## FEATURES

## High speed

$730 \mathrm{MHz},-3 \mathrm{~dB}$ bandwidth
625 V/us slew rate
13 ns settling time to $0.5 \%$
Wide supply range: 5 V to 12 V
Low power: 6 mA/amplifier
0.1 dB flatness: 100 MHz

Differential gain: 0.01\%
Differential phase: $\mathbf{0 . 0 2}^{\circ}$
Low voltage offset: $\mathbf{1 0 0 ~} \boldsymbol{\mu \mathrm { V }}$ (typical)
High output current: 25 mA
Power down

## APPLICATIONS

## Consumer video

## Professional video

Broadband video
ADC buffers
Active filters

## GENERAL DESCRIPTION

The ADA4861-3 is a low cost, high speed, current feedback, triple op amp that provides excellent overall performance. The $730 \mathrm{MHz},-3 \mathrm{~dB}$ bandwidth, and $625 \mathrm{~V} / \mu \mathrm{s}$ slew rate make this amplifier well suited for many high speed applications. With its combination of low price, excellent differential gain ( $0.01 \%$ ), differential phase $\left(0.02^{\circ}\right)$, and 0.1 dB flatness out to 100 MHz , this amplifier is ideal for both consumer and professional video applications.

The ADA4861-3 is designed to operate on supply voltages as low as +5 V and up to $\pm 5 \mathrm{~V}$ using only $6 \mathrm{~mA} /$ amplifier of supply current. To further reduce power consumption, each amplifier is equipped with a power-down feature that lowers the supply current to $0.3 \mathrm{~mA} /$ amplifier when not being used.

The ADA4861-3 is available in a 14 -lead SOIC_N package and is designed to work over the extended temperature range of $-40^{\circ} \mathrm{C}$ to $+105^{\circ} \mathrm{C}$.


Figure 2. Large Signal $0.1 d B$ Flatness

Rev, A
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## ADA4861-3* Product Page Quick Links

Last Content Update: 11/01/2016

## Comparable Parts $\square$

View a parametric search of comparable parts

## Evaluation Kits

- ADA4861-3 Evaluation Board


## Documentation

## Data Sheet

- ADA4861-3: High Speed, Low Cost, Triple Op Amp Data Sheet


## Product Highlight

- Amplifier pricing where you want it,


## User Guides

- UG-114: Universal Evaluation Board for Triple, High Speed Op Amps Offered in 14-Lead SOIC Packages


## Tools and Simulations

- ADA4861 SPICE Macro Model


## Reference Materials <br> Informational

- Advantiv ${ }^{\text {TM }}$ Advanced TV Solutions

Product Selection Guide

- Amplifiers for Video Distribution
- High Speed Amplifiers Selection Table

Tutorials

- MT-034: Current Feedback (CFB) Op Amps
- MT-051: Current Feedback Op Amp Noise Considerations
- MT-057: High Speed Current Feedback Op Amps
- MT-059: Compensating for the Effects of Input Capacitance on VFB and CFB Op Amps Used in Current-to-Voltage Converters


## Design Resources $\square$

- ADA4861-3 Material Declaration
- PCN-PDN Information
- Quality And Reliability
- Symbols and Footprints


## Discussions

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## Sample and Buy $\square$

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[^0]
## ADA4861-3

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## SPECIFICATIONS

$V_{S}=+5 V\left(@ T_{A}=25^{\circ} \mathrm{C}, \mathrm{G}=+2, \mathrm{R}_{\mathrm{L}}=150 \Omega, \mathrm{C}_{\mathrm{L}}=4 \mathrm{pF}\right.$, unless otherwise noted); for $\mathrm{G}=+2, \mathrm{R}_{\mathrm{F}}=\mathrm{R}_{\mathrm{G}}=301 \Omega$; and for $\mathrm{G}=+1, \mathrm{R}_{\mathrm{F}}=499 \Omega$.
Table 1.

| Parameter | Conditions | Min | Typ | Max | Unit |
| :---: | :---: | :---: | :---: | :---: | :---: |
| DYNAMIC PERFORMANCE <br> -3 dB Bandwidth <br> Bandwidth for 0.1 dB Flatness <br> +Slew Rate (Rising Edge) <br> -Slew Rate (Falling Edge) <br> Settling Time to 0.5\% (Rise/Fall) | $\begin{aligned} & \mathrm{V}_{0}=0.2 \mathrm{~V} \text { p-p } \\ & \mathrm{V}_{\mathrm{o}}=2 \mathrm{~V} \text { p-p } \\ & \mathrm{G}=+1, \mathrm{~V}_{\mathrm{o}}=0.2 \mathrm{~V} \text { p-p } \\ & \mathrm{V}_{\mathrm{o}}=2 \mathrm{~V} \text { p-p } \\ & \mathrm{V}_{\mathrm{o}}=2 \mathrm{~V} \text { p-p } \\ & \mathrm{V}_{\mathrm{o}}=2 \mathrm{~V} \text { p-p } \\ & \mathrm{V}_{\mathrm{o}}=2 \mathrm{~V} \text { step } \end{aligned}$ |  | $\begin{aligned} & 350 \\ & 145 \\ & 560 \\ & 85 \\ & 590 \\ & 480 \\ & 12 / 13 \end{aligned}$ |  | MHz <br> MHz <br> MHz <br> MHz <br> V/ $\mu \mathrm{s}$ <br> V/us <br> ns |
| NOISE/DISTORTION PERFORMANCE <br> Harmonic Distortion HD2/HD3 <br> Harmonic Distortion HD2/HD3 <br> Input Voltage Noise <br> Input Current Noise <br> Differential Gain <br> Differential Phase <br> All-Hostile Crosstalk | $\begin{aligned} & \mathrm{f}_{\mathrm{c}}=1 \mathrm{MHz}, \mathrm{~V}_{\mathrm{o}}=2 \mathrm{Vp}-\mathrm{p} \\ & \mathrm{f}_{\mathrm{c}}=5 \mathrm{MHz}, \mathrm{~V}_{\mathrm{o}}=2 \mathrm{~V}-\mathrm{p} \\ & \mathrm{f}=100 \mathrm{kHz} \\ & \mathrm{f}=100 \mathrm{kHz},+\mathrm{IN} /-\mathrm{IN} \end{aligned}$ <br> Amplifier 1 and Amplifier 2 driven, Amplifier 3 output measured, $\mathrm{f}=1 \mathrm{MHz}$ |  | $-81 /-89$ $-69 /-76$ 3.8 $1.7 / 5.5$ 0.02 0.03 -65 |  | dBc <br> dBc <br> $\mathrm{nV} / \sqrt{ } \mathrm{Hz}$ <br> $\mathrm{pA} / \sqrt{ } \mathrm{Hz}$ <br> \% <br> Degrees <br> dB |
| DC PERFORMANCE <br> Input Offset Voltage <br> +Input Bias Current <br> -Input Bias Current <br> Open-Loop Transresistance |  | $\begin{aligned} & -13 \\ & -2 \\ & -8 \\ & 400 \end{aligned}$ | $\begin{aligned} & -0.9 \\ & -0.8 \\ & +2.3 \\ & 620 \end{aligned}$ | $\begin{aligned} & +13 \\ & +1 \\ & +13 \end{aligned}$ | $\begin{aligned} & \mathrm{mV} \\ & \mu \mathrm{~A} \\ & \mu \mathrm{~A} \\ & \mathrm{k} \Omega \end{aligned}$ |
| INPUT CHARACTERISTICS Input Resistance <br> Input Capacitance Input Common-Mode Voltage Range Common-Mode Rejection Ratio | $\begin{aligned} & +\mathrm{IN} \\ & -\mathrm{IN} \\ & +\mathrm{IN} \\ & \mathrm{G}=+1 \\ & \mathrm{~V}_{\mathrm{CM}}=2 \mathrm{~V} \text { to } 3 \mathrm{~V} \end{aligned}$ | $-54$ | $\begin{aligned} & 14 \\ & 85 \\ & 1.5 \\ & 1.2 \text { to } 3.8 \\ & -56.5 \end{aligned}$ |  | $\begin{aligned} & \mathrm{M} \Omega \\ & \Omega \\ & \mathrm{pF} \\ & \mathrm{~V} \\ & \mathrm{~dB} \end{aligned}$ |
| POWER-DOWN PINS <br> Input Voltage <br> Bias Current <br> Turn-On Time <br> Turn-Off Time | Enabled <br> Power down <br> Enabled <br> Power down |  | $\begin{aligned} & 0.6 \\ & 1.8 \\ & -3 \\ & 115 \\ & 200 \\ & 3.5 \\ & \hline \end{aligned}$ |  | $\begin{aligned} & \mathrm{V} \\ & \mathrm{~V} \\ & \mu \mathrm{~A} \\ & \mu \mathrm{~A} \\ & \mathrm{~ns} \\ & \mu \mathrm{~s} \\ & \hline \end{aligned}$ |
| OUTPUT CHARACTERISTICS <br> Output Overdrive Recovery Time (Rise/Fall) Output Voltage Swing <br> Short-Circuit Current | $\begin{aligned} & \mathrm{V}_{\mathrm{IN}}=+2.25 \mathrm{~V} \text { to }-0.25 \mathrm{~V} \\ & \mathrm{R}_{\mathrm{L}}=150 \Omega \\ & \mathrm{R}_{\mathrm{L}}=1 \mathrm{k} \Omega \end{aligned}$ <br> Sinking and sourcing | $\begin{aligned} & 1.2 \text { to } 3.8 \\ & 0.9 \text { to } 4.1 \end{aligned}$ | $\begin{aligned} & 55 / 100 \\ & 1.1 \text { to } 3.9 \\ & 0.85 \text { to } 4.15 \\ & 65 \end{aligned}$ |  | ns V V mA |
| POWER SUPPLY <br> Operating Range <br> Total Quiescent Current Quiescent Current/Amplifier Power Supply Rejection Ratio +PSR | Enabled <br> POWER DOWN pins $=+V_{s}$ $+\mathrm{V}_{\mathrm{s}}=4 \mathrm{~V} \text { to } 6 \mathrm{~V},-\mathrm{V}_{\mathrm{s}}=0 \mathrm{~V}$ | $\begin{aligned} & 5 \\ & 12.5 \\ & \\ & -60 \\ & \hline \end{aligned}$ | 16.1 <br> 0.2 $-64$ | $\begin{aligned} & 12 \\ & 18.5 \\ & 0.33 \end{aligned}$ | $\begin{aligned} & \mathrm{V} \\ & \mathrm{~mA} \\ & \mathrm{~mA} \\ & \mathrm{~dB} \end{aligned}$ |

## ADA4861-3

$V_{s}= \pm 5 \mathrm{~V}\left(@ T_{A}=25^{\circ} \mathrm{C}, \mathrm{G}=+2, \mathrm{R}_{\mathrm{L}}=150 \Omega, \mathrm{C}_{\mathrm{L}}=4 \mathrm{pF}\right.$, unless otherwise noted); for $\mathrm{G}=+2, \mathrm{R}_{\mathrm{F}}=\mathrm{R}_{\mathrm{G}}=301 \Omega$; and for $\mathrm{G}=+1, \mathrm{R}_{\mathrm{F}}=499 \Omega$.
Table 2.

| Parameter | Conditions | Min | Typ | Max | Unit |
| :---: | :---: | :---: | :---: | :---: | :---: |
| DYNAMIC PERFORMANCE <br> -3 dB Bandwidth <br> Bandwidth for 0.1 dB Flatness <br> +Slew Rate (Rising Edge) <br> -Slew Rate (Falling Edge) <br> Settling Time to $0.5 \%$ (Rise/Fall) | $\begin{aligned} & \mathrm{V}_{\mathrm{o}}=0.2 \mathrm{~V} \text { p-p } \\ & \mathrm{V}_{\mathrm{o}}=2 \mathrm{~V} \text { p-p } \\ & \mathrm{G}=+1, \mathrm{~V} \text { o }=0.2 \mathrm{~V} \text { p-p } \\ & \mathrm{V}_{\mathrm{o}}=2 \mathrm{~V} \text { p-p } \\ & \mathrm{V}_{\mathrm{o}}=2 \mathrm{~V} \text { p-p } \\ & \mathrm{V}_{\mathrm{o}}=2 \mathrm{~V} \text { p-p } \\ & \mathrm{V}_{\mathrm{o}}=2 \mathrm{~V} \text { step } \end{aligned}$ |  | $\begin{aligned} & 370 \\ & 210 \\ & 730 \\ & 100 \\ & 910 \\ & 680 \\ & 12 / 13 \end{aligned}$ |  | MHz <br> MHz <br> MHz <br> MHz <br> V/ $\mu \mathrm{s}$ <br> V/ $\mu \mathrm{s}$ <br> ns |
| NOISE/DISTORTION PERFORMANCE <br> Harmonic Distortion HD2/HD3 <br> Harmonic Distortion HD2/HD3 <br> Input Voltage Noise <br> Input Current Noise <br> Differential Gain <br> Differential Phase <br> All-Hostile Crosstalk | $\begin{aligned} & \mathrm{f}_{\mathrm{c}}=1 \mathrm{MHz}, \mathrm{~V}_{\mathrm{o}}=2 \mathrm{~V} p-\mathrm{p} \\ & \mathrm{f}_{\mathrm{c}}=5 \mathrm{MHz}, \mathrm{~V}_{\mathrm{o}}=2 \mathrm{~V} \mathrm{p}-\mathrm{p} \\ & \mathrm{f}=100 \mathrm{kHz} \\ & \mathrm{f}=100 \mathrm{kHz},+\mathrm{IN} /-\mathrm{IN} \end{aligned}$ <br> Amplifier 1 and Amplifier 2 driven, Amplifier 3 output measured, $\mathrm{f}=1 \mathrm{MHz}$ |  | $\begin{aligned} & -85 /-99 \\ & -73 /-86 \\ & 3.8 \\ & 1.7 / 5.5 \\ & 0.01 \\ & 0.02 \\ & -65 \end{aligned}$ |  | dBc <br> dBc <br> $\mathrm{nV} / \sqrt{ } \mathrm{Hz}$ <br> $\mathrm{pA} / \sqrt{ } \mathrm{Hz}$ <br> \% <br> Degrees <br> dB |
| DC PERFORMANCE <br> Input Offset Voltage <br> +Input Bias Current <br> -Input Bias Current <br> Open-Loop Transresistance |  | $\begin{aligned} & -13 \\ & -2 \\ & -8 \\ & 500 \end{aligned}$ | $\begin{aligned} & -0.1 \\ & -0.7 \\ & +2.9 \\ & 720 \end{aligned}$ | $\begin{aligned} & +13 \\ & +1 \\ & +13 \end{aligned}$ | $\begin{aligned} & \mathrm{mV} \\ & \mu \mathrm{~A} \\ & \mu \mathrm{~A} \\ & \mathrm{k} \Omega \end{aligned}$ |
| INPUT CHARACTERISTICS <br> Input Resistance <br> Input Capacitance <br> Input Common-Mode Voltage Range <br> Common-Mode Rejection Ratio | $\begin{aligned} & +\mathrm{IN} \\ & -\mathrm{IN} \\ & +\mathbb{N} \\ & \mathrm{G}=+1 \\ & \mathrm{~V}_{\mathrm{CM}}= \pm 2 \mathrm{~V} \end{aligned}$ | -55 | $\begin{aligned} & 15 \\ & 90 \\ & 1.5 \\ & -3.7 \text { to }+3.7 \\ & -58 \end{aligned}$ |  | $\begin{aligned} & \mathrm{M} \Omega \\ & \Omega \\ & \mathrm{pF} \\ & \mathrm{~V} \\ & \mathrm{~dB} \end{aligned}$ |
| POWER-DOWN PINS Input Voltage <br> Bias Current <br> Turn-On Time Turn-Off Time | Enabled <br> Power down <br> Enabled <br> Power down |  | $\begin{aligned} & -4.4 \\ & -3.2 \\ & -3 \\ & 250 \\ & 200 \\ & 3.5 \end{aligned}$ |  |  |
| OUTPUT CHARACTERISTICS <br> Output Overdrive Recovery Time (Rise/Fall) Output Voltage Swing <br> Short-Circuit Current | $\begin{aligned} & \mathrm{V}_{\mathbb{I}}= \pm 3.0 \mathrm{~V} \\ & \mathrm{R}_{\mathrm{L}}=150 \Omega \\ & \mathrm{R}_{\mathrm{L}}=1 \mathrm{k} \Omega \end{aligned}$ <br> Sinking and sourcing | $\begin{aligned} & \pm 2 \\ & \pm 3.9 \end{aligned}$ | $\begin{aligned} & 30 / 90 \\ & -3.1 \text { to }+3.65 \\ & \pm 4.05 \\ & 100 \end{aligned}$ |  | ns <br> V <br> V <br> mA |
| POWER SUPPLY <br> Operating Range <br> Total Quiescent Current <br> Quiescent Current/Amplifier <br> Power Supply Rejection Ratio $\begin{aligned} & \text { +PSR } \\ & \text {-PSR } \end{aligned}$ | Enabled <br> POWER DOWN pins $=+V_{s}$ $\begin{aligned} & +V_{s}=4 \mathrm{~V} \text { to } 6 \mathrm{~V},-\mathrm{V}_{\mathrm{s}}=-5 \mathrm{~V} \\ & +\mathrm{V}_{\mathrm{s}}=5 \mathrm{~V},-\mathrm{V}_{\mathrm{s}}=-4 \mathrm{~V} \text { to }-6 \mathrm{~V}, \end{aligned}$ $\text { POWER DOWN pins }=-V_{s}$ | $\begin{aligned} & 5 \\ & 13.5 \\ & \\ & -63 \\ & -59 \end{aligned}$ | $\begin{aligned} & 17.9 \\ & 0.3 \\ & \\ & -66 \\ & -62 \end{aligned}$ | $\begin{aligned} & 12 \\ & 20.5 \\ & 0.5 \end{aligned}$ | $\begin{aligned} & \mathrm{V} \\ & \mathrm{~mA} \\ & \mathrm{~mA} \\ & \mathrm{~dB} \\ & \mathrm{~dB} \end{aligned}$ |

## ABSOLUTE MAXIMUM RATINGS

Table 3.

| Parameter | Rating |
| :--- | :--- |
| Supply Voltage | 12.6 V |
| Power Dissipation | See Figure 3 |
| Common-Mode Input Voltage | $-\mathrm{V}_{\mathrm{S}}+1 \mathrm{~V}$ to $+\mathrm{V}_{\mathrm{S}}-1 \mathrm{~V}$ |
| Differential Input Voltage | $\pm \mathrm{V}_{\mathrm{S}}$ |
| Storage Temperature | $-65^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ |
| Operating Temperature Range | $-40^{\circ} \mathrm{C}$ to $+105^{\circ} \mathrm{C}$ |
| Lead Temperature | $\mathrm{JEDEC} \mathrm{J}-$ STD -20 |
| Junction Temperature | $150^{\circ} \mathrm{C}$ |

Stresses above those listed under Absolute Maximum Ratings may cause permanent damage to the device. This is a stress rating only; functional operation of the device at these or any other conditions above those indicated in the operational section of this specification is not implied. Exposure to absolute maximum rating conditions for extended periods may affect device reliability.

## THERMAL RESISTANCE

$\theta_{\text {JA }}$ is specified for the worst-case conditions, that is, $\theta_{\text {JA }}$ is specified for device soldered in circuit board for surface-mount packages.
Table 4. Thermal Resistance

| Package Type | $\boldsymbol{\theta}_{\mathrm{JA}}$ | Unit |
| :--- | :--- | :--- |
| 14-lead SOIC_N | 90 | ${ }^{\circ} \mathrm{C} / \mathrm{W}$ |

## Maximum Power Dissipation

The maximum safe power dissipation for the ADA4861-3 is limited by the associated rise in junction temperature $\left(\mathrm{T}_{\mathrm{J}}\right)$ on the die. At approximately $150^{\circ} \mathrm{C}$, which is the glass transition temperature, the plastic changes its properties. Even temporarily exceeding this temperature limit can change the stresses that the package exerts on the die, permanently shifting the parametric performance of the amplifiers. Exceeding a junction temperature of $150^{\circ} \mathrm{C}$ for an extended period can result in changes in silicon devices, potentially causing degradation or loss of functionality.

The power dissipated in the package $\left(\mathrm{P}_{\mathrm{D}}\right)$ is the sum of the quiescent power dissipation and the power dissipated in the die due to the amplifiers' drive at the output. The quiescent power is the voltage between the supply pins $\left(\mathrm{V}_{\mathrm{s}}\right)$ times the quiescent current (Is).

$$
\begin{aligned}
P_{D} & =\text { Quiescent Power }+(\text { Total Drive Power }- \text { Load Power }) \\
P_{D} & =\left(V_{S} \times I_{S}\right)+\left(\frac{V_{S}}{2} \times \frac{V_{\text {OUT }}}{R_{L}}\right)-\frac{V_{\text {OUT }}{ }^{2}}{R_{L}}
\end{aligned}
$$

RMS output voltages should be considered.
Airflow increases heat dissipation, effectively reducing $\theta_{\mathrm{IA}}$. In addition, more metal directly in contact with the package leads and through holes under the device reduces $\theta_{J A}$.

Figure 3 shows the maximum safe power dissipation in the package vs. the ambient temperature for the 14-lead SOIC_N $\left(90^{\circ} \mathrm{C} / \mathrm{W}\right)$ on a JEDEC standard 4-layer board. $\theta_{\mathrm{JA}}$ values are approximations.


Figure 3. Maximum Power Dissipation vs. Temperature for a 4-Layer Board

## ESD CAUTION

ESD (electrostatic discharge) sensitive device. Electrostatic charges as high as 4000 V readily accumulate on the human body and test equipment and can discharge without detection. Although this product features proprietary ESD protection circuitry, permanent damage may occur on devices subjected to high energy electrostatic discharges. Therefore, proper ESD precautions are recommended to avoid performance degradation or loss of functionality.

## ADA4861-3

## TYPICAL PERFORMANCE CHARACTERISTICS

$\mathrm{R}_{\mathrm{L}}=150 \Omega$ and $\mathrm{C}_{\mathrm{L}}=4 \mathrm{pF}$, unless otherwise noted.


Figure 4. Small Signal Frequency Response for Various Gains


Figure 5. Large Signal Frequency Response for Various Gains


Figure 6. Large Signal $0.1 d B$ Flatness


Figure 7. Small Signal Frequency Response for Various Gains


Figure 8. Large Signal Frequency Response for Various Gains


Figure 9. Large Signal Frequency Response for Various Output Levels


Figure 10. Small Signal Frequency Response vs. $R_{F}$


Figure 11. Harmonic Distortion vs. Frequency


Figure 12. Harmonic Distortion vs. Frequency


Figure 13. Large Signal Frequency Response vs. $R_{F}$


Figure 14. Harmonic Distortion vs. Frequency


Figure 15. Harmonic Distortion vs. Frequency


Figure 16. Small Signal Transient Response for Various Supplies


Figure 17. Small Signal Transient Response for Various Capacitor Loads


Figure 18. Small Signal Transient Response for Various Capacitor Loads


Figure 19. Small Signal Transient Response for Various Supplies


Figure 20. Small Signal Transient Response for Various Capacitor Loads


Figure 21. Small Signal Transient Response for Various Capacitor Loads


Figure 22. Large Signal Transient Response for Various Supplies


Figure 23. Large Signal Transient Response for Various Capacitor Loads


Figure 24. Large Signal Transient Response for Various Capacitor Loads


Figure 25. Large Signal Transient Response for Various Supplies


Figure 26. Large Signal Transient Response for Various Capacitor Loads


Figure 27. Large Signal Transient Response for Various Capacitor Loads

## ADA4861-3



Figure 28. Slew Rate vs. Input Voltage


Figure 29. Slew Rate vs. Input Voltage


Figure 30. Settling Time Rising Edge


Figure 31. Slew Rate vs. Input Voltage


Figure 32. Slew Rate vs. Input Voltage


Figure 33. Settling Time Falling Edge


Figure 34. Transimpedance and Phase vs. Frequency


Figure 35. Power Supply Rejection vs. Frequency


Figure 36. Output Overdrive Recovery


Figure 37. Large Signal All-Hostile Crosstalk


Figure 38. Common-Mode Rejection vs. Frequency


Figure 39. Output Overdrive Recovery


Figure 40. Input Voltage Noise vs. Frequency


Figure 41. Total Supply Current vs. Supply Voltage


Figure 42. Input Vos vs. Common-Mode Voltage


Figure 43. Input Current Noise vs. Frequency


Figure 44. Total Supply Current at Various Supplies vs. Temperature


Figure 45. Input Bias Current vs. Output Voltage

## APPLICATIONS

## GAIN CONFIGURATIONS

Unlike conventional voltage feedback amplifiers, the feedback resistor has a direct impact on the closed-loop bandwidth and stability of the current feedback op amp circuit. Reducing the resistance below the recommended value can make the amplifier response peak and even become unstable. Increasing the size of the feedback resistor reduces the closed-loop bandwidth. Table 5 provides a convenient reference for quickly determining the feedback and gain set resistor values and bandwidth for common gain configurations.
Table 5. Recommended Values and Frequency Performance ${ }^{1}$

|  |  |  |  | Large Signal <br> Gain |
| :--- | :--- | :--- | :--- | :--- |
| $\mathbf{R F}_{\mathbf{F}}(\boldsymbol{\Omega})$ | $\mathbf{R G}_{\mathbf{G}}(\boldsymbol{\Omega})$ | $\mathbf{- 3} \mathbf{~ d B} \mathbf{S S} \mathbf{B W}(\mathbf{M H z})$ | $\mathbf{0 . 1} \mathbf{d B}$ Flatness |  |

${ }^{1}$ Conditions: $\mathrm{V}_{\mathrm{S}}= \pm 5 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C}, \mathrm{R}_{\mathrm{L}}=150 \Omega$.
Figure 46 and Figure 47 show the typical noninverting and inverting configurations and recommended bypass capacitor values.


Figure 47. Inverting Gain

## 20 MHz ACTIVE LOW-PASS FILTER

The ADA4861-3 triple amplifier lends itself to higher order active filters. Figure 48 shows a $28 \mathrm{MHz}, 6$-pole, Sallen-Key low-pass filter.


Figure 48. 28 MHz, 6-Pole Low-Pass Filter
The filter has a gain of approximately 23 dB and flat frequency response out to 22 MHz . This type of filter is commonly used at the output of a video DAC as a reconstruction filter. The frequency response of the filter is shown in Figure 49.


Figure 49. 20 MHz Low-Pass Filter Frequency Response

## ADA4861-3

## RGB VIDEO DRIVER

Figure 50 shows a typical RGB driver application using bipolar supplies. The gain of the amplifier is set at +2 , where $R_{F}=R_{G}=$ $301 \Omega$. The amplifier inputs are terminated with shunt $75 \Omega$ resistors, and the outputs have series $75 \Omega$ resistors for proper video matching. In Figure 50, the POWER-DOWN pins are not shown connected to any signal source for simplicity. If the power-down function is not used, it is recommended that the power-down pins be tied to the negative supply and not be left floating (not connected).

For applications that require a fixed gain of +2 , consider using the ADA4862-3 with integrated $\mathrm{R}_{\mathrm{F}}$ and $\mathrm{R}_{\mathrm{G}}$. The ADA4862-3 is another high performance triple current feedback amplifier that can simplify design and reduce board area.


Figure 50. RGB Video Driver

## DRIVING TWO VIDEO LOADS

In applications that require two video loads be driven simultaneously, the ADA4861-3 can deliver. Figure 51 shows the ADA4861-3 configured with dual video loads. Figure 52 shows the dual video load 0.1 dB bandwidth performance.


Figure 51. Video Driver Schematic for Two Video Loads


Figure 52. Large Signal Frequency Response for Various Supplies, $R_{L}=75 \Omega$

## POWER-DOWN PINS

The ADA4861-3 is equipped with three independent POWER DOWN pins, one for each amplifier. This allows the user the ability to reduce the quiescent supply current when an amplifier is inactive. The power-down threshold levels are derived from the voltage applied to the $-\mathrm{V}_{s}$ pin. When used in single-supply applications, this is especially useful with conventional logic levels. The amplifier is powered down when the voltage applied to the POWER DOWN pins is greater than $-\mathrm{V}_{\mathrm{s}}+1 \mathrm{~V}$. In a single-supply application, this is $>+1 \mathrm{~V}$ (that is, $0 \mathrm{~V}+1 \mathrm{~V}$ ), in a $\pm 5 \mathrm{~V}$ supply application, the voltage is $>-4 \mathrm{~V}$. The amplifier is enabled whenever the POWER DOWN pins are left either open or the voltage on the POWER DOWN pins is lower than 1 V above -V . If the POWER DOWN pins are not used, it is best to connect them to the negative supply.

## SINGLE-SUPPLY OPERATION

The ADA4861-3 can also be operated from a single power supply. Figure 53 shows the schematic for a single 5 V supply video driver. The input signal is ac-coupled into the amplifier via C1. Resistor R2 and Resistor R4 establish the input midsupply reference for the amplifier. Capacitor C5 prevents constant current from being drawn through the gain set resistor and enables the ADA4861-3 at dc to provide unity gain to the input midsupply voltage, thereby establishing the output voltage dc operating point. Capacitor C6 is the output coupling capacitor. For more information on single-supply operation of op amps, see www.analog.com/library/analogDialogue/archives/3502/avoiding/.


Figure 53. Single-Supply Video Driver Schematic

## POWER SUPPLY BYPASSING

Careful attention must be paid to bypassing the power supply pins of the ADA4861-3. High quality capacitors with low equivalent series resistance (ESR), such as multilayer ceramic capacitors (MLCCs), should be used to minimize supply voltage ripple and power dissipation. A large, usually tantalum, $2.2 \mu \mathrm{~F}$ to $47 \mu \mathrm{~F}$ capacitor located in proximity to the ADA4861-3 is required to provide good decoupling for lower frequency signals. The actual value is determined by the circuit transient and frequency requirements. In addition, $0.1 \mu \mathrm{~F}$ MLCC decoupling capacitors should be located as close to each of the power supply pins as is physically possible, no more than $1 / 8$ inch away. The ground returns should terminate immediately into the ground plane. Locating the bypass capacitor return close to the load return minimizes ground loops and improves performance.

## LAYOUT

As is the case with all high-speed applications, careful attention to printed circuit board (PCB) layout details prevents associated board parasitics from becoming problematic. The ADA4861-3 can operate at up to 730 MHz ; therefore, proper RF design techniques must be employed. The PCB should have a ground plane covering all unused portions of the component side of the board to provide a low impedance return path. Removing the ground plane on all layers from the area near and under the input and output pins reduces stray capacitance. Signal lines connecting the feedback and gain resistors should be kept as short as possible to minimize the inductance and stray capacitance associated with these traces. Termination resistors and loads should be located as close as possible to their respective inputs and outputs. Input and output traces should be kept as far apart as possible to minimize coupling (crosstalk) through the board. Adherence to microstrip or stripline design techniques for long signal traces (greater than 1 inch ) is recommended. For more information on high speed board layout, go to: www.analog.com and www.analog.com/library/analogDialogue/archives/3909/layout.html.

## ADA4861-3

## OUTLINE DIMENSIONS



| Model | Temperature Range | Package Description | Package Option | Ordering Quantity |
| :---: | :---: | :---: | :---: | :---: |
| ADA4861-3YRZ ${ }^{1}$ | $-40^{\circ} \mathrm{C}$ to $+105^{\circ} \mathrm{C}$ | 14-Lead SOIC_N | R-14 | 1 |
| ADA4861-3YRZ-RL ${ }^{1}$ | $-40^{\circ} \mathrm{C}$ to $+105^{\circ} \mathrm{C}$ | 14-Lead SOIC_N | R-14 | 2,500 |
| ADA4861-3YRZ-RL7 ${ }^{1}$ | $-40^{\circ} \mathrm{C}$ to $+105^{\circ} \mathrm{C}$ | 14-Lead SOIC_N | R-14 | 1,000 |

${ }^{1} \mathrm{Z}=\mathrm{Pb}$-free part.


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