

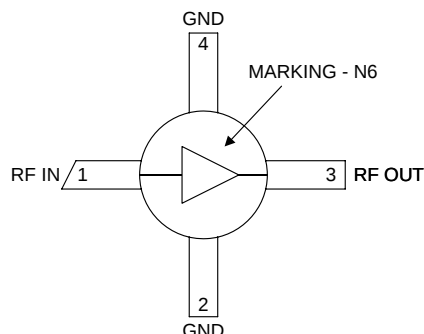


Features

- Reliable, Low-Cost HBT Design
- 12.7 dB Gain, +12.6dBm P1dB@2GHz
- High P1dB of +14.9dBm@6.0GHz and +13.1dBm@10.0GHz
- Single Power Supply Operation
- 50Ω I/O Matched for High Freq. Use

Applications

- Narrow and Broadband Commercial and Military Radio Designs
- Linear and Saturated Amplifiers
- Gain Stage or Driver Amplifiers for MWRadio/Optical Designs (PTP/PMP/LMDS/UNII/VSAT/WLAN/Cellular/DWDM)



Functional Block Diagram

Product Description

The NLB-310 cascadable broadband InGaP/GaAs MMIC amplifier is a low-cost, high-performance solution for general purpose RF and microwave amplification needs. This 50Ω gain block is based on a reliable HBT proprietary MMIC design, providing unsurpassed performance for small-signal applications. Designed with an external bias resistor, the NLB-310 provides flexibility and stability. The NLB-310 is packaged in a low-cost, surface-mount plastic package, providing ease of assembly for high-volume tape-and-reel requirements.

Ordering Information

NLB-310	Cascadable Broadband GaAs MMIC Amplifier DC to 10GHz
NLB-310-T1	Tape & Reel, 1000 Pieces
NLB-310-E	Fully Assembled Evaluation Board
NBB-X-K1	Extended Frequency InGaP Amp Designer's Tool Kit

Optimum Technology Matching® Applied

- | | | | |
|---|--------------------------------------|-------------------------------------|-----------------------------------|
| ☐ GaAs HBT | ☐ SiGe BiCMOS | ☐ GaAs pHEMT | ☐ GaN HEMT |
| ☐ GaAs MESFET | ☐ Si BiCMOS | ☐ Si CMOS | ☐ RF MEMS |
| ☒ InGaP HBT | ☐ SiGe HBT | ☐ Si BJT | |

Absolute Maximum Ratings

Parameter	Rating	Unit
RF Input Power	+20	dBm
Power Dissipation	300	mW
Device Current	70	mA
Channel Temperature	200	°C
Operating Temperature	-45 to +85	°C
Storage Temperature	-65 to +150	°C

Exceeding any one or a combination of these limits may cause permanent damage.

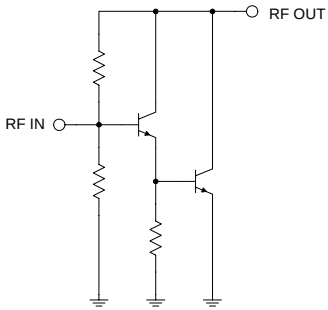


Caution! ESD sensitive device.

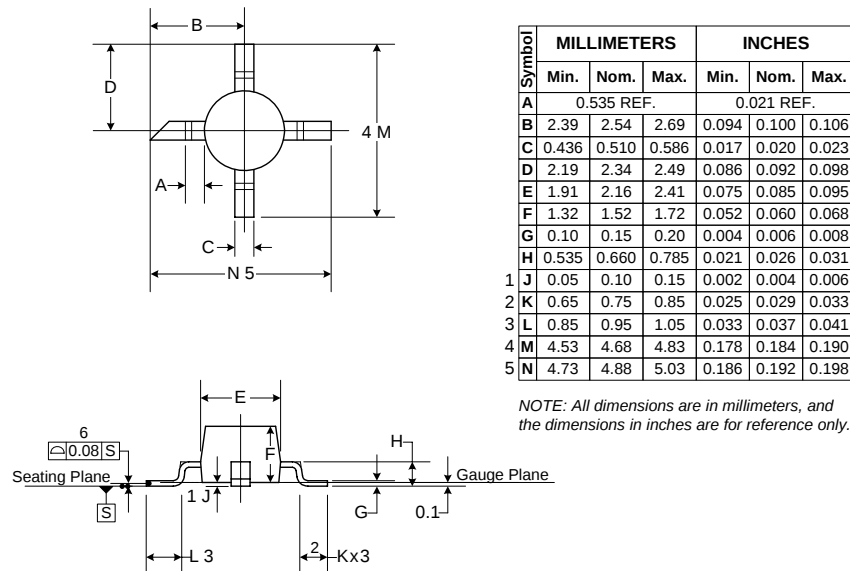
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RoHS status based on EUDirective2002/95/EC (at time of this document revision).

Parameter	Specification			Unit	Condition
	Min.	Typ.	Max.		
Overall					$V_D = +4.6V$, $I_{CC} = 50mA$, $Z_0 = 50\Omega$, $T_A = +25^\circ C$
Small Signal Power Gain, S21	12.0	12.7		dB	f=0.1GHz to 1.0GHz
		10.7		dB	f=1.0GHz to 4.0GHz
		10.0		dB	f=4.0GHz to 6.0GHz
	8.5	9.7		dB	f=6.0GHz to 10.0GHz
		9.6		dB	f=10.0GHz to 12.0GHz
Gain Flatness, GF		± 0.3		dB	f=5.0GHz to 10.0GHz
Input VSWR		1.6:1			f=0.1GHz to 4.0GHz
		1.75:1			f=4.0GHz to 7.0GHz
		1.6:1			f=7.0GHz to 11.0GHz
Output VSWR		1.5:1			f=0.1GHz to 4.0GHz
		1.8:1			f=4.0GHz to 7.0GHz
		1.6:1			f=7.0GHz to 11.0GHz
Output Power @ -1dB Compression, P1dB		12.6		dBm	f=2.0GHz
		14.9		dBm	f=6.0GHz
		13.1		dBm	f=10.0GHz
Noise Figure, NF		5.0		dB	f=3.0GHz
Third Order Intercept, IP3		+28.9		dBm	f=2.0GHz
		+27.9			f=6.0GHz
Reverse Isolation, S12		-17		dB	f=0.1GHz to 20.0GHz
Device Voltage, V_D	4.4	4.6	4.8	V	
Gain Temperature Coefficient, $\delta G_T / \delta T$		-0.0015		dB/°C	
MTTF versus Temperature @ $I_{CC} = 50mA$					
Case Temperature		85		°C	
Junction Temperature		125		°C	
MTTF		>1,000,000		hours	
Thermal Resistance					
θ_{JC}		174		°C/W	$\frac{J_T - T_{CASE}}{V_D \cdot I_{CC}} = \theta_{JC} (^\circ C / Watt)$

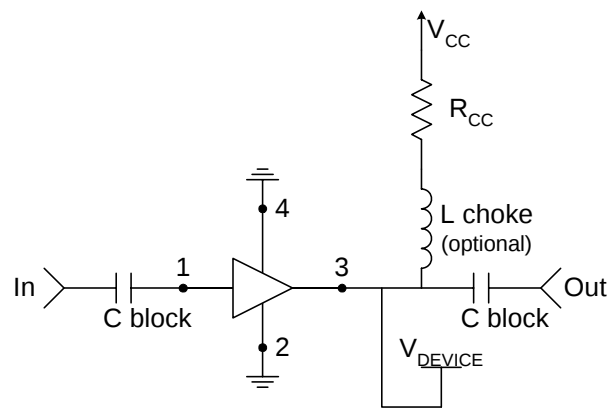
Pin	Function	Description	Interface Schematic
1	RF IN	RF input pin. This pin is NOT internally DC blocked. A DC blocking capacitor, suitable for the frequency of operation, should be used in most applications. DC coupling of the input is not allowed, because this will override the internal feedback loop and cause temperature instability.	
2	GND	Ground connection. For best performance, keep traces physically short and connect immediately to ground plane.	
3	RF OUT	RF output and bias pin. Biasing is accomplished with an external series resistor and choke inductor to V_{CC}. The resistor is selected to set the DC current into this pin to a desired level. The resistor value is determined by the following equation: $R = \frac{(V_{CC} - V_{DEVICE})}{I_{CC}}$ Care should also be taken in the resistor selection to ensure that the current into the part never exceeds maximum datasheet operating current over the planned operating temperature. This means that a resistor between the supply and this pin is always required, even if a supply near 5.0V is available, to provide DC feedback to prevent thermal runaway. Because DC is present on this pin, a DC blocking capacitor, suitable for the frequency of operation, should be used in most applications. The supply side of the bias network should also be well bypassed.	
4	GND	Same as pin 2.	

Package Drawing



Typical Bias Configuration

Application notes related to biasing circuit, device footprint, and thermal considerations are available on request.

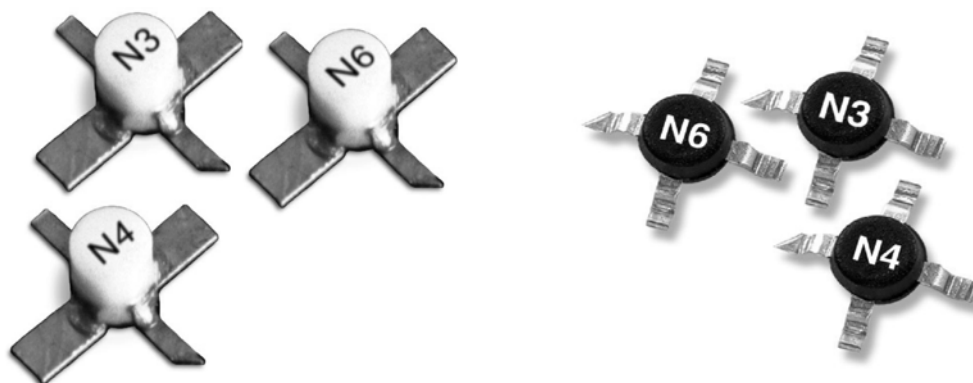


Recommended Bias Resistor Values					
Supply Voltage, V_{CC} (V)	8	10	12	15	20
Bias Resistor, R_{CC} (Ω)	60	100	140	200	300

Extended Frequency InGaP Amplifier Designer's Tool Kit NBB-X-K1

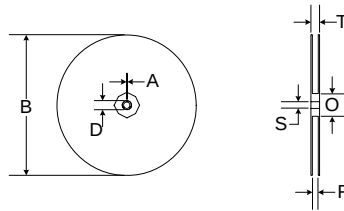
This tool kit was created to assist in the design-in of the RFMD NBB- and NLB-series InGaP HBT gain block amplifiers. Each tool kit contains the following.

- 5 each NBB-300, NBB-310 and NBB-400 Ceramic Micro-X Amplifiers
- 5 each NLB-300, NLB-310 and NLB-400 Plastic Micro-X Amplifiers
- 2 Broadband Evaluation Boards and High Frequency SMA Connectors
- Broadband Bias Instructions and Specification Summary Index for ease of operation

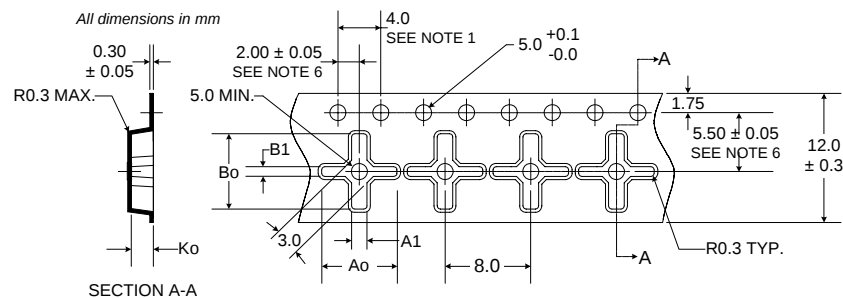
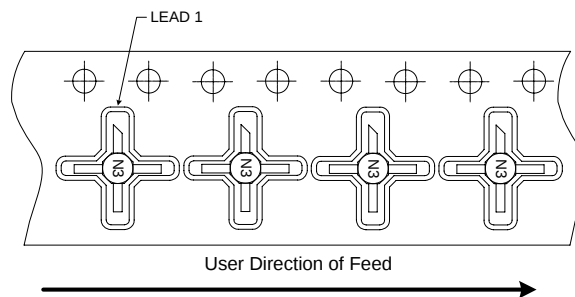


Tape and Reel Dimensions

All Dimensions in Millimeters



14.732 mm (7") REEL			Plastic, Micro-X	
	ITEMS	SYMBOL	SIZE (mm)	SIZE (inches)
FLANGE	Diameter	B	178 +0.25/-4.0	7.0 +0.079/-0.158
	Thickness	T	18.4 MAX	0.724 MAX
	Space Between Flange	F	12.8 +2.0	0.50 +0.08
HUB	Outer Diameter	O	76.2 REF	3.0 REF
	Spindle Hole Diameter	S	13.716 +0.5/-0.2	0.540 +0.020/-0.008
	Key Slit Width	A	1.5 MIN	0.059 MIN
	Key Slit Diameter	D	20.2 MIN	0.795 MIN

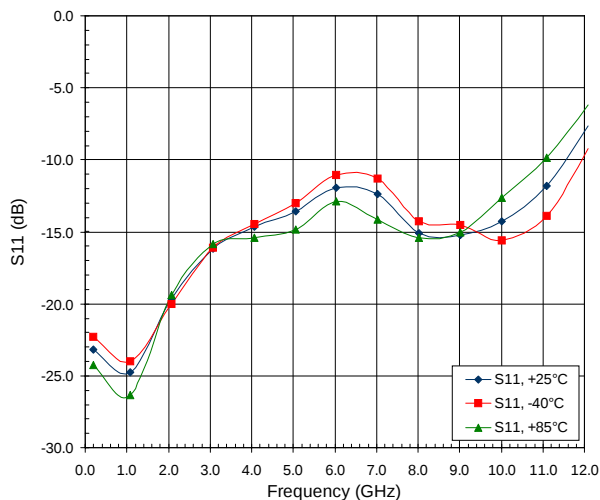


NOTES:

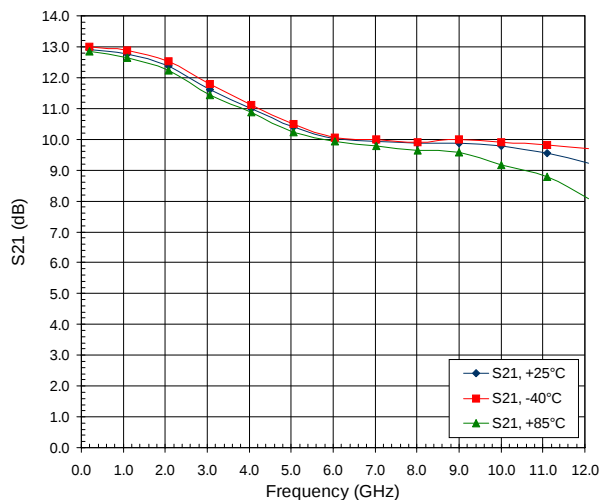
1. 10 sprocket hole pitch cumulative tolerance ± 0.2 .
2. Camber not to exceed 1 mm in 100 mm.
3. Material: PS+C.
4. Ao and Bo measured on a plane 0.3 mm above the bottom of the pocket.
5. Ko measured from a plane on the inside bottom of the pocket to the surface of the carrier.
6. Pocket position relative to sprocket hole measured as true position of pocket, not pocket hole.

$A_o = 7.0 \text{ MM}$
 $A_1 = 1.8 \text{ MM}$
 $B_o = 7.0 \text{ MM}$
 $B_1 = 1.3 \text{ MM}$
 $K_o = 2.1 \text{ MM}$

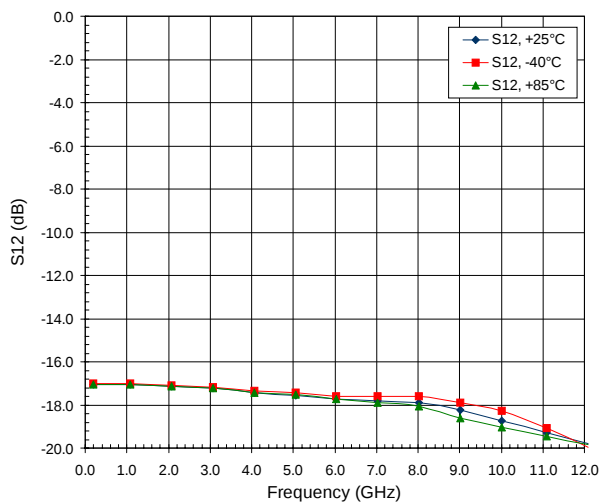
S11 versus Frequency, Over Temperature



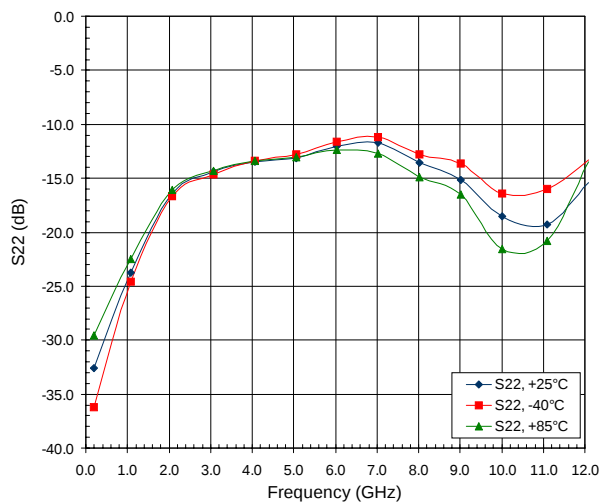
S21 versus Frequency, Over Temperature



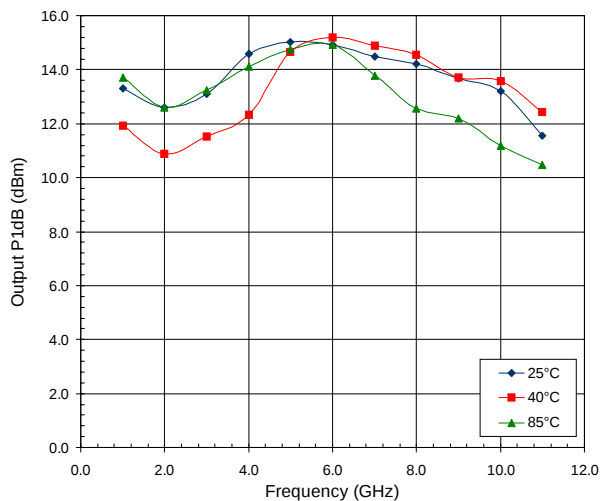
S12 versus Frequency, Over Temperature



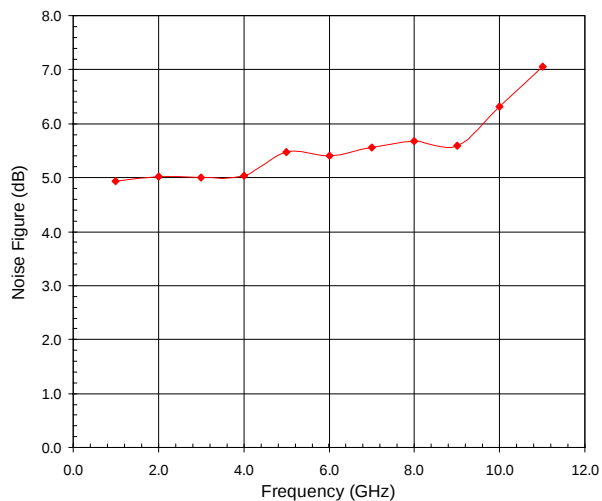
S22 versus Frequency, Over Temperature



Output P1dB versus Frequency Across Temperature



Noise Figure versus Frequency at +25°C



Note: The s-parameter gain results shown include device performance as well as evaluation board and connector loss variations. The insertion losses of the evaluation board and connectors are as follows:

1GHz to 4GHz=-0.06dB

5GHz to 9GHz=-0.22dB

10GHz to 14GHz=-0.50dB

15GHz to 20GHz=-1.08dB