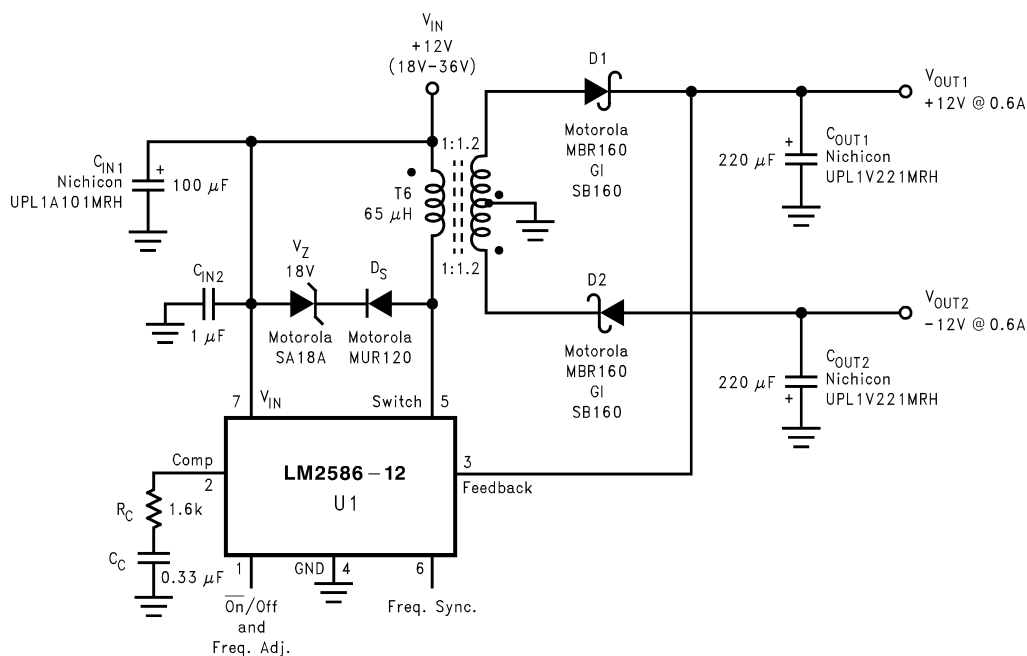


Figure 31. Dual-Output Flyback Regulator

Typical Applications (continued)

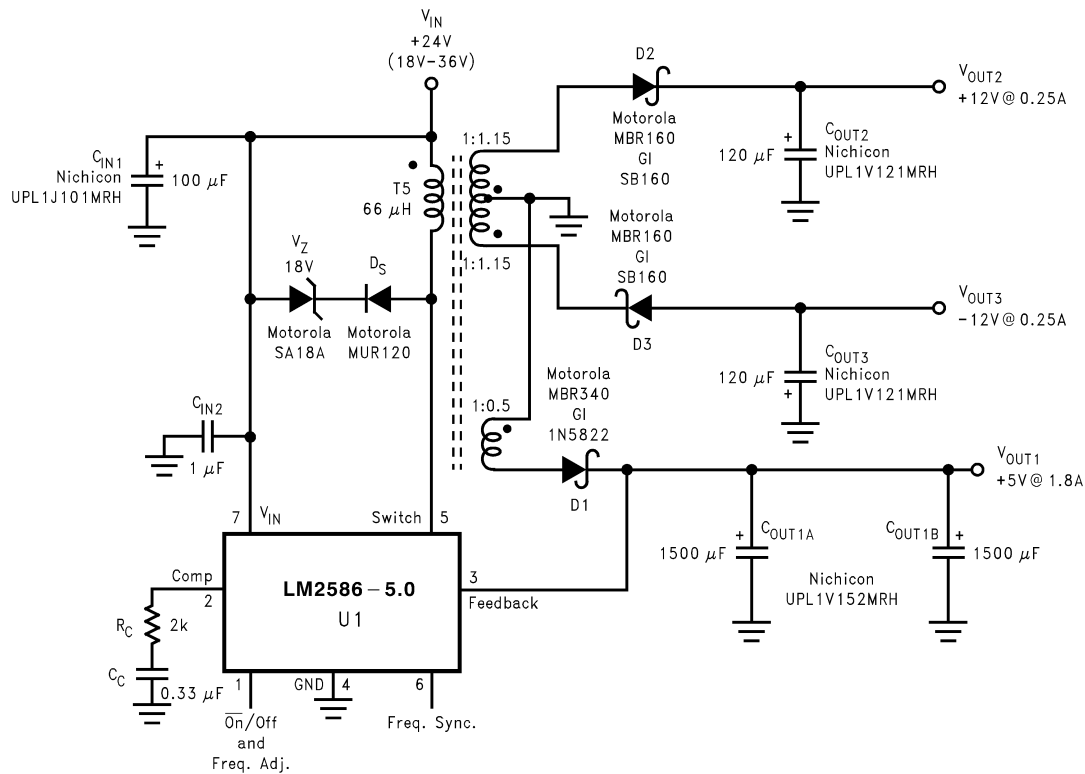


Figure 32. Triple-Output Flyback Regulator

8.2.1.1 Design Requirements

8.2.1.1.1 Transformer Selection (T)

Table 2 lists the standard transformers available for flyback regulator applications. Included in the table are the turns ratio(s) for each transformer, as well as the output voltages, input voltage ranges, and the maximum load currents for each circuit.

Table 2. Transformer Selection Table

Applications	Figure 27	Figure 28	Figure 29	Figure 30	Figure 31	Figure 32
Transformers	T7	T7	T7	T6	T6	T5
V_{IN}	4V–6V	4V–6V	8V–16V	4V–6V	18V–36V	18V–36V
V_{OUT1}	3.3V	5V	12V	12V	12V	5V
$I_{OUT1} (Max)$	1.4A	1A	0.8A	0.15A	0.6A	1.8A
N_1	1	1	1	1.2	1.2	0.5
V_{OUT2}				–12V	–12V	12V
$I_{OUT2} (Max)$				0.15A	0.6A	0.25A
N_2				1.2	1.2	1.15
V_{OUT3}						–12V
$I_{OUT3} (Max)$						0.25A
N_3						1.15

Table 3. Transformer Manufacturer Guide

Transformer Type	Manufacturers' Part Numbers					
	Coilcraft ⁽¹⁾	Coilcraft ⁽¹⁾ Surface Mount	Pulse ⁽²⁾ Surface Mount	Pulse ⁽²⁾	Renco ⁽³⁾	Schott ⁽⁴⁾
T5	Q4338-B	Q4437-B	PE-68413	—	RL-5532	67140890
T6	Q4339-B	Q4438-B	PE-68414	—	RL-5533	67140900
T7	S6000-A	S6057-A	—	PE-68482	RL-5751	26606

- (1) Coilcraft Inc., Phone: (800) 322-2645
1102 Silver Lake Road, Cary, IL 60013 Fax: (708) 639-1469
European Headquarters, 21 Napier Place Phone: +44 1236 730 595
Wardpark North, Cumbernauld, Scotland G68 0LL Fax: +44 1236 730 627
- (2) Pulse Engineering Inc., Phone: (619) 674-8100
12220 World Trade Drive, San Diego, CA 92128 Fax: (619) 674 -8262
European Headquarters, Dunmore Road Phone: +353 93 24 107
Tuam, Co. Galway, Ireland Fax: +353 93 24 459
- (3) Renco Electronics Inc., Phone: (800) 645-5828
60 Jeffryn Blvd. East, Deer Park, NY 11729 Fax: (516) 586-5562
- (4) Schott Corp., Phone: (612) 475-1173
1000 Parkers Lane Road, Wayzata, MN 55391 Fax: (612) 475-1786

8.2.1.1.2 Transformer Footprints

Figure 33 through Figure 47 show the footprints of each transformer, listed in Table 3.

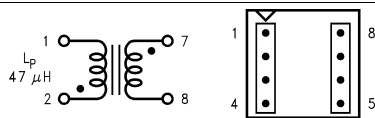


Figure 33. Coilcraft S6000-A (Top View)

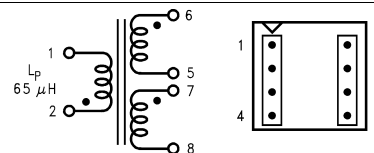


Figure 34. Coilcraft Q4339-B (Top View)

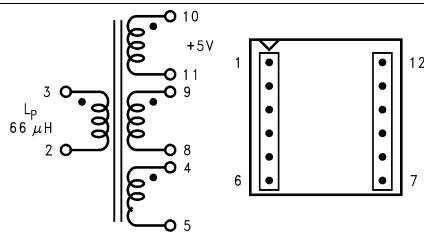


Figure 35. Coilcraft Q4437-B (Surface Mount) (Top View)

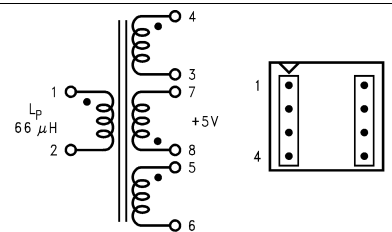
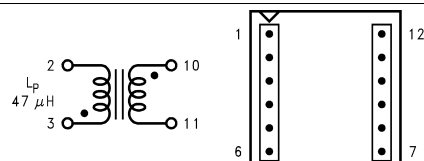
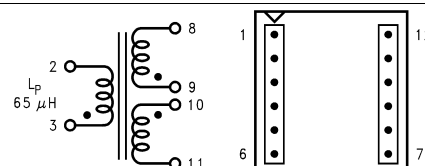


Figure 36. Coilcraft Q4338-B (Top View)



**Figure 37. Coilcraft S6057-A
(Surface Mount) (Top View)**



**Figure 38. Coilcraft Q4438-B
(Surface Mount) (Top View)**

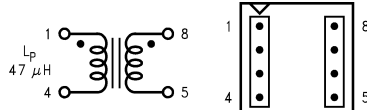
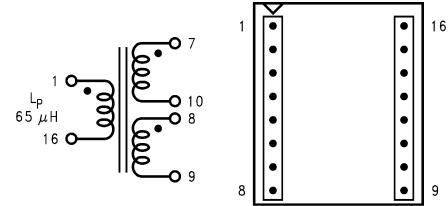
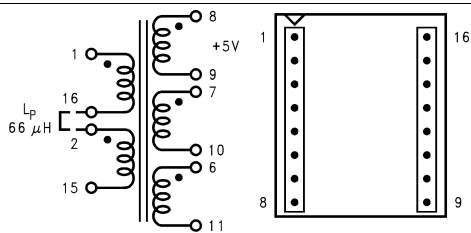


Figure 39. Pulse PE-68482 (Top View)



**Figure 40. Pulse PE-68414
(Surface Mount) (Top View)**



**Figure 41. Pulse PE-68413
(Surface Mount) (Top View)**

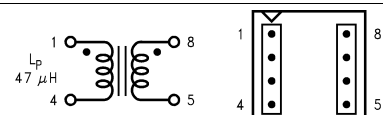


Figure 42. Renco RI-5751 (Top View)

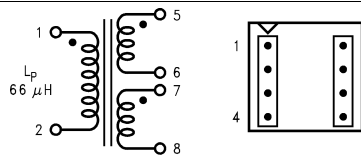


Figure 43. Renco RI-5533 (Top View)

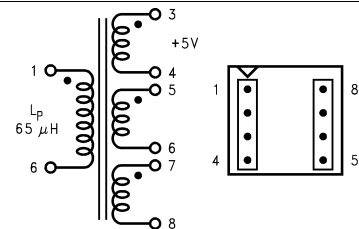


Figure 44. Renco RI-5532 (Top View)

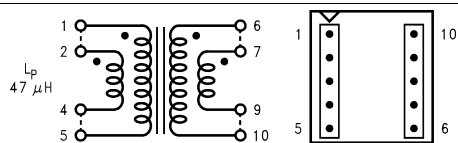


Figure 45. Schott 26606 (Top View)

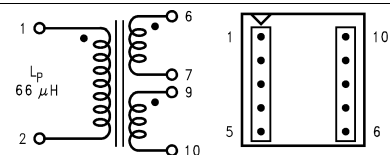


Figure 46. Schott 67140900 (Top View)

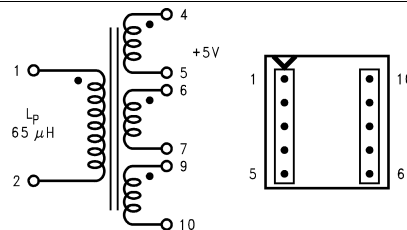


Figure 47. Schott 67140890 (Top View)

8.2.1.2 Detailed Design Procedure

8.2.1.2.1 Custom Design With WEBENCH® Tools

[Click here](#) to create a custom design using the LM2586 device with the WEBENCH® Power Designer.

1. Start by entering the input voltage (V_{IN}), output voltage (V_{OUT}), and output current (I_{OUT}) requirements.
2. Optimize the design for key parameters such as efficiency, footprint, and cost using the optimizer dial.
3. Compare the generated design with other possible solutions from Texas Instruments.

The WEBENCH Power Designer provides a customized schematic along with a list of materials with real-time pricing and component availability.

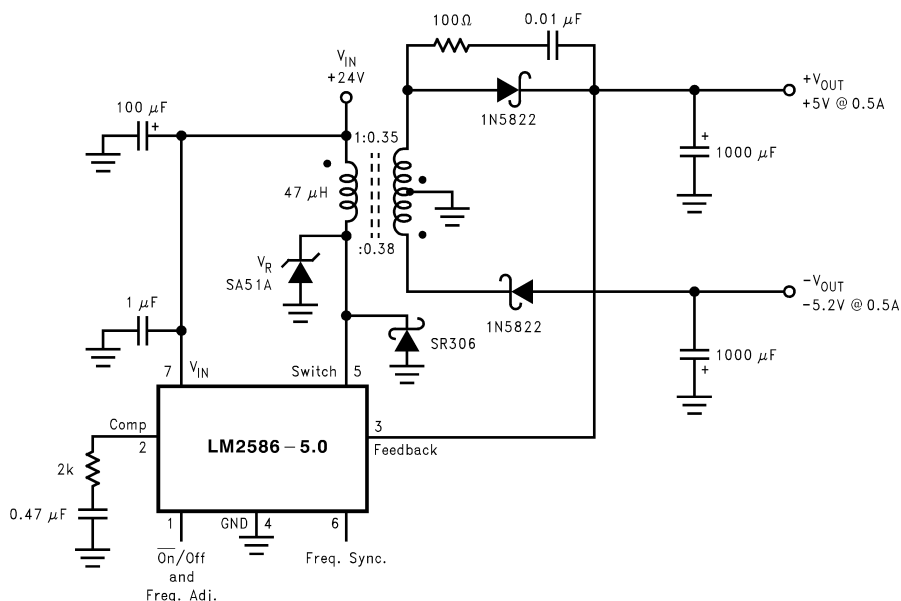
In most cases, these actions are available:

- Run electrical simulations to see important waveforms and circuit performance
- Run thermal simulations to understand board thermal performance
- Export customized schematic and layout into popular CAD formats
- Print PDF reports for the design, and share the design with colleagues

Get more information about WEBENCH tools at www.ti.com/WEBENCH.

8.2.1.2.2 Flyback Regulator Input Capacitors

A flyback regulator draws discontinuous pulses of current from the input supply. Therefore, there are two input capacitors needed in a flyback regulator—one for energy storage and one for filtering (see [Figure 48](#)). Both are required due to the inherent operation of a flyback regulator. To keep a stable or constant voltage supply to the LM2586, a storage capacitor ($\geq 100 \mu\text{F}$) is required. If the input source is a rectified DC supply and/or the application has a wide temperature range, the required rms current rating of the capacitor might be very large. This means a larger value of capacitance or a higher voltage rating will be needed for the input capacitor. The storage capacitor will also attenuate noise which may interfere with other circuits connected to the same input supply voltage.


Figure 48. Flyback Regulator

In addition, a small bypass capacitor is required due to the noise generated by the input current pulses. To eliminate the noise, insert a 1-μF ceramic capacitor between V_{IN} and ground as close as possible to the device.

8.2.1.2.3 Switch Voltage Limits

In a flyback regulator, the maximum steady-state voltage appearing at the switch, when it is off, is set by the transformer turns ratio, N , the output voltage, V_{OUT} , and the maximum input voltage, V_{IN} (maximum):

$$V_{SW(OFF)} = V_{IN} (\text{maximum}) + (V_{OUT} + V_F)/N$$

where

- V_F is the forward biased voltage of the output diode, and is typically 0.5 V for Schottky diodes and 0.8 V for ultra-fast recovery diodes (3)

In certain circuits, there exists a voltage spike, V_{LL} , superimposed on top of the steady-state voltage (see , waveform A). Usually, this voltage spike is caused by the transformer leakage inductance and/or the output rectifier recovery time. To “clamp” the voltage at the switch from exceeding its maximum value, a transient suppressor in series with a diode is inserted across the transformer primary (as shown in the circuit in [Figure 16](#) and other flyback regulator circuits throughout the datasheet). The schematic in [Figure 48](#) shows another method of clamping the switch voltage. A single voltage transient suppressor (the SA51A) is inserted at the switch pin. This method clamps the total voltage across the switch, not just the voltage across the primary.

If poor circuit layout techniques are used (see the [Circuit Layout Guideline](#) section), negative voltage transients may appear on the Switch pin (pin 5). Applying a negative voltage (with respect to the IC's ground) to any monolithic IC pin causes erratic and unpredictable operation of that IC. This holds true for the LM2586 IC as well. When used in a flyback regulator, the voltage at the Switch pin (pin 5) can go negative when the switch turns on. The “ringing” voltage at the switch pin is caused by the output diode capacitance and the transformer leakage inductance forming a resonant circuit at the secondary(ies). The resonant circuit generates the “ringing” voltage, which gets reflected back through the transformer to the switch pin. There are two common methods to avoid this problem. One is to add an RC snubber around the output rectifier(s), as in [Figure 48](#). The values of the resistor and the capacitor must be chosen so that the voltage at the Switch pin does not drop below -0.4 V. The resistor may range in value between 10Ω and $1\text{ k}\Omega$, and the capacitor will vary from $0.001\text{ }\mu\text{F}$ to $0.1\text{ }\mu\text{F}$. Adding a snubber will (slightly) reduce the efficiency of the overall circuit.

The other method to reduce or eliminate the “ringing” is to insert a Schottky diode clamp between pins 5 and 4 (ground), also shown in [Figure 48](#). This prevents the voltage at pin 5 from dropping below -0.4 V. The reverse voltage rating of the diode must be greater than the switch off voltage.

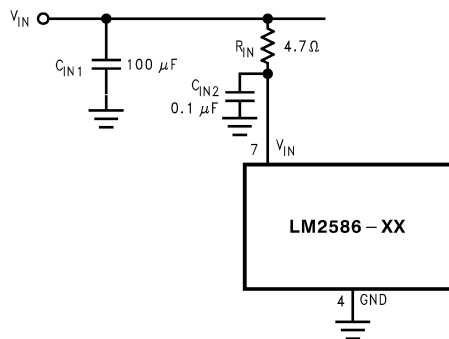


Figure 49. Input Line Filter

8.2.1.2.4 Output Voltage Limitations

The maximum output voltage of a boost regulator is the maximum switch voltage minus a diode drop. In a flyback regulator, the maximum output voltage is determined by the turns ratio, N , and the duty cycle, D , by the equation:

$$V_{OUT} \approx N \times V_{IN} \times D / (1 - D) \quad (4)$$

The duty cycle of a flyback regulator is determined by [Equation 5](#):

$$D = \frac{V_{OUT} + V_F}{N(V_{IN} - V_{SAT}) + V_{OUT} + V_F} \approx \frac{V_{OUT}}{N(V_{IN}) + V_{OUT}} \quad (5)$$

Theoretically, the maximum output voltage can be as large as desired—just keep increasing the turns ratio of the transformer. However, there exists some physical limitations that prevent the turns ratio, and thus the output voltage, from increasing to infinity. The physical limitations are capacitances and inductances in the LM2586 switch, the output diode(s), and the transformer—such as reverse recovery time of the output diode (mentioned above).

8.2.1.2.5 Noisy Input Line Condition

A small, low-pass RC filter should be used at the input pin of the LM2586 if the input voltage has an unusually large amount of transient noise, such as with an input switch that bounces. The circuit in [Figure 49](#) demonstrates the layout of the filter, with the capacitor placed from the input pin to ground and the resistor placed between the input supply and the input pin. Note that the values of R_{IN} and C_{IN} shown in the schematic are good enough for most applications, but some readjusting might be required for a particular application. If efficiency is a major concern, replace the resistor with a small inductor (say 10 μ H and rated at 200 mA).

8.2.1.2.6 Stability

All current-mode controlled regulators can suffer from an instability, known as subharmonic oscillation, if they operate with a duty cycle above 50%. To eliminate subharmonic oscillations, a minimum value of inductance is required to ensure stability for all boost and flyback regulators. The minimum inductance is given by:

$$L(\text{Min}) = \frac{2.92 [(V_{IN}(\text{Min}) - V_{SAT}) \bullet (2D(\text{Max}) - 1)]}{1 - D(\text{Max})} (\mu\text{H})$$

where

- V_{SAT} is the switch saturation voltage and can be found in the Characteristic Curves (6)

8.2.2 Typical Boost Regulator Applications

Figure 50 through Figure 53 show four typical boost applications—one fixed and three using the adjustable version of the LM2586. Each drawing contains the part number(s) and manufacturer(s) for every component. For the fixed 12-V output application, the part numbers and manufacturers' names for the inductor are listed in Table 4. For applications with different output voltages, refer to the *Switchers Made Simple* software.

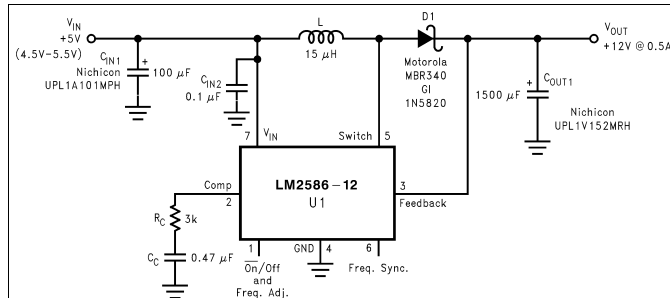


Figure 50. 5-V to 12-V Boost Regulator

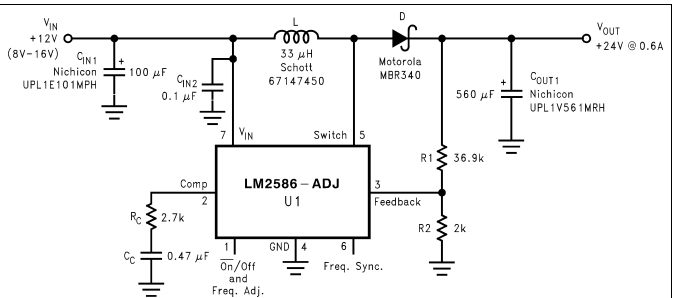
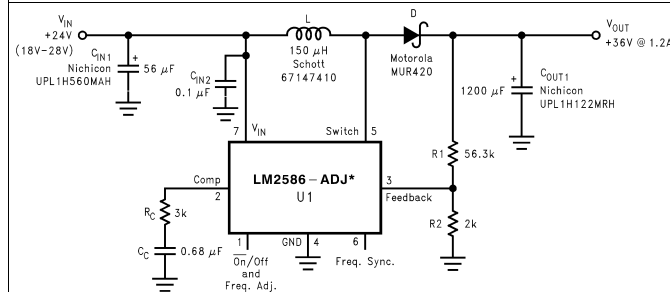
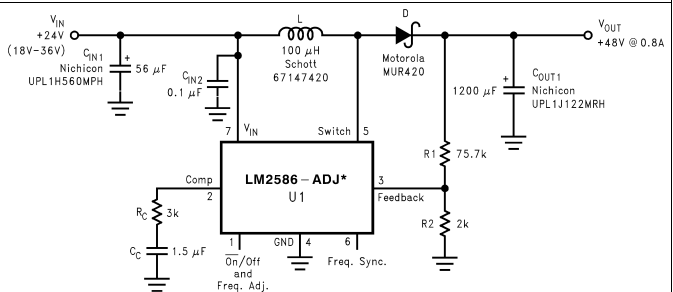


Figure 51. 12-V to 24-V Boost Regulator



The LM2586 requires a heat sink in this application. The size of the heat sink depends on the maximum ambient temperature. To calculate the thermal resistance of the IC and the size of the heat sink needed, see [Heat Sink/Thermal Considerations](#).

Figure 52. 24-V to 36-V Boost Regulator



The LM2586 requires a heat sink in this application. The size of the heat sink depends on the maximum ambient temperature. To calculate the thermal resistance of the IC and the size of the heat sink needed, see [Heat Sink/Thermal Considerations](#).

Figure 53. 24-V to 48-V Boost Regulator

8.2.2.1 Design Requirements

Table 4 contains a list of standard inductors, by part number and corresponding manufacturer, for the fixed output regulator of Figure 50.

Table 4. Inductor Selection Table

Coilcraft ⁽¹⁾	Pulse ⁽²⁾	Renco ⁽³⁾	Schott ⁽⁴⁾	Schott ⁽⁴⁾ (Surface Mount)
DO3316-153	PE-53898	RL-5471-7	67146510	67146540

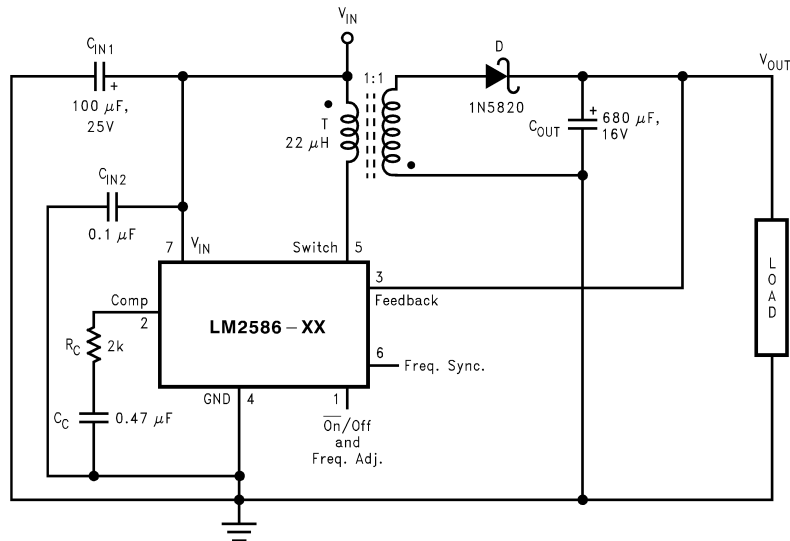
- (1) Coilcraft Inc., Phone: (800) 322-2645
1102 Silver Lake Road, Cary, IL 60013 Fax: (708) 639-1469
European Headquarters, 21 Napier Place Phone: +44 1236 730 595
Wardpark North, Cumbernauld, Scotland G68 0LL Fax: +44 1236 730 627
- (2) Pulse Engineering Inc., Phone: (619) 674-8100
12220 World Trade Drive, San Diego, CA 92128 Fax: (619) 674 -8262
European Headquarters, Dunmore Road Phone: +353 93 24 107
Tuam, Co. Galway, Ireland Fax: +353 93 24 459
- (3) Renco Electronics Inc., Phone: (800) 645-5828
60 Jeffrynn Blvd. East, Deer Park, NY 11729 Fax: (516) 586-5562
- (4) Schott Corp., Phone: (612) 475-1173
1000 Parkers Lane Road, Wayzata, MN 55391 Fax: (612) 475-1786

8.2.2.2 Detailed Design Procedure

See [Detailed Design Procedure](#)

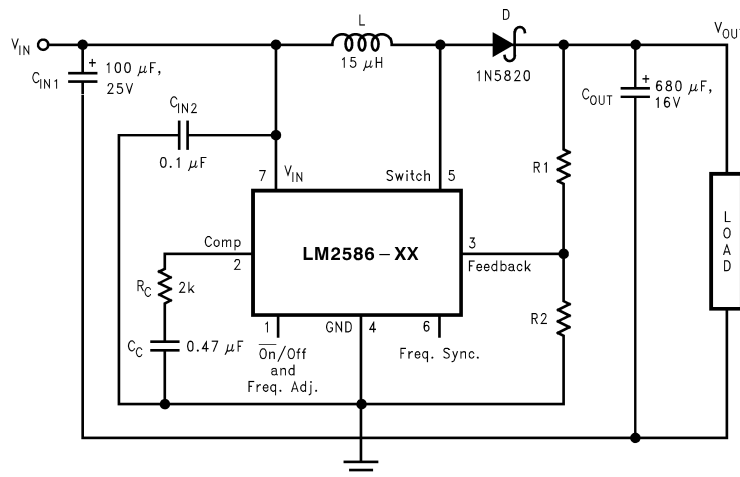
8.3 System Examples

8.3.1 Test Circuits



C_{IN1} —100 μ F, 25V Aluminum Electrolytic
 C_{IN2} —0.1 μ F Ceramic
 T —22 μ H, 1:1 Schott #67141450
 D —1N5820
 C_{OUT} —680 μ F, 16V Aluminum Electrolytic
 C_C —0.47 μ F Ceramic
 R_C —2k

Figure 54. 3.3-V LM2586 and 5-V LM2586

System Examples (continued)


C_{IN1} —100 μ F, 25V Aluminum Electrolytic

C_{IN2} —0.1 μ F Ceramic

L—15 μ H, Renco #RL-5472-5

D—1N5820

C_{OUT} —680 μ F, 16V Aluminum Electrolytic

C_C —0.47 μ F Ceramic

R_C —2k

For 12V Devices: $R1$ = Short (0 Ω) and 2 = Open

For ADJ Devices: $R1$ = 48.75k, $\pm 0.1\%$ and 2 = 5.62k, $\pm 0.1\%$

Figure 55. LM2586-12 and LM2586-ADJ

9 Layout

9.1 Layout Guidelines

As in any switching regulator, layout is very important. Rapidly switching currents associated with wiring inductance generate voltage transients which can cause problems. For minimal inductance and ground loops, keep the length of the leads and traces as short as possible. Use single point grounding or ground plane construction for best results. Separate the signal grounds from the power grounds (as indicated in Figure 56). When using the adjustable version, physically locate the programming resistors as close as possible to the regulator IC, to keep the sensitive feedback wiring short.

9.2 Layout Example

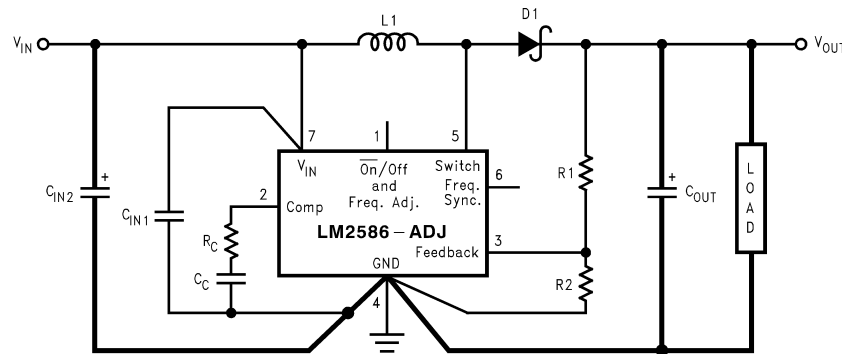


Figure 56. Circuit Board Layout

9.3 Heat Sink/Thermal Considerations

In many cases, a heat sink is not required to keep the LM2586 junction temperature within the allowed operating temperature range. For each application, to determine whether or not a heat sink will be required, the following must be identified:

- 1) Maximum ambient temperature (in the application).
- 2) Maximum regulator power dissipation (in the application).
- 3) Maximum allowed junction temperature (125°C for the LM2586). For a safe, conservative design, a temperature approximately 15°C cooler than the maximum junction temperature should be selected (110°C).
- 4) LM2586 package thermal resistances θ_{JA} and θ_{JC} (given in the Electrical Characteristics).

Total power dissipated (P_D) by the LM2586 can be estimated as follows:

Boost:

$$P_D = 0.15\Omega \cdot \left(\frac{I_{LOAD}}{1-D} \right)^2 \cdot D + \frac{I_{LOAD}}{50 \cdot (1-D)} \cdot D \cdot V_{IN}$$

Flyback:

$$P_D = 0.15\Omega \cdot \left(\frac{N \cdot \sum I_{LOAD}}{1-D} \right)^2 \cdot D + \frac{N \cdot \sum I_{LOAD}}{50 \cdot (1-D)} \cdot D \cdot V_{IN}$$

where

- V_{IN} is the minimum input voltage
- V_{OUT} is the output voltage
- N is the transformer turns ratio, D is the duty cycle
- I_{LOAD} is the maximum load current (and $\sum I_{LOAD}$ is the sum of the maximum load currents for multiple-output flyback regulators)

(7)

The duty cycle is given by:

Heat Sink/Thermal Considerations (continued)

Boost:

$$D = \frac{V_{OUT} + V_F - V_{IN}}{V_{OUT} + V_F - V_{SAT}} \approx \frac{V_{OUT} - V_{IN}}{V_{OUT}}$$

Flyback:

$$D = \frac{V_{OUT} + V_F}{N(V_{IN} - V_{SAT}) + V_{OUT} + V_F} \approx \frac{V_{OUT}}{N(V_{IN}) + V_{OUT}}$$

where

- V_F is the forward biased voltage of the diode and is typically 0.5 V for Schottky diodes and 0.8 V for fast recovery diodes
- V_{SAT} is the switch saturation voltage and can be found in the Characteristic Curves (8)

When no heat sink is used, the junction temperature rise is:

$$\Delta T_J = P_D \cdot \theta_{JA} \quad (9)$$

Adding the junction temperature rise to the maximum ambient temperature gives the actual operating junction temperature:

$$T_J = \Delta T_J + T_A \quad (10)$$

If the operating junction temperature exceeds the maximum junction temperature in item 3 above, then a heat sink is required. When using a heat sink, the junction temperature rise can be determined by the following:

$$\Delta T_J = P_D \cdot (\theta_{JC} + \theta_{Interface} + \theta_{Heat\ Sink}) \quad (11)$$

Again, the operating junction temperature will be:

$$T_J = \Delta T_J + T_A \quad (12)$$

As before, if the maximum junction temperature is exceeded, a larger heat sink is required (one that has a lower thermal resistance).

Included in the **Switchers Made Simple**® design software is a more precise (non-linear) thermal model that can be used to determine junction temperature with different input-output parameters or different component values. It can also calculate the heat sink thermal resistance required to maintain the regulator junction temperature below the maximum operating temperature.

*To further simplify the flyback regulator design procedure, Texas Instruments is making available computer design software to be used with the Simple Switcher® line of switching regulators. **Switchers Made Simple** is available on a 3½" diskette for IBM compatible computers from a Texas Instruments sales office in your area or the Texas Instruments Customer Response Center ((800) 477-8924).*

10 器件和文档支持

10.1 器件支持

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10.1.2 开发支持

10.1.2.1 使用 WEBENCH® 工具创建定制设计

单击[此处](#)，使用 LM2586 器件并借助 WEBENCH® 电源设计器创建定制设计方案。

1. 首先输入输入电压 (V_{IN})、输出电压 (V_{OUT}) 和输出电流 (I_{OUT}) 要求。
2. 使用优化器拨盘优化该设计的关键参数，如效率、尺寸和成本。
3. 将生成的设计与德州仪器 (TI) 的其他可行的解决方案进行比较。

WEBENCH 电源设计器可提供定制原理图以及罗列实时价格和组件供货情况的物料清单。

在多数情况下，可执行以下操作：

- 运行电气仿真，观察重要波形以及电路性能
- 运行热性能仿真，了解电路板热性能
- 将定制原理图和布局方案以常用 CAD 格式导出
- 打印设计方案的 PDF 报告并与同事共享

有关 WEBENCH 工具的详细信息，请访问 www.ti.com.cn/WBENCH。

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ESD 的损坏小至导致微小的性能降级，大至整个器件故障。精密的集成电路可能更容易受到损坏，这是因为非常细微的参数更改都可能会导致器件与其发布的规格不相符。

10.6 Glossary

[SLYZ022](#) — *TI Glossary*.

This glossary lists and explains terms, acronyms, and definitions.

11 机械、封装和可订购信息

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PACKAGING INFORMATION

Orderable Device	Status (1)	Package Type	Package Drawing	Pins	Package Qty	Eco Plan (2)	Lead/Ball Finish (6)	MSL Peak Temp (3)	Op Temp (°C)	Device Marking (4/5)	Samples
LM2586S-12/NOPB	ACTIVE	DDPAK/ TO-263	KTW	7	45	Green (RoHS & no Sb/Br)	SN	Level-3-245C-168 HR	-40 to 125	LM2586S -12 P+	Samples
LM2586S-3.3/NOPB	ACTIVE	DDPAK/ TO-263	KTW	7	45	Green (RoHS & no Sb/Br)	SN	Level-3-245C-168 HR	-40 to 125	LM2586S -3.3 P+	Samples
LM2586S-5.0/NOPB	ACTIVE	DDPAK/ TO-263	KTW	7	45	Green (RoHS & no Sb/Br)	SN	Level-3-245C-168 HR	-40 to 125	LM2586S -5.0 P+	Samples
LM2586S-ADJ/NOPB	ACTIVE	DDPAK/ TO-263	KTW	7	45	Green (RoHS & no Sb/Br)	SN	Level-3-245C-168 HR	-40 to 125	LM2586S -ADJ P+	Samples
LM2586SX-3.3/NOPB	ACTIVE	DDPAK/ TO-263	KTW	7	500	Green (RoHS & no Sb/Br)	SN	Level-3-245C-168 HR	-40 to 125	LM2586S -3.3 P+	Samples
LM2586SX-5.0/NOPB	ACTIVE	DDPAK/ TO-263	KTW	7	500	Green (RoHS & no Sb/Br)	SN	Level-3-245C-168 HR	-40 to 125	LM2586S -5.0 P+	Samples
LM2586SX-ADJ/NOPB	ACTIVE	DDPAK/ TO-263	KTW	7	500	Green (RoHS & no Sb/Br)	SN	Level-3-245C-168 HR	-40 to 125	LM2586S -ADJ P+	Samples
LM2586T-3.3/NOPB	ACTIVE	TO-220	NDZ	7	45	Green (RoHS & no Sb/Br)	SN	Level-1-NA-UNLIM	-40 to 125	LM2586T -3.3 P+	Samples
LM2586T-5.0/NOPB	ACTIVE	TO-220	NDZ	7	45	Green (RoHS & no Sb/Br)	SN	Level-1-NA-UNLIM	-40 to 125	LM2586T -5.0 P+	Samples
LM2586T-ADJ	NRND	TO-220	NDZ	7	45	TBD	Call TI	Call TI	-40 to 125	LM2586T -ADJ P+	
LM2586T-ADJ/NOPB	ACTIVE	TO-220	NDZ	7	45	Green (RoHS & no Sb/Br)	SN	Level-1-NA-UNLIM	-40 to 125	LM2586T -ADJ P+	Samples

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- ⁽⁴⁾ There may be additional marking, which relates to the logo, the lot trace code information, or the environmental category on the device.
- ⁽⁵⁾ Multiple Device Markings will be inside parentheses. Only one Device Marking contained in parentheses and separated by a "~" will appear on a device. If a line is indented then it is a continuation of the previous line and the two combined represent the entire Device Marking for that device.
- ⁽⁶⁾ Lead/Ball Finish - Orderable Devices may have multiple material finish options. Finish options are separated by a vertical ruled line. Lead/Ball Finish values may wrap to two lines if the finish value exceeds the maximum column width.

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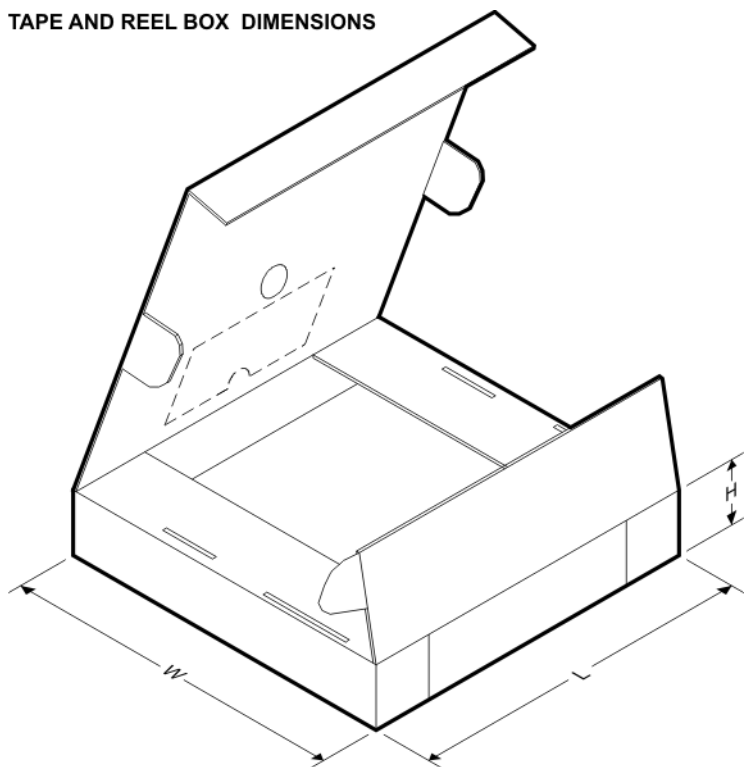
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*All dimensions are nominal

Device	Package Type	Package Drawing	Pins	SPQ	Reel Diameter (mm)	Reel Width W1 (mm)	A0 (mm)	B0 (mm)	K0 (mm)	P1 (mm)	W (mm)	Pin1 Quadrant
LM2586SX-3.3/NOPB	DDPAK/TO-263	KTW	7	500	330.0	24.4	10.75	14.85	5.0	16.0	24.0	Q2
LM2586SX-5.0/NOPB	DDPAK/TO-263	KTW	7	500	330.0	24.4	10.75	14.85	5.0	16.0	24.0	Q2
LM2586SX-ADJ/NOPB	DDPAK/TO-263	KTW	7	500	330.0	24.4	10.75	14.85	5.0	16.0	24.0	Q2

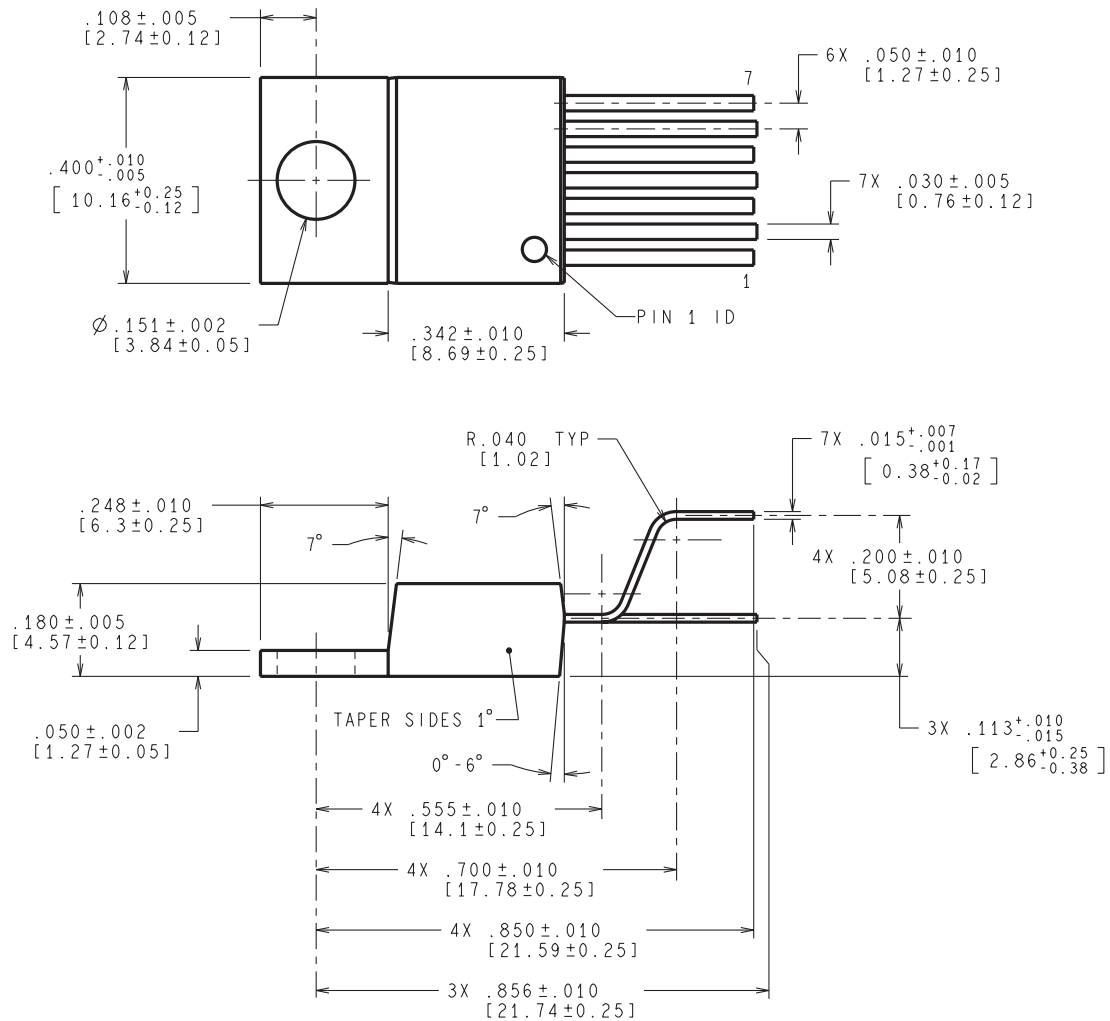
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*All dimensions are nominal

Device	Package Type	Package Drawing	Pins	SPQ	Length (mm)	Width (mm)	Height (mm)
LM2586SX-3.3/NOPB	DDPAK/TO-263	KTW	7	500	367.0	367.0	45.0
LM2586SX-5.0/NOPB	DDPAK/TO-263	KTW	7	500	367.0	367.0	45.0
LM2586SX-ADJ/NOPB	DDPAK/TO-263	KTW	7	500	367.0	367.0	45.0

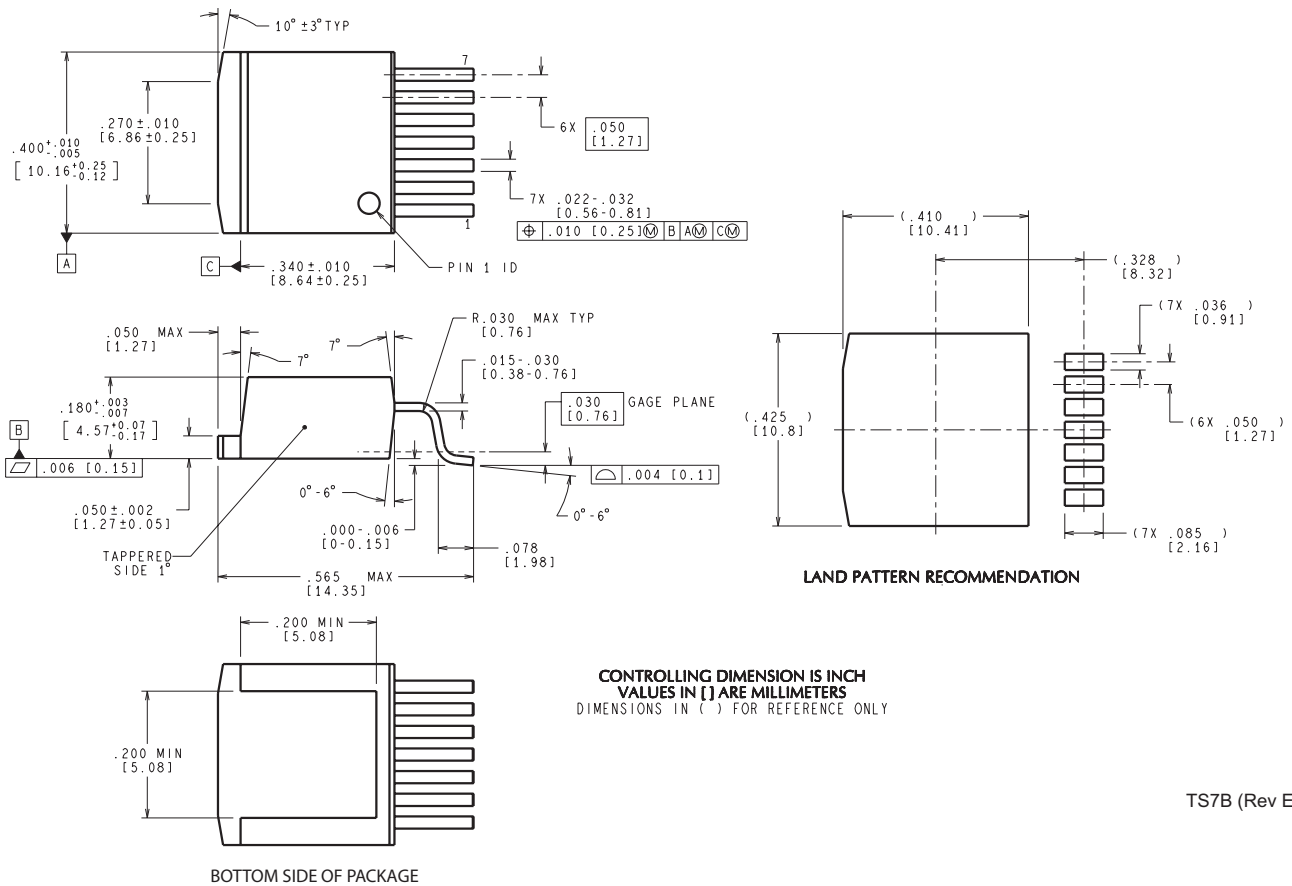
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KTW0007B



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